

Sample Calculations, Stack Outlet, Method 5B/202, Run 1

Area of Sample Location

$$A_s = \pi \times \left(\frac{d_s}{2 \times 12} \right)^2$$

$$A_s = \pi \times \left(\frac{408}{2 \times 12} \right)^2$$

$$A_s = 908 \text{ ft}^2$$

where:

- A_s = area of sample location (ft²)
- d_s = diameter of sample location (in)
- 12 = conversion factor (in/ft)
- 2 = conversion factor (diameter to radius)

Stack Pressure Absolute

$$P_a = P_b + \frac{P_s}{13.6}$$

$$P_a = 29.56 + \frac{-0.2}{13.6}$$

$$P_a = 29.55 \text{ in.Hg}$$

where:

- P_a = stack pressure absolute (in. Hg)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure (in. H₂O)
- 13.6 = conversion factor (in. H₂O/in. Hg)

Volume of Dry Gas Collected Corrected to Standard Temperature and Pressure

$$V_{m(std)} = \frac{17.64(V_m)(Y_d)\left(P_b + \frac{\Delta H}{13.6}\right)}{(T_m + 460)}$$
$$V_{m(std)} = \frac{17.64(54.71)(0.9891)\left(29.56 + \frac{1.17}{13.6}\right)}{(100 + 460)}$$

$$V_{m(std)} = 50.54 \text{ scf}$$

where:

- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- V_m = volume of gas sampled at meter conditions (ft^3)
- Y_d = gas meter correction factor (dimensionless)
- P_b = barometric pressure (in. Hg)
- ΔH = average sample pressure (in. H_2O)
- T_m = average gas meter temperature ($^\circ\text{F}$)
- 13.6 = conversion factor (in. $\text{H}_2\text{O}/\text{in. Hg}$)
- 17.64 = ratio of standard temperature over standard pressure ($^\circ\text{R}/\text{in.Hg}$)
- 460 = conversion ($^\circ\text{F}$ to $^\circ\text{R}$)

Volume of Water Vapor Collected Corrected to Standard Temperature and Pressure

$$V_{w(std)} = 0.04715 \times (V_{wc} + V_{wsg})$$
$$V_{w(std)} = 0.04715 \times (150.4 + 25.6)$$
$$V_{w(std)} = 8.30 \text{ scf}$$

where:

- $V_{w(std)}$ = volume of water vapor at standard conditions (scf)
- V_{wc} = weight of liquid collected (g)
- V_{wsg} = weight gain of silica gel (g)
- 0.04715 = volume occupied by one gram of water at standard temperature and pressure (ft^3/g)

Percent Moisture²

$$B_{ws} = 100 \times \left[\frac{V_{w(std)}}{(V_{m(std)} + V_{w(std)})} \right]$$

$$B_{ws} = 100 \times \left[\frac{8.30}{(50.54 + 8.30)} \right]$$

$$B_{ws} = 14.1\%$$

where:

- B_{ws} = moisture content of the gas stream (%)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- $V_{w(std)}$ = volume of water vapor at standard conditions (scf)
- 100 = conversion factor

Molecular Weight of Dry Gas Stream³

$$M_d = \left(44 \times \frac{\%CO_2}{100} \right) + \left(32 \times \frac{\%O_2}{100} \right) + \left(28 \times \frac{(\%N_2)}{100} \right)$$

$$M_d = \left(44 \times \frac{12.7}{100} \right) + \left(32 \times \frac{6.53}{100} \right) + \left(28 \times \frac{(80.8)}{100} \right)$$

$$M_d = 30.29 \text{ lb / lbmole}$$

where:

- M_d = molecular weight of the dry gas stream (lb/lb-mole)
- $\%CO_2$ = carbon dioxide content of the dry gas stream (%)
- 44 = molecular weight of carbon dioxide (lb/lb-mole)
- $\%O_2$ = oxygen content of the dry gas stream (%)
- 32 = molecular weight of oxygen (lb/lb-mole)
- $\%N_2$ = nitrogen content of the dry gas stream (%)
- 28 = molecular weight of nitrogen and carbon monoxide (lb/lb-mole)
- 100 = conversion factor

² The moisture saturation point is used for all calculations if it is exceeded by the actual moisture content.

³ The remainder of the gas stream after subtracting carbon dioxide and oxygen is assumed to be nitrogen.

Molecular Weight of Wet Gas Stream

$$M_s = \left(M_d \times \left(1 - \frac{B_{ws}}{100} \right) \right) + \left(18 \times \frac{B_{ws}}{100} \right)$$

$$M_s = \left(30.29 \times \left(1 - \frac{14.1}{100} \right) \right) + \left(18 \times \frac{14.1}{100} \right)$$

$$M_s = 28.56 \text{ lb / lbmole}$$

where:

- M_s = molecular weight of the wet gas stream (lb/lb-mole)
- M_d = molecular weight of the dry gas stream (lb/lb-mole)
- B_{ws} = moisture content of the gas stream (%)
- 18 = molecular weight of water (lb/lb-mole)
- 100 = conversion factor

Velocity of Gas Stream

$$V_s = 85.49(C_p) \left(\sqrt{\Delta P} \right) \sqrt{\frac{(T_s + 460)}{(M_s) \left(P_b + \frac{P_s}{13.6} \right)}}$$

$$V_s = 85.49(0.84)(0.466) \sqrt{\frac{(129 + 460)}{(28.56) \left(29.56 + \frac{-0.2}{13.6} \right)}}$$

$$V_s = 28.0 \text{ ft / sec}$$

where:

- V_s = average velocity of the gas stream (ft/sec)
- C_p = pitot tube coefficient dimensionless
- $\sqrt{\Delta P}$ = average square root of velocity pressures (in. H₂O)^{1/2}
- T_s = average stack temperature (°F)
- M_s = molecular weight of the wet gas stream (lb/lb-mole)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure of gas stream (in. H₂O)
- 85.49 = pitot tube constant (ft/sec)/[(lb/lb-mole)(in. Hg)]/[(⁰R)(in. H₂O)]^{1.2}
- 460 = conversion (°F to °R)
- 13.6 = conversion factor (in. H₂O/in. Hg)

Volumetric Flow of Gas Stream - Actual Conditions

$$Q_a = 60(V_s)(A_s)$$

$$Q_a = 60(28.0)(908)$$

$$Q_a = 1,522,906 \text{ acfm}$$

where:

- Q_a = volumetric flow rate of the gas stream at actual conditions (acfm)
- V_s = average velocity of the gas stream (ft/sec)
- A_s = area of duct or stack (ft²)
- 60 = conversion factor (min/hr)

Volumetric Flow of Gas Stream - Standard Conditions

$$Q_{std} = \frac{17.64(Q_a) \left(P_b + \frac{P_s}{13.6} \right)}{(T_s + 460)}$$

$$Q_{std} = \frac{17.64(1,522,906) \left(29.56 + \frac{-0.2}{13.6} \right)}{(129 + 460)}$$

$$Q_{std} = 1,348,504 \text{ scfm}$$

where:

- Q_{std} = volumetric flow rate of the gas stream at standard conditions (scfm)
- Q_a = volumetric flow rate of the gas stream at actual conditions (acfm)
- T_s = average stack temperature (°F)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure of gas stream (in. H₂O)
- 13.6 = conversion factor (in. H₂O/in. Hg)
- 17.64 = ratio of standard temperature over standard pressure (°R/in. Hg)
- 460 = conversion (°F to °R)

Volumetric Flow of Gas Stream - Standard Conditions - Dry Basis

$$Q_{dstd} = Q_{std} \left(1 - \frac{B_{ws}}{100} \right)$$

$$Q_{dstd} = 1,348,504 \left(1 - \frac{14.1}{100} \right)$$

$$Q_{dstd} = 1,158,769 \text{ dscfm}$$

where:

- Q_{dstd} = volumetric flow rate of the gas stream at standard conditions, on a dry basis (dscfm)
- Q_{std} = volumetric flow rate of the gas stream at standard conditions (scfm)
- B_{ws} = moisture content of the gas stream (%)
- 100 = conversion factor

Area of Nozzle

$$A_n = \pi \times \left(\frac{d_n}{2 \times 12} \right)^2$$

$$A_n = \pi \times \left(\frac{0.312}{2 \times 12} \right)^2$$

$$A_n = 0.000531 \text{ ft}^2$$

where:

- A_n = area of nozzle (ft²)
- d_n = diameter of nozzle (in)
- 12 = conversion factor (in/ft)
- 2 = conversion factor (diameter to radius)

Percent Isokinetic

$$I = \frac{0.0945(T_s + 460)(V_{m(std)})}{\left(P_b + \frac{P_s}{13.6}\right)(v_s)(A_n)(\Theta)\left(1 - \frac{B_{ws}}{100}\right)}$$

$$I = \frac{0.0945(129 + 460)(50.54)}{\left(29.56 + \frac{-0.2}{13.6}\right)(28.0)(5.31 \times 10^{-4})(90)\left(1 - \frac{14.1}{100}\right)}$$

$$I = 82.9\%$$

where:

I	= percent isokinetic (%)
T _s	= average stack temperature (°F)
V _{m(std)}	= volume of gas collected at standard temperature and pressure (scf)
P _b	= barometric pressure (in. Hg)
P _s	= static pressure of gas stream (in. H ₂ O)
V _s	= average velocity of the gas stream (ft/sec)
A _n	= cross sectional area of nozzle (ft ²)
Θ	= sample time (min)
B _{ws}	= moisture content of the gas stream (%)
0.0945	= constant (°R/in. Hg)
460	= conversion (°F to °R)
13.6	= conversion factor (in. H ₂ O/in Hg)
100	= conversion factor

Acetone Wash Blank-Particulate

$$W_a = \frac{(m_{ab})(v_{aw})}{v_{awb}}$$

$$W_a = \frac{(0.0000)(200)}{100}$$

$$W_a = 0.0000g$$

where:

- W_a = particulate mass in acetone wash, blank corrected (g)
- m_{ab} = mass collected, acetone wash blank (g)
- v_{aw} = volume of acetone wash (ml)
- v_{awb} = volume of acetone wash blank (ml)

Mass in Front Half, Acetone Blank Corrected

$$m_f = m_{fil} + (m_a - W_a)$$

$$m_f = 0.0053 + (0.0289 - 0.0000)$$

$$m_f = 0.0342g$$

where:

- m_f = mass in front half filter, and acetone wash, blank corrected (g)
- m_{fil} = mass in front half filter (g)
- m_a = mass in acetone wash (g)
- W_a = particulate mass in acetone wash blank (g)

Total Particulate Catch

$$M_n = m_f + m_b$$

$$M_n = 0.0342 + 0.0172$$

$$M_n = 0.0513g$$

where:

- M_n = total mass catch (g)
- m_f = mass in front half filter, and acetone wash, blank corrected (g)
- m_b = mass in back half organic fraction, and inorganic fraction, blank corrected (g)

Total Particulate Concentration, grains/dscf

$$C_{gr, dscf} = \frac{(M_n)(15.43)}{V_{m, std}}$$

$$C_{gr, dscf} = \frac{(0.0513)(15.43)}{50.54}$$

$$C_{gr, dscf} = 0.0157 \text{ grains / dscf}$$

where:

- $C_{gr, dscf}$ = particulate concentration (grains/dscf)
- M_n = total particulate catch (g)
- $V_{m(std)}$ = volume of gas collected at standard conditions (scf)
- 15.43 = conversion factor (grains/g)

Calculated F_d Factor, dscf/mmBtu

$$F_d = K((K_{hd} \times H) + (K_c \times C) + (K_s \times S) + (K_n \times N) - (K_o \times O_2)) / GCV_w$$

$$F_d = 10^6 ((3.64 \times 4.53) + (1.53 \times 74.48) + (0.57 \times 4.20) + (0.14 \times 1.44) - (0.46 \times 7.62)) / 13,129$$

$$F_d = 9,866$$

where:

- F_d = calculated fuel factor (dscf/mmBtu)
- K = conversion factor (Btu/million Btu)
- K_{hd} = constant (scf/lb)
- H = weight percent hydrogen in coal (%)
- K_c = constant (scf/lb)
- C = weight percent carbon in coal (%)
- K_s = constant (scf/lb)
- S = weight percent sulfur in coal (%)
- K_n = constant (scf/lb)
- N = weight percent nitrogen in coal (%)
- K_o = constant (scf/lb)
- O_2 = weight percent oxygen in coal (%)
- GCV_w = gross calorific value of fuel, wet (Btu/lb)

Total Particulate Emission Rate, lb/mmBtu ⁴

$$E_{PM} = \frac{(M_n)(F_d)(20.9)}{(V_{m(std)})(453.6)(20.9 - O_2)}$$

$$E_{PM} = \frac{(0.0513)(9,866)(20.9)}{(50.54)(453.6)(20.9 - 6.53)}$$

$$E_{PM} = 0.0321 \text{ lb / mmBtu}$$

where:

- E_{PM} = total particulate matter emission rate, (lb/mmBtu)
- M_n = total particulate catch (g)
- F_d = fuel factor (dcsf/mmBtu)
- 20.9 = oxygen content of ambient air (%)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 453.6 = conversion factor (g/lb)
- % O_2 = oxygen content of the dry gas stream (%)

Total Particulate Emission Rate, lb/hr

$$E_{lb/hr} = \frac{(M_n)(Q_{dstd})(60)}{(V_{m,std})(453.6)}$$

$$E_{lb/hr} = \frac{(0.0513)(1,158,769)(60)}{(50.54)(453.6)}$$

$$E_{lb/hr} = 156 \text{ lb / hr}$$

where:

- $E_{lb/hr}$ = particulate emission rate (lb/hr)
- M_n = total particulate catch (g)
- $V_{m(std)}$ = volume of gas collected at standard conditions (scf)
- Q_{dstd} = volumetric flow rate of the dry gas stream at standard conditions (dscfm)
- 60 = conversion factor (min/hr)
- 453.6 = conversion factor (g/lb)

⁴ All particulate emission rates are calculated in a similar manner.

Sample Calculations, Method 26A, Run 1

Concentration of Hydrogen Chloride in Flue Gas (lb/dscf)

$$C_{HCl} = \frac{(M_{HCl})}{(V_{m(std)}) (10^3) (453.6)}$$

$$C_{HCl} = \frac{(0.194)}{(74.34) (10^3) (453.6)}$$

$$C_{HCl} = 5.75 \times 10^{-9} \text{ lb / dscf}$$

where:

- C_{HCl} = concentration of hydrogen chloride in flue gas (lb/dscf)
- M_{HCl} = mass of hydrogen chloride collected in sample (mg)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 10^3 = conversion factor (mg/g)
- 453.6 = conversion factor (g/lb)

Concentration of Hydrogen Chloride in Flue Gas (ppmdv)

$$C_{ppmv} = \frac{(M_{HCl}) (385.3) (10^6)}{(MW_{HCl}) (V_{m(std)}) (10^3) (453.6)}$$

$$C_{ppmv} = \frac{(0.194) (385.3) (10^6)}{(36.458) (74.34) (10^3) (453.6)}$$

$$C_{ppmv} = 0.0608 \text{ ppmdv}$$

where:

- C_{ppmv} = concentration of hydrogen chloride in flue gas (ppmv)
- M_{HCl} = mass of hydrogen chloride collected in sample (mg)
- 385.3 = volume occupied by one pound gas at standard conditions (dscf/lbmole)
- 10^6 = conversion factor (fraction to ppm)
- MW_{HCl} = molecular weight of hydrogen chloride (lb/lb-mole)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 10^3 = conversion factor (mg/g)
- 453.6 = conversion factor (g/lb)

Hydrogen Chloride Emission Rate, lb/mmBtu

$$E_{HCl} = \frac{(C_{HCl})(F_d)(20.9)}{(20.9 - O_2)}$$

$$E_{HCl} = \frac{(5.75 \times 10^{-9})(9,971)(20.9)}{(20.9 - 6.92)}$$

$$E_{HCl} = 0.0000858 \text{ lb} / \text{mmBtu}$$

where:

- E_{HCl} = hydrogen chloride emission rate, (lb/mmBtu)
- C_{HCl} = hydrogen chloride concentration, (lb/dscf)
- F_d = fuel factor (dcsf/mmBtu)
- 20.9 = oxygen content of ambient air (%)
- % O_2 = oxygen content of the dry gas stream (%)

Hydrogen Chloride Emission Rate

$$E_{HCl} = C_{HCl} \times Q_{dstd} \times 60$$

$$E_{HCl} = 5.75 \times 10^{-9} \times 1,184,178 \times 60$$

$$E_{HCl} = 0.409 \text{ lb} / \text{hr}$$

where:

- E_{HCl} = hydrogen chloride emission rate, (lb/hr)
- $C_{ppm\text{dv}}$ = hydrogen chloride concentration, dry basis, (ppm_{dv})
- Q_{dstd} = volumetric flow rate of the dry gas stream at standard conditions (dscfm)
- MW = molecular weight of hydrogen chloride (lb/lbmole)
- 60 = conversion factor (min/hr)
- 385.3 = volume occupied by one pound gas at standard conditions (dscf/lbmole)
- 10^6 = conversion factor (fraction to ppm)

Sample Calculations, Method 29, Run 1

Concentration of Lead in Flue Gas, ug/dscm⁵

$$C_{ug/dscm} = \frac{(M_c)}{(V_{m(std)})} (35.31)$$

$$C_{ug/dscm} = \frac{(5.36)}{(64.59)} (35.31)$$

$$C_{ug/dscm} = 2.93ug/dscm$$

where:

- $C_{ug/dscm}$ = concentration of lead in flue gas (ug/dscm)
- M_c = mass of lead in sample (ug)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 35.31 = conversion factor (ft^3/m^3)

Emission Rate of Lead in Flue Gas, lb/mmBtu⁶

$$E = \frac{(C_{ug/dscm})(F_d)(20.9)}{(35.315)(20.9 - \%O_2)(453.6)(10^6)}$$

$$E = \frac{(2.93)(9,971)(20.9)}{(35.31)(20.9 - 6.92)(453.6)(10^6)}$$

$$E = 2.72 \times 10^{-6} mg/dscm@7\%O_2$$

where:

- E = lead emission rate (lb/mmBtu)
- $C_{ug/dscm}$ = lead concentration (ug/dscm)
- F_d = fuel factor (dcsf/mmBtu)
- 35.31 = conversion factor (ft^3/m^3)
- 20.9 = oxygen content of ambient air (%)
- $\%O_2$ = oxygen content of the dry gas stream (%)
- 453.6 = conversion factor (g/lb)
- 10^6 = conversion factor (ug/g)

⁵ The concentrations of all MHs and mercury are calculated in a similar manner.

⁶ The emission rates of all MHs and mercury are calculated in a similar manner.

Lead Emission Rate, lb/hr

$$E_{lb/hr} = \frac{(C_{ug/dscm})(Q_{dstd})(60)}{(35.31)(10^6)(453.6)}$$

$$E_{lb/hr} = \frac{(2.93)(1,187,686)(60)}{(35.31)(10^3)(10^3)(453.6)}$$

$$E_{lb/hr} = 0.0130 lb/hr$$

where:

$E_{lb/hr}$	= lead emission rate (lb/hr)
$C_{ug/dscm}$	= lead concentration (ug/dscm)
Q_{dstd}	= volumetric flow rate of dry gas stream at standard conditions (dscfm)
10^3	= conversion factor (ug/mg)
10^3	= conversion factor (mg/g)
35.31	= conversion factor (ft ³ /m ³)
60.0	= conversion factor (min/hr)
453.6	= conversion factor (g/lb)