

Sample Calculations

Sample Calculations, Stack Outlet, Method 5B/202, Run 1

Area of Sample Location

$$A_s = \pi \times \left(\frac{d_s}{2 \times 12} \right)^2$$

$$A_s = \pi \times \left(\frac{180}{2 \times 12} \right)^2$$

$$A_s = 177 \text{ ft}^2$$

where:

- A_s = area of sample location (ft²)
- d_s = diameter of sample location (in)
- 12 = conversion factor (in/ft)
- 2 = conversion factor (diameter to radius)

Stack Pressure Absolute

$$P_a = P_b + \frac{P_s}{13.6}$$

$$P_a = 29.56 + \frac{-0.1}{13.6}$$

$$P_a = 29.55 \text{ in. Hg}$$

where:

- P_a = stack pressure absolute (in. Hg)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure (in. H₂O)
- 13.6 = conversion factor (in. H₂O/in. Hg)

Volume of Dry Gas Collected Corrected to Standard Temperature and Pressure

$$V_{m(std)} = \frac{17.64(V_m)(Y_d)\left(P_b + \frac{\Delta H}{13.6}\right)}{(T_m + 460)}$$
$$V_{m(std)} = \frac{17.64(60.01)(1.0034)\left(29.56 + \frac{1.73}{13.6}\right)}{(91.9 + 460)}$$
$$V_{m(std)} = 60.01 \text{ scf}$$

where:

- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- V_m = volume of gas sampled at meter conditions (ft^3)
- Y_d = gas meter correction factor (dimensionless)
- P_b = barometric pressure (in. Hg)
- ΔH = average sample pressure (in. H_2O)
- T_m = average gas meter temperature ($^{\circ}\text{F}$)
- 13.6 = conversion factor (in. $\text{H}_2\text{O}/\text{in. Hg}$)
- 17.64 = ratio of standard temperature over standard pressure ($^{\circ}\text{R}/\text{in.Hg}$)
- 460 = conversion ($^{\circ}\text{F}$ to $^{\circ}\text{R}$)

Volume of Water Vapor Collected Corrected to Standard Temperature and Pressure

$$V_{w(std)} = 0.04715 \times (V_{wc} + V_{wsg})$$
$$V_{w(std)} = 0.04715 \times (175.8 + 11.0)$$
$$V_{w(std)} = 8.81 \text{ scf}$$

where:

- $V_{w(std)}$ = volume of water vapor at standard conditions (scf)
- V_{wc} = weight of liquid collected (g)
- V_{wsg} = weight gain of silica gel (g)
- 0.04715 = volume occupied by one gram of water at standard temperature and pressure (ft^3/g)

Percent Moisture²

$$B_{ws} = 100 \times \left[\frac{V_{w(std)}}{V_{m(std)} + V_{w(std)}} \right]$$

$$B_{ws} = 100 \times \left[\frac{8.81}{(60.01 + 8.81)} \right]$$

$$B_{ws} = 12.8\%$$

where:

B_{ws} = moisture content of the gas stream (%)

$V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)

$V_{w(std)}$ = volume of water vapor at standard conditions (scf)

100 = conversion factor

Molecular Weight of Dry Gas Stream³

$$M_d = \left(44 \times \frac{\%CO_2}{100} \right) + \left(32 \times \frac{\%O_2}{100} \right) + \left(28 \times \frac{(\%N_2)}{100} \right)$$

$$M_d = \left(44 \times \frac{11.6}{100} \right) + \left(32 \times \frac{7.72}{100} \right) + \left(28 \times \frac{(80.7)}{100} \right)$$

$$M_d = 30.16 \text{ lb/lbmole}$$

where:

M_d = molecular weight of the dry gas stream (lb/lb-mole)

$\%CO_2$ = carbon dioxide content of the dry gas stream (%)

44 = molecular weight of carbon dioxide (lb/lb-mole)

$\%O_2$ = oxygen content of the dry gas stream (%)

32 = molecular weight of oxygen (lb/lb-mole)

$\%N_2$ = nitrogen content of the dry gas stream (%)

28 = molecular weight of nitrogen and carbon monoxide (lb/lb-mole)

100 = conversion factor

² The moisture saturation point is used for all calculations if it is exceeded by the actual moisture content.

³ The remainder of the gas stream after subtracting carbon dioxide and oxygen is assumed to be nitrogen.

Molecular Weight of Wet Gas Stream

$$M_s = \left(M_d \times \left(1 - \frac{B_{ws}}{100} \right) \right) + \left(18 \times \frac{B_{ws}}{100} \right)$$

$$M_s = \left(30.16 \times \left(1 - \frac{12.8}{100} \right) \right) + \left(18 \times \frac{12.8}{100} \right)$$

$$M_s = 28.61 \text{ lb/lbmole}$$

where:

- M_s = molecular weight of the wet gas stream (lb/lb-mole)
- M_d = molecular weight of the dry gas stream (lb/lb-mole)
- B_{ws} = moisture content of the gas stream (%)
- 18 = molecular weight of water (lb/lb-mole)
- 100 = conversion factor

Velocity of Gas Stream

$$V_s = 85.49 (C_p) \left(\sqrt{\Delta P} \right) \sqrt{\frac{(T_s + 460)}{(M_s) \left(P_b + \frac{P_s}{13.6} \right)}}$$

$$V_s = 85.49 (0.84) (1.39) \sqrt{\frac{(128 + 460)}{(28.61) \left(29.56 + \frac{-0.1}{13.6} \right)}}$$

$$V_s = 83.2 \text{ ft/sec}$$

where:

- V_s = average velocity of the gas stream (ft/sec)
- C_p = pitot tube coefficient dimensionless
- $\sqrt{\Delta P}$ = average square root of velocity pressures (in. H₂O)^{1.2}
- T_s = average stack temperature (°F)
- M_s = molecular weight of the wet gas stream (lb/lb-mole)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure of gas stream (in. H₂O)
- 85.49 = pitot tube constant (ft/sec)/[(lb/lb-mole)(in. Hg)]/[({°R})(in. H₂O)]^{1/2}
- 460 = conversion (°F to °R)
- 13.6 = conversion factor (in. H₂O/in. Hg)

Volumetric Flow of Gas Stream - Actual Conditions

$$Q_a = 60(V_s)(A_s)$$

$$Q_a = 60(83.2)(177)$$

$$Q_a = 882,234 \text{ acfm}$$

where:

Q_a = volumetric flow rate of the gas stream at actual conditions (acfm)

V_s = average velocity of the gas stream (ft/sec)

A_s = area of duct or stack (ft²)

60 = conversion factor (min/hr)

Volumetric Flow of Gas Stream - Standard Conditions

$$Q_{std} = \frac{17.64(Q_a) \left(P_b + \frac{P_s}{13.6} \right)}{(T_s + 460)}$$

$$Q_{std} = \frac{17.64(882,234) \left(29.56 + \frac{-0.1}{13.6} \right)}{(128 + 460)}$$

$$Q_{std} = 782,725 \text{ scfm}$$

where:

Q_{std} = volumetric flow rate of the gas stream at standard conditions (scfm)

Q_a = volumetric flow rate of the gas stream at actual conditions (acfm)

T_s = average stack temperature (°F)

P_b = barometric pressure (in. Hg)

P_s = static pressure of gas stream (in. H₂O)

13.6 = conversion factor (in. H₂O/in. Hg)

17.64 = ratio of standard temperature over standard pressure (°R/in. Hg)

460 = conversion (°F to °R)

Volumetric Flow of Gas Stream - Standard Conditions - Dry Basis

$$Q_{dstd} = Q_{std} \left(1 - \frac{B_{ws}}{100} \right)$$

$$Q_{dstd} = 782,715 \left(1 - \frac{12.8}{100} \right)$$

$$Q_{dstd} = 682,820 \text{ dscfm}$$

where:

Q_{dstd} = volumetric flow rate of the gas stream at standard conditions, on a dry basis (dscfm)

Q_{std} = volumetric flow rate of the gas stream at standard conditions (scfm)

B_{ws} = moisture content of the gas stream (%)

100 = conversion factor

Area of Nozzle

$$A_n = \pi \times \left(\frac{d_n}{2 \times 12} \right)^2$$

$$A_n = \pi \times \left(\frac{0.184}{2 \times 12} \right)^2$$

$$A_n = 0.000185 \text{ ft}^2$$

where:

A_n = area of nozzle (ft²)

d_n = diameter of nozzle (in)

12 = conversion factor (in/ft)

2 = conversion factor (diameter to radius)

Percent Isokinetic

$$I = \frac{0.0945(T_s + 460)(V_{m(std)})}{\left(P_b + \frac{P_s}{13.6}\right)(v_s)(A_n)(\Theta)\left(1 - \frac{B_{ws}}{100}\right)}$$

$$I = \frac{0.0945(128 + 460)(60.01)}{\left(29.56 + \frac{-0.1}{13.6}\right)(83.2)(1.85 \times 10^{-4})(90)\left(1 - \frac{12.8}{100}\right)}$$

$$I = 93.5\%$$

where:

I	= percent isokinetic (%)
T _s	= average stack temperature (°F)
V _{m(std)}	= volume of gas collected at standard temperature and pressure (scf)
P _b	= barometric pressure (in. Hg)
P _s	= static pressure of gas stream (in. H ₂ O)
V _s	= average velocity of the gas stream (ft/sec)
A _n	= cross sectional area of nozzle (ft ²)
Θ	= sample time (min)
B _{ws}	= moisture content of the gas stream (%)
0.0945	= constant (°R/in. Hg)
460	= conversion (°F to °R)
13.6	= conversion factor (in. H ₂ O/in Hg)
100	= conversion factor

Acetone Wash Blank-Particulate

$$W_a = \frac{(m_{ab})(v_{aw})}{v_{awb}}$$

$$W_a = \frac{(0.0000)(75)}{200}$$

$$W_a = 0.0000g$$

where:

- W_a = particulate mass in acetone wash, blank corrected (g)
- m_{ab} = mass collected, acetone wash blank (g)
- v_{aw} = volume of acetone wash (ml)
- v_{awb} = volume of acetone wash blank (ml)

Mass in Front Half, Acetone Blank Corrected

$$m_f = m_{fil} + (m_a - W_a)$$

$$m_f = 0.0026 + (0.0058 - 0.0000)$$

$$m_f = 0.0083g$$

where:

- m_f = mass in front half filter, and acetone wash, blank corrected (g)
- m_{fil} = mass in front half filter (g)
- m_a = mass in acetone wash (g)
- W_a = particulate mass in acetone wash blank (g)

Total Particulate Catch

$$M_n = m_f + m_b$$

$$M_n = 0.0083 + 0.0137$$

$$M_n = 0.0220g$$

where:

- M_n = total mass catch (g)
- m_f = mass in front half filter, and acetone wash, blank corrected (g)
- m_b = mass in back half organic fraction, and inorganic fraction, blank corrected (g)

Total Particulate Concentration, grains/dscf

$$C_{gr./dscf} = \frac{(M_n)(15.43)}{V_{m,std}}$$

$$C_{gr./dscf} = \frac{(0.0220)(15.43)}{60.01}$$

$$C_{gr./dscf} = 0.00566 \text{ grains / dscf}$$

where:

- $C_{gr./dscf}$ = particulate concentration (grains/dscf)
- M_n = total particulate catch (g)
- $V_{m(std)}$ = volume of gas collected at standard conditions (scf)
- 15.43 = conversion factor (grains/g)

Calculated F_d Factor, dscf/mmBtu

$$F_d = K((K_{hd} \times H) + (K_c \times C) + (K_s \times S) + (K_n \times N) - (K_o \times O_2)) / GCV_w$$

$$F_d = 10^6 ((3.64 \times 4.83) + (1.53 \times 73.83) + (0.57 \times 3.59) + (0.14 \times 1.51) - (0.46 \times 8.24)) / 13,080$$

$$F_d = 9,863$$

where:

- F_d = calculated fuel factor (dscf/mmBtu)
- K = conversion factor (Btu/million Btu)
- K_{hd} = constant (scf/lb)
- H = weight percent hydrogen in coal (%)
- K_c = constant (scf/lb)
- C = weight percent carbon in coal (%)
- K_s = constant (scf/lb)
- S = weight percent sulfur in coal (%)
- K_n = constant (scf/lb)
- N = weight percent nitrogen in coal (%)
- K_o = constant (scf/lb)
- O_2 = weight percent oxygen in coal (%)
- GCV_w = gross calorific value of fuel, wet (Btu/lb)

Total Particulate Emission Rate, lb/mmBtu⁴

$$E_{PM} = \frac{(M_n)(F_d)(20.9)}{(V_{m(std)})(453.6)(20.9 - O_2)}$$
$$E_{PM} = \frac{(0.0220)(9,863)(20.9)}{(60.27)(453.6)(20.9 - 7.72)}$$
$$E_{PM} = 0.0126 \text{ lb / mmBtu}$$

where:

- E_{PM} = total particulate matter emission rate, (lb/mmBtu)
- M_n = total particulate catch (g)
- F_d = fuel factor (dcsf/mmBtu)
- 20.9 = oxygen content of ambient air (%)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 453.6 = conversion factor (g/lb)
- % O_2 = oxygen content of the dry gas stream (%)

Total Particulate Emission Rate, lb/hr

$$E_{lb/hr} = \frac{(M_n)(Q_{dstd})(60)}{(V_{m,std})(453.6)}$$
$$E_{lb/hr} = \frac{(0.0220)(682,820)(60)}{(60.01)(453.6)}$$
$$E_{lb/hr} = 33.1 \text{ lb / hr}$$

where:

- $E_{lb/hr}$ = particulate emission rate (lb/hr)
- M_n = total particulate catch (g)
- $V_{m(std)}$ = volume of gas collected at standard conditions (scf)
- Q_{dstd} = volumetric flow rate of the dry gas stream at standard conditions (dscfm)
- 60 = conversion factor (min/hr)
- 453.6 = conversion factor (g/lb)

⁴ All particulate emission rates are calculated in a similar manner.

Sample Calculations, Method 26A, Run 1

Concentration of Hydrogen Chloride in Flue Gas (lb/dscf)⁵

$$C_{HCl} = \frac{(M_{HCl})}{(V_{m(std)}) (10^3) (453.6)}$$

$$C_{HCl} = \frac{(1.15)}{(94.71)(10^3)(453.6)}$$

$$C_{HCl} = 2.68 \times 10^{-8} \text{ lb / dscf}$$

where:

- C_{HCl} = concentration of hydrogen chloride in flue gas (lb/dscf)
- M_{HCl} = mass of hydrogen chloride collected in sample (mg)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 10^3 = conversion factor (mg/g)
- 453.6 = conversion factor (g/lb)

Concentration of Hydrogen Chloride in Flue Gas (ppmdv)⁶

$$C_{ppmv} = \frac{(M_{HCl})(385.3)(10^6)}{(MW_{HCl})(V_{m(std)}) (10^3) (453.6)}$$

$$C_{ppmv} = \frac{(1.15)(385.3)(10^6)}{(36.458)(94.71)(10^3)(453.6)}$$

$$C_{ppmv} = 0.283 \text{ ppmdv}$$

where:

- C_{ppmv} = concentration of hydrogen chloride in flue gas (ppmv)
- M_{HCl} = mass of hydrogen chloride collected in sample (mg)
- 385.3 = volume occupied by one pound gas at standard conditions (dscf/lbmole)
- 10^6 = conversion factor (fraction to ppm)
- MW_{HCl} = molecular weight of hydrogen chloride (lb/lb-mole)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 10^3 = conversion factor (mg/g)
- 453.6 = conversion factor (g/lb)

⁵ The HF concentration was calculated in a similar manner.

⁶ The HF concentration was calculated in a similar manner.

Hydrogen Chloride Emission Rate, lb/mmBtu⁷

$$E_{HCl} = \frac{(C_{HCl})(F_d)(20.9)}{(20.9 - O_2)}$$

$$E_{HCl} = \frac{(2.68 \times 10^{-8})(9,863)(20.9)}{(20.9 - 7.72)}$$

$$E_{HCl} = 0.000419 \text{ lb} / \text{mmBtu}$$

where:

- E_{HCl} = hydrogen chloride emission rate, (lb/mmBtu)
- C_{HCl} = hydrogen chloride concentration, (lb/dscf)
- F_d = fuel factor (dscf/mmBtu)
- 20.9 = oxygen content of ambient air (%)
- % O_2 = oxygen content of the dry gas stream (%)

Hydrogen Chloride Emission Rate

$$E_{HCl} = C_{HCl} \times Q_{dstd} \times 60$$

$$E_{HCl} = 2.68 \times 10^{-8} \times 654,404 \times 60$$

$$E_{HCl} = 1.05 \text{ lb} / \text{hr}$$

where:

- E_{HCl} = hydrogen chloride emission rate, (lb/hr)
- $C_{ppm dv}$ = hydrogen chloride concentration, dry basis, (ppm dv)
- Q_{dstd} = volumetric flow rate of the dry gas stream at standard conditions (dscfm)
- MW = molecular weight of hydrogen chloride (lb/lbmole)
- 60 = conversion factor (min/hr)
- 385.3 = volume occupied by one pound gas at standard conditions (dscf/lbmole)
- 10^6 = conversion factor (fraction to ppm)

⁷ The HF emission rate was calculated in a similar manner.

Sample Calculations, Method 29, Run 1

Concentration of Lead in Flue Gas, ug/dscm⁸

$$C_{ug/dscm} = \frac{(M_C)}{(V_{m(std)})} (35.31)$$

$$C_{ug/dscm} = \frac{(4.79)}{(66.01)} (35.31)$$

$$C_{ug/dscm} = 2.56 \text{ ug / dscm}$$

where:

- $C_{ug/dscm}$ = concentration of lead in flue gas (ug/dscm)
- M_C = mass of lead in sample (ug)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 35.31 = conversion factor (ft^3/m^3)

Emission Rate of Lead in Flue Gas, lb/mmBtu⁹

$$E = \frac{(C_{ug/dscm})(F_d)(20.9)}{(35.315)(20.9 - \%O_2)(453.6)(10^6)}$$

$$E = \frac{(2.56)(9,863)(20.9)}{(35.315)(20.9 - 7.72)(453.6)(10^6)}$$

$$E = 2.50 \times 10^{-6} \text{ lb / mmBtu}$$

where:

- E = lead emission rate (lb/mmBtu)
- $C_{ug/dscm}$ = lead concentration (ug/dscm)
- F_d = fuel factor (dcsf/mmBtu)
- 35.31 = conversion factor (ft^3/m^3)
- 20.9 = oxygen content of ambient air (%)
- $\%O_2$ = oxygen content of the dry gas stream (%)
- 453.6 = conversion factor (g/lb)
- 10^6 = conversion factor (ug/g)

⁸ The concentrations of all MHs and mercury are calculated in a similar manner.

⁹ The emission rates of all MHs and mercury are calculated in a similar manner.

Lead Emission Rate, lb/hr

$$E_{lb/hr} = \frac{(C_{ug/dscm})(Q_{dstd})(60)}{(35.31)(10^6)(453.6)}$$

$$E_{lb/hr} = \frac{(2.56)(684,896)(60)}{(35.31)(10^3)(10^3)(453.6)}$$

$$E_{lb/hr} = 0.00657 lb/hr$$

where:

$E_{lb/hr}$	= lead emission rate (lb/hr)
$C_{ug/dscm}$	= lead concentration (ug/dscm)
Q_{dstd}	= volumetric flow rate of dry gas stream at standard conditions (dscfm)
10^3	= conversion factor (ug/mg)
10^3	= conversion factor (mg/g)
35.31	= conversion factor (ft ³ /m ³)
60.0	= conversion factor (min/hr)
453.59	= conversion factor (g/lb)