



**Report on the  
Air Emissions Test Program**

**Conducted for Big Rivers Electric Corporation  
At the Green Station Facility located in Robards, Kentucky**

*Report No. 3648 Green Unit 1  
August 29, 2011*

## Table of Contents

<b>PROJECT OVERVIEW</b> .....	<b>2</b>
<i>General</i> .....	2
<i>Methodology</i> .....	2
Parameters.....	4
<i>Results</i> .....	4
<b>SUMMARY OF RESULTS</b> .....	<b>6</b>
<i>Table 1 – Summary of Inlet A HCl and HF Results</i> .....	6
<i>Table 2 – Summary of Inlet A Hg Results</i> .....	7
<i>Table 3 – Summary of Inlet B HCl and HF Results</i> .....	8
<i>Table 4 – Summary of Inlet B Hg Results</i> .....	9
<i>Table 5 – Summary of the Stack Outlet FPM and CPM Results</i> .....	10
<i>Table 6 – Summary of the Stack Outlet HCl and HF Results</i> .....	11
<i>Table 7 – Summary of the Stack Outlet Metallic HAP Results</i> .....	12
<i>Table 8 – Summary of the Stack Outlet Hg Results</i> .....	14
<b>TEST PROCEDURES</b> .....	<b>15</b>
<i>Method Listing</i> .....	15
<i>Method Descriptions</i> .....	15
Method 1 .....	15
Method 2.....	16
Method 3.....	16
Method 4.....	17
Method 5B/202 .....	17
Method 19.....	20
Method 26A.....	20
Method 29.....	21
Method 30B .....	22
<b>APPENDIX</b>	
Figures	
Sample Calculations	
Parameters	
Field Data Printouts	
Field Data	
Analyzer Data	
Laboratory Data	
Calibration Data	

## Project Overview

### General

Airtech Environmental Services Inc. (Airtech) was contracted by Big Rivers Electric Corporation (Big Rivers) to perform an air emission test program at the Green Station facility located in Robards, Kentucky. Testing was conducted to gather stack test data for an evaluation of any corrective action that may be needed to comply with the Transport Rule and Utility MACT emission limits.

Testing was conducted at the inlets to the Unit 1 electrostatic precipitator (ESP) also referred to herein as Inlet A and Inlet B and the Unit 1 Stack outlet. Testing was conducted to meet the requirements of Big Rivers and Sargent & Lundy, LLC.

The specific objectives of the test program were:

- Determine the emissions of filterable particulate matter (FPM) and condensable particulate matter (CPM) from the Unit 1 exhaust stack.
- Determine the emissions of hydrogen chloride (HCl) and hydrogen fluoride (HF) from both the Unit 1 ESP inlets and the exhaust stack.
- Determine the emissions of metallic hazardous air pollutants (HAP)<sup>1</sup> from the Unit 1 exhaust stack.
- Determine the emissions of ash bound, oxidized and elemental mercury (Hg) from both the Unit 1 ESP inlets and the exhaust stack.

Testing was performed on July 27, 2011. Coordinating the field portion of the test program were:

Mike Galbraith – Big Rivers Electric Corporation  
Brandon Check – Airtech Environmental Services Inc.

### Methodology

All methods employed during the test program were performed in strict adherence with the latest published version(s). Recovery of all sample trains was performed in an on-site mobile laboratory. All sample trains were sealed with Teflon tape when not in use. All test components were sealed when transported between the laboratory and the test location. All field technicians wore polyethylene or plastic gloves while recovering field samples.

As much as possible, testing for a given pollutant was conducted simultaneously at the ESP exhausts and stack locations.

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<sup>1</sup> Metallic HAPs are defined as: antimony (Sb), arsenic (As), beryllium (Be), cadmium (Cd), chromium (Cr), cobalt (Co), lead (Pb), manganese (Mn), nickel (Ni) and selenium (Se).

EPA Methods 5B and 202 were used in a combined sampling train to determine the concentrations of non-sulfuric acid filterable particulate matter (FPM), condensable particulate matter (CPM) and total PM at the Unit 1 exhaust stack. For the EPA Methods 5B/202, a sample of the gas stream was withdrawn isokinetically from the source. Non-sulfuric acid FPM was collected in a heated probe and on a heated glass fiber filter. CPM passed through the probe and filter and was collected in a dry, glass impinger system. The amount of particulate matter collected with each sample fraction was compared to the volume of dry gas sampled to calculate a particulate concentration. Results for FPM, CPM and total PM are expressed in units of grains per dry standard cubic foot (gr/dscf), in units of pounds per hour (lb/hr) and in units of pounds per million Btu (lb/mmBtu).

EPA Method 26A was used to determine the concentrations of HCl and HF at the ESP inlets and stack test locations. For the EPA Method 26A, a sample of the stack gas was withdrawn isokinetically from the source through a glass nozzle, a heated probe and a heated Teflon filter. HCl and HF in the sample stream passed through the probe and filter and were collected in a series of impingers containing a dilute sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) solution. At the conclusion of each test run, the H<sub>2</sub>SO<sub>4</sub> solution was recovered from the sampling train and analyzed for HCl and HF by ion chromatography. Analysis was performed at the Airtech laboratory located in Denver, Colorado. HCl and HF results are expressed in pounds per dry standard cubic foot (lb/dscf), parts per million, dry volume basis (ppmdv), pounds per million Btu (lb/mmBtu) and pounds per hour (lb/hr). Three (3) test runs were performed.

EPA Method 29 was used to determine the metallic HAPs concentrations at the stack outlet. For this project, metallic HAPs are defined as antimony (Sb), arsenic (As), beryllium (Be), cadmium (Cd), chromium (Cr), cobalt (Co), lead (Pb), manganese (Mn), nickel (Ni) and selenium (Se). With the Method 29 approach, a sample of the gas stream was withdrawn isokinetically from the stack and the metallic HAPs in the sample gas were collected in a heated glass sample probe, on a heated quartz fiber filter, and in a series of chilled, glass impingers charged with metals absorbing solution. Analysis of the samples was performed by ElementOne Laboratories located in Wilmington, North Carolina. Metallic HAPs results are expressed in units of micrograms per dry standard cubic meter (ug/dscm), pounds per million Btu (lb/mmBtu) and pounds per hour (lb/hr). Three (3) test runs were performed.

EPA Method 30B was used to determine the concentrations of ash bound, oxidized, elemental and total vapor-phase Hg at each test location. For the EPA Method 30B, a sample of the effluent was withdrawn from the source at a constant rate through paired, in-situ, sorbent media traps. One trap was spiked and the other was packed with multiple stages of media designed to separately collect ash bound mercury, total gaseous oxidized mercury (Hg<sup>+2</sup>) and total gaseous elemental mercury (Hg<sup>0</sup>). Because the speciating tubes are sensitive to sample loss and breakthrough at temperatures in excess of 210°F, air cooled probes were employed at the ESP outlet test location. The air cooled probes used small fans to circulate ambient air through the outer sheath, thus keeping the temperature of the traps below the critical temperature. At both test locations, probe heaters were also

in operation to ensure that the tubes were maintained above the dew point of the sample gas. The masses of the mercury species collected with the traps was compared to the volume of dry gas sampled to calculate the mercury concentrations. Analysis for the various mercury species was performed by Airtech Environmental Services Inc. at its laboratory located in Denver, Colorado. Results for Hg are expressed in units of micrograms per dry standard cubic meter (ug/dscm), pounds per million Btu (lb/mmBtu) and pounds per hour (lb/hr). Three (3), ninety-minute test runs were performed at each test location.

### ***Parameters***

The following specific parameters were determined at each test location except where noted:

- gas temperature
- volumetric flow rate
- carbon dioxide content
- oxygen content
- moisture content
- filterable particulate matter (Stack only)
- condensable particulate matter concentration (Stack only)
- hydrogen chloride concentration
- hydrogen fluoride concentration
- metallic hazardous air pollutant concentration (Stack only)
- ash bound mercury concentration
- oxidized mercury concentration
- elemental mercury concentration

### **Results**

A summary of test results is presented in Tables 1 through 8 on Pages 6 through 14.

The  $F_d$  factors listed in the tables were calculated from coal samples collected during the testing. The  $F_d$  factor worksheets can be found in the Parameters section of the Appendix. All coal analysis can be found in the Laboratory section of the Appendix.

For the metals results, if a metal was not detected in one fraction of the sample train but detected in another fraction of the sample train, the reporting limit was used in the calculation of the total amount collected by the sample train for the non-detect fraction. These metals results are noted with a “\*”.

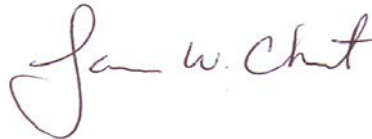
To calculate the mass emission rates for mercury at the ESP Outlets the volumetric flow rate determined by the Method 26A sampling trains was used. At the stack location, the mass emission rates for mercury were determined using the volumetric flow rate from the Method 29 sampling train.

Each Method 30B test run consisted of a spiked sample and an un-spiked sample. For this testing all spikes met the method spike recovery requirement of  $85\% < R < 115\%$ . All samples also met the relative deviation duplicate requirement of  $RD < 10\%$ . Individual spike recovery and duplicate results analysis can be found in the parameters section of the Appendix.

All carbon dioxide data was downloaded from the installed Plant continuous emission monitoring system (CEMS). Oxygen values were calculated using the Plant CO<sub>2</sub> data and the F<sub>o</sub> calculations listed in EPA Method 3B. Because the CEMS are located only at the stack, the inlet carbon dioxide and oxygen concentrations were assumed to be the same as the stack.

Submitted by:

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Cathy Busse

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James Christ

## Summary of Results

**Table 1 – Summary of Inlet A HCl and HF Results**

<b><u>Test Parameters</u></b>	<b>Run 1</b>	<b>Run 2</b>	<b>Run 3</b>	<b>Average</b>
Date	7/27/11	7/27/11	7/27/11	
Start Time	7:53	11:16	14:08	
Stop Time	10:15	13:35	13:35	
Fd (dscf/mmBtu)	10,185	9,926	9,868	
<b><u>Gas Conditions</u></b>				
Temperature (°F)	301	306	307	<b>305</b>
Volumetric Flow Rate (acfm)	469,000	463,100	441,400	<b>457,800</b>
Volumetric Flow Rate (scfm)	307,400	301,600	286,900	<b>298,600</b>
Volumetric Flow Rate (dscfm)	281,500	274,800	265,300	<b>273,900</b>
Carbon Dioxide (% dry)	11.1	11.0	11.1	<b>11.1</b>
Oxygen (% dry)	8.17	8.31	8.25	<b>8.24</b>
Moisture (%)	8.46	8.92	7.57	<b>8.32</b>
<b><u>Hydrogen Chloride Results</u></b>				
Concentration (lb/dscf)	1.31E-06	1.48E-06	2.11E-06	<b>1.64E-06</b>
Concentration (ppmdv)	13.9	15.7	22.3	<b>17.3</b>
Emission Rate (lb/mmBtu)	0.0219	0.0244	0.0345	<b>0.0269</b>
Emission Rate (lb/hr)	22.2	24.4	33.6	<b>26.7</b>
<b><u>Hydrogen Fluoride Results</u></b>				
Concentration (lb/dscf)	2.41E-07	3.18E-07	4.50E-07	<b>3.36E-07</b>
Concentration (ppmdv)	4.63	6.12	8.67	<b>6.47</b>
Emission Rate (lb/mmBtu)	0.00402	0.00523	0.00734	<b>0.00553</b>
Emission Rate (lb/hr)	4.06	5.24	7.17	<b>5.49</b>

**Table 2 – Summary of Inlet A Hg Results**

<b><u>Test Parameters</u></b>	<b>Run 1</b>	<b>Run 2</b>	<b>Run 3</b>	<b>Average</b>
Date	7/27/11	7/27/11	7/27/11	
Start Time	7:53	11:16	14:08	
Stop Time	9:26	12:48	15:41	
Fd (dscf/mmBtu)	10,185	9,926	9,868	
<b><u>Gas Conditions</u></b>				
M26A Volumetric Flowrate, (dscfm)	281,500	274,800	265,300	<b>273,867</b>
M26A Oxygen (% dry)	8.17	8.31	8.25	<b>8.24</b>
M26A Moisture (%)	8.46	8.92	7.57	<b>8.32</b>
<b><u>Ash Bound Mercury Results</u></b>				
Concentration Train A (µg/dscm)	2.26	2.78	3.95	<b>3.00</b>
Emission Rate (lb/mmBtu)	2.36E-06	2.86E-06	4.02E-06	<b>3.08E-06</b>
Emission Rate (lb/hr)	0.00239	0.00286	0.00393	<b>0.00306</b>
<b><u>Oxidized Mercury Results</u></b>				
Concentration Train A (µg/dscm)	2.28	2.66	1.45	<b>2.13</b>
Emission Rate (lb/mmBtu)	2.38E-06	2.74E-06	1.47E-06	<b>2.20E-06</b>
Emission Rate (lb/hr)	0.00240	0.00274	0.00144	<b>0.00219</b>
<b><u>Elemental Mercury Results</u></b>				
Concentration Train A (µg/dscm)	2.23	2.90	5.53	<b>3.55</b>
Emission Rate (lb/mmBtu)	2.32E-06	2.98E-06	5.63E-06	<b>3.65E-06</b>
Emission Rate (lb/hr)	0.00235	0.00298	0.00550	<b>0.00361</b>
<b><u>Total Mercury Results</u></b>				
Concentration Train A (µg/dscm)	6.77	8.33	10.92	<b>8.67</b>
Concentration Train B (µg/dscm)	7.60	7.97	9.88	<b>8.48</b>
Average Concentration (µg/dscm)	7.18	8.15	10.40	<b>8.58</b>
Emission Rate (lb/mmBtu)	7.50E-06	8.38E-06	1.06E-05	<b>8.82E-06</b>
Emission Rate (lb/hr)	0.00757	0.00839	0.0103	<b>0.00876</b>



**Table 3 – Summary of Inlet B HCl and HF Results**

<b><u>Test Parameters</u></b>	<b>Run 1</b>	<b>Run 2</b>	<b>Run 3</b>	<b>Average</b>
Date	7/27/11	7/27/11	7/27/11	
Start Time	7:53	11:16	14:08	
Stop Time	10:08	13:34	16:16	
Fd (dscf/mmBtu)	10,185	9,926	9,868	
<b><u>Gas Conditions</u></b>				
Temperature (°F)	304	302	302	<b>303</b>
Volumetric Flow Rate (acfm)	489,400	483,600	494,300	<b>489,100</b>
Volumetric Flow Rate (scfm)	322,700	319,700	326,900	<b>323,100</b>
Volumetric Flow Rate (dscfm)	303,400	315,800	294,900	<b>304,700</b>
Carbon Dioxide (% dry)	11.1	11.0	11.1	<b>11.1</b>
Oxygen (% dry)	8.17	8.31	8.25	<b>8.24</b>
Moisture (%)	6.02	1.27	9.84	<b>5.71</b>
<b><u>Hydrogen Chloride Results</u></b>				
Concentration (lb/dscf)	1.40E-06	1.54E-06	1.59E-06	<b>1.51E-06</b>
Concentration (ppmdv)	14.8	16.3	16.8	<b>15.9</b>
Emission Rate (lb/mmBtu)	0.0234	0.0254	0.0259	<b>0.0249</b>
Emission Rate (lb/hr)	25.4	29.2	28.1	<b>27.6</b>
<b><u>Hydrogen Fluoride Results</u></b>				
Concentration (lb/dscf)	2.58E-07	2.24E-07	2.10E-07	<b>2.31E-07</b>
Concentration (ppmdv)	4.97	4.32	4.04	<b>4.44</b>
Emission Rate (lb/mmBtu)	0.00431	0.00370	0.00342	<b>0.00381</b>
Emission Rate (lb/hr)	4.70	4.25	3.71	<b>4.22</b>

**Table 4 – Summary of Inlet B Hg Results**

<b><u>Test Parameters</u></b>	<b>Run 1</b>	<b>Run 2</b>	<b>Run 3</b>	<b>Average</b>
Date	7/27/11	7/27/11	7/27/11	
Start Time	7:53	11:16	14:08	
Stop Time	9:36	12:54	15:49	
Fd (dscf/mmBtu)	10,185	9,926	9,868	
<b><u>Gas Conditions</u></b>				
M26 Volumetric Flowrate, (dscfm)	303,400	315,800	294,900	<b>304,700</b>
M26 Oxygen (% dry)	8.17	8.31	8.25	<b>8.24</b>
M26 Moisture (%)	6.02	1.27	9.84	<b>5.71</b>
<b><u>Ash Bound Mercury Results</u></b>				
Concentration Train A (µg/dscm)	2.99	0.239	2.20	<b>1.81</b>
Emission Rate (lb/mmBtu)	3.12E-06	2.45E-07	2.24E-06	<b>1.87E-06</b>
Emission Rate (lb/hr)	0.00340	0.000282	0.00243	<b>0.00204</b>
<b><u>Oxidized Mercury Results</u></b>				
Concentration Train A (µg/dscm)	3.73	3.05	2.69	<b>3.16</b>
Emission Rate (lb/mmBtu)	3.90E-06	3.14E-06	2.74E-06	<b>3.26E-06</b>
Emission Rate (lb/hr)	0.00424	0.00361	0.00297	<b>0.00361</b>
<b><u>Elemental Mercury Results</u></b>				
Concentration Train A (µg/dscm)	4.05	4.52	4.75	<b>4.44</b>
Emission Rate (lb/mmBtu)	4.22E-06	4.65E-06	4.84E-06	<b>4.57E-06</b>
Emission Rate (lb/hr)	0.00460	0.00535	0.00525	<b>0.00507</b>
<b><u>Total Mercury Results</u></b>				
Concentration Train A (µg/dscm)	6.39	6.12	9.28	<b>7.26</b>
Concentration Train B (µg/dscm)	5.75	6.04	9.09	<b>6.96</b>
Average Concentration (µg/dscm)	6.07	6.08	9.18	<b>7.11</b>
Emission Rate (lb/mmBtu)	6.34E-06	6.25E-06	9.35E-06	<b>7.31E-06</b>
Emission Rate (lb/hr)	0.00690	0.00719	0.0101	<b>0.00808</b>

**Table 5 – Summary of the Stack Outlet FPM and CPM Results**

<b><u>Test Parameters</u></b>	<b>Run 1</b>	<b>Run 2</b>	<b>Run 3</b>	<b>Average</b>
Date	7/27/2011	7/27/2011	7/27/2011	
Start Time	7:53	11:16	14:08	
Stop Time	10:15	14:00	16:20	
Fd (dscf/mmBtu)	10,185	9,926	9,868	
<b><u>Gas Conditions</u></b>				
Temperature (°F)	130	130	128	<b>129</b>
Volumetric Flow Rate (acfm)	923,700	935,500	935,800	<b>931,700</b>
Volumetric Flow Rate (scfm)	813,100	823,800	825,900	<b>820,940</b>
Volumetric Flow Rate (dscfm)	701,100	714,700	717,500	<b>711,100</b>
Carbon Dioxide (% dry)	11.1	11.0	11.1	<b>11.1</b>
Oxygen (% dry)	8.17	8.31	8.25	<b>8.24</b>
Moisture (%)	13.8	13.3	13.2	<b>13.4</b>
<b><u>Filterable PM Results</u></b>				
Concentration (grains/dscf)	0.00407	0.00370	0.00295	<b>0.00357</b>
Emission Rate (lb/mmBtu)	0.00973	0.00871	0.00686	<b>0.00843</b>
Emission Rate (lb/hr)	24.5	22.7	18.1	<b>21.8</b>
<b><u>Condensable PM Results</u></b>				
Concentration (grains/dscf)	0.00339	0.00475	0.00601	<b>0.00472</b>
Emission Rate (lb/mmBtu)	0.00810	0.0112	0.0140	<b>0.0111</b>
Emission Rate (lb/hr)	20.4	29.1	36.9	<b>28.8</b>
<b><u>Total Particulate</u></b>				
Concentration (grains/dscf)	0.00746	0.00845	0.00895	<b>0.00829</b>
Emission Rate (lb/mmBtu)	0.0178	0.0199	0.0209	<b>0.0195</b>
Emission Rate (lb/hr)	44.9	51.8	55.1	<b>50.6</b>

**Table 6 – Summary of the Stack Outlet HCl and HF Results**

<b><u>Test Parameters</u></b>	<b>Run 1</b>	<b>Run 2</b>	<b>Run 3</b>	<b>Average</b>
Date	7/27/11	7/27/11	7/27/11	
Start Time	7:53	11:16	14:08	
Stop Time	10:15	13:35	16:20	
<b><u>Fuel Conditions</u></b>				
Fd (dscf/mmBtu)	10,185	9,926	9,868	
Chlorine (mg/kg dry)	443	451	327	
Fluorine (mg/kg dry)	82	87	84	
<b><u>Gas Conditions</u></b>				
Temperature (°F)	132	131	130	<b>131</b>
Volumetric Flow Rate (acfm)	915,000	918,900	933,200	<b>922,400</b>
Volumetric Flow Rate (scfm)	803,100	808,000	821,500	<b>810,900</b>
Volumetric Flow Rate (dscfm)	700,700	730,700	713,100	<b>714,800</b>
Carbon Dioxide (% dry)	11.1	11.0	11.1	<b>11.1</b>
Oxygen (% dry)	8.17	8.31	8.25	<b>8.24</b>
Moisture (%)	12.8	9.61	13.2	<b>11.9</b>
<b><u>Hydrogen Chloride Results</u></b>				
Concentration (lb/dscf)	1.92E-08	1.48E-08	1.71E-08	<b>1.70E-08</b>
Concentration (ppmdv)	0.203	0.156	0.181	<b>0.180</b>
Emission Rate (lb/mmBtu)	0.000322	0.000243	0.000279	<b>0.000281</b>
Emission Rate (lb/hr)	0.808	0.648	0.733	<b>0.730</b>
<b><u>Hydrogen Fluoride Results</u></b>				
Concentration (lb/dscf)	2.03E-09	1.67E-09	7.92E-10	<b>1.50E-09</b>
Concentration (ppmdv)	0.0391	0.0322	0.0152	<b>0.0289</b>
Emission Rate (lb/mmBtu)	0.0000339	0.0000276	0.0000129	<b>0.0000248</b>
Emission Rate (lb/hr)	0.0853	0.0734	0.0339	<b>0.0642</b>

**Table 7 – Summary of the Stack Outlet Metallic HAP Results**

<u>Test Parameters</u>	Run 1	Run 2	Run 3	Average
Date	7/27/11	7/27/11	7/27/11	
Start Time	7:53	11:16	14:08	
Stop Time	10:13	13:35	16:20	
<b><u>Fuel Conditions</u></b>				
F <sub>d</sub> (dscf/mmBtu)	10,185	9,926	9,868	
Antimony (mg/kg dry)	0.01	0.03	0.02	
Arsenic (mg/kg dry)	2.99	7.76	6.93	
Beryllium (mg/kg dry)	0.50	0.24	0.69	
Cadmium (mg/kg dry)	0.07	0.15	0.24	
Chromium (mg/kg dry)	3.24	6.45	5.23	
Cobalt (mg/kg dry)	1.10	1.71	1.96	
Lead (mg/kg dry)	9.74	12.97	18.33	
Manganese (mg/kg dry)	10.52	14.68	24.64	
Nickel (mg/kg dry)	4.96	4.17	9.02	
<b><u>Gas Conditions</u></b>				
Temperature (°F)	131	130	129	<b>130</b>
Volumetric Flow Rate (acfm)	973,300	1,001,800	946,100	<b>973,800</b>
Volumetric Flow Rate (scfm)	855,500	882,400	834,200	<b>857,400</b>
Volumetric Flow Rate (dscfm)	722,900	750,300	713,400	<b>728,800</b>
Carbon Dioxide (% dry)	11.1	11.0	11.1	<b>11.1</b>
Oxygen (% dry)	8.17	8.31	8.25	<b>8.24</b>
Moisture (%)	15.5	15.0	14.5	<b>15.0</b>
<b><u>Antimony - Sb</u></b>				
Concentration (ug/dscm)	0.259*	0.228*	0.357*	<b>0.282</b>
Emission Rate (lb/mmBtu)	2.71E-07*	2.35E-07*	3.64E-07*	<b>2.90E-07</b>
Emission Rate (lb/hr)	0.000703*	0.000641*	0.000955*	<b>0.000766</b>
<b><u>Arsenic - As</u></b>				
Concentration (ug/dscm)	3.94	4.34	6.19	<b>4.82</b>
Emission Rate (lb/mmBtu)	4.11E-06	4.46E-06	6.30E-06	<b>4.96E-06</b>
Emission Rate (lb/hr)	0.0107	0.0122	0.0166	<b>0.0131</b>
<b><u>Beryllium - Be</u></b>				
Concentration (ug/dscm)	0.0571*	0.0656*	0.0406*	<b>0.0544</b>
Emission Rate (lb/mmBtu)	5.96E-08*	6.75E-08*	4.13E-08*	<b>5.61E-08</b>
Emission Rate (lb/hr)	0.000155*	0.000184*	0.000109*	<b>0.000149</b>

\* indicates that a fraction of the sample was below the detection limit.

**Table 7 – Summary of the Stack Outlet Metallic HAP Results (continued)**

<u>Test Parameters</u>	Run 1	Run 2	Run 3	Average
Date	7/27/11	7/27/11	7/27/11	
Start Time	7:53	11:16	14:08	
Stop Time	10:13	13:35	16:20	
<b><u>Cadmium - Cd</u></b>				
Concentration (ug/dscm)	0.248*	0.531	0.160*	<b>0.313</b>
Emission Rate (lb/mmBtu)	2.59E-07*	5.46E-07	1.63E-07*	<b>3.23E-07</b>
Emission Rate (lb/hr)	0.000671*	0.00149	0.000429*	<b>0.000864</b>
<b><u>Chromium - Cr</u></b>				
Concentration (ug/dscm)	3.05	99.9	3.15	<b>35.4</b>
Emission Rate (lb/mmBtu)	3.18E-06	1.03E-04	3.21E-06	<b>3.64E-05</b>
Emission Rate (lb/hr)	0.00826	0.281	0.00842	<b>0.0991</b>
<b><u>Cobalt- Co</u></b>				
Concentration (ug/dscm)	0.195*	0.271*	0.149*	<b>0.205</b>
Emission Rate (lb/mmBtu)	2.04E-07*	2.78E-07*	1.52E-07*	<b>2.11E-07</b>
Emission Rate (lb/hr)	0.000529*	0.000761*	0.000398*	<b>0.000563</b>
<b><u>Lead - Pb</u></b>				
Concentration (ug/dscm)	2.55	2.68	2.64	<b>2.62</b>
Emission Rate (lb/mmBtu)	2.66E-06	2.76E-06	2.69E-06	<b>2.70E-06</b>
Emission Rate (lb/hr)	0.00690	0.0075	0.00706	<b>0.00716</b>
<b><u>Manganese - Mn</u></b>				
Concentration (ug/dscm)	7.20	6.98	6.19	<b>6.79</b>
Emission Rate (lb/mmBtu)	7.52E-06	7.18E-06	6.30E-06	<b>7.00E-06</b>
Emission Rate (lb/hr)	0.0195	0.0196	0.0166	<b>0.0186</b>
<b><u>Nickel - Ni</u></b>				
Concentration (ug/dscm)	2.31	7.34	2.16	<b>3.94</b>
Emission Rate (lb/mmBtu)	2.42E-06	7.55E-06	2.20E-06	<b>4.06E-06</b>
Emission Rate (lb/hr)	0.00627	0.0206	0.00579	<b>0.0109</b>
<b><u>Selenium - Se</u></b>				
Concentration (ug/dscm)	43.1	27.3	30.2	<b>33.5</b>
Emission Rate (lb/mmBtu)	4.50E-05	2.81E-05	3.08E-05	<b>3.46E-05</b>
Emission Rate (lb/hr)	0.117	0.0767	0.0808	<b>0.0914</b>

\*indicates that one fraction of the sample was below the detection limit.

**Table 8 – Summary of the Stack Outlet Hg Results**

<b><u>Test Parameters</u></b>	<b>Run 1</b>	<b>Run 2</b>	<b>Run 3</b>	<b>Average</b>
Date	7/27/11	7/27/11	7/27/11	
Start Time	7:53	11:16	14:08	
Stop Time	10:13	13:35	15:41	
<b><u>Fuel Conditions</u></b>				
Fd (dscf/mmBtu)	10,185	9,926	9,868	
Mercury (mg/kg dry)	0.159	0.204	0.159	
<b><u>Gas Conditions</u></b>				
M29 Volumetric Flowrate, (dscfm)	723,100	750,100	713,700	<b>729,000</b>
M29 Oxygen (% dry)	8.17	8.31	8.25	<b>8.24</b>
M29 Moisture (%)	15.5	15.0	14.5	<b>15.0</b>
<b><u>Oxidized Mercury Results</u></b>				
Concentration Train A (µg/dscm)	0.448	0.335	0.248	<b>0.344</b>
Emission Rate (lb/mmBtu)	4.67E-07	3.44E-07	2.53E-07	<b>3.55E-07</b>
Emission Rate (lb/hr)	0.00121	0.000941	0.000663	<b>0.000939</b>
<b><u>Elemental Mercury Results</u></b>				
Concentration Train A (µg/dscm)	2.04	2.69	3.23	<b>2.66</b>
Emission Rate (lb/mmBtu)	2.13E-06	2.77E-06	3.29E-06	<b>2.73E-06</b>
Emission Rate (lb/hr)	0.00553	0.00757	0.00863	<b>0.00725</b>
<b><u>Total Mercury Results</u></b>				
Concentration Train A (µg/dscm)	2.49	3.03	3.47	<b>3.00</b>
Concentration Train B (µg/dscm)	2.01	3.22	3.27	<b>2.84</b>
Average Concentration (µg/dscm)	2.25	3.13	3.37	<b>2.92</b>
Emission Rate (lb/mmBtu)	2.32E-06	3.09E-06	3.36E-06	<b>2.93E-06</b>
Emission Rate (lb/hr)	0.00610	0.00878	0.00901	<b>0.00797</b>

## Test Procedures

### Method Listing

The test methods found in 40 CFR Part 60, Appendix A and 40 CFR Part 51, Appendix M were referenced during the test program. The following individual methods were used:

EPA Method 1	Sample and Velocity Traverse for Stationary Sources
EPA Method 2	Determination of Stack Gas Velocity and Volumetric Flow Rate (Type S pitot tube)
EPA Method 3	Gas analysis for the Determination of Dry Molecular Weight
EPA Method 4	Determination of Moisture Content in Stack Gases
EPA Method 5B	Determination of Non-Sulfuric Acid Particulate Matter Emissions from Stationary Sources
EPA Method 19	Determination of Sulfur Dioxide Removal Efficiency and Particulate Matter, Sulfur Dioxide, and Nitrogen Oxides Emission Rates
EPA Method 26	Determination of Hydrogen Halide and Halogen Emissions from Stationary Sources – Non-isokinetic Method
EPA Method 26A	Determination of Hydrogen Halide and Halogen Emissions from Stationary Sources - Isokinetic Method
EPA Method 29	Determination of Metals Emissions from Stationary Sources
EPA Method 30B	Determination of Total Vapor Phase Mercury Emissions from Coal-Fired Combustion Sources Using Carbon Sorbent Traps
EPA Method 202	Dry Impinger Method for Determining Condensable Particulate Emissions from Stationary Sources

### Method Descriptions

#### *Method 1*

Method 1 was used to determine the suitability of each ESP and the Stack test location and to determine the sample points used for the isokinetic pollutant concentration determinations. The Stack Outlet test location conformed to the minimum requirements of being located at least 2.0 diameters downstream and at least 0.5 diameters upstream from the nearest flow disturbance. The ESP test locations did not meet Method 1 requirements.



The Inlet A test location was a rectangular, horizontal stack with dimensions of 162 inches by 198 inches. Thirteen points were sampled in each of two test ports for the Method 26A determinations. A cross section of the sampling location, showing the sample points, can be found in Figure 1 of the Appendix.

The Inlet B test location was a rectangular, horizontal stack with dimensions of 162 inches by 198 inches. Thirteen points were sampled in each of two test ports for the Method 26A determinations. A cross section of the sampling location, showing the sample points, can be found in Figure 2 of the Appendix.

The Stack Outlet test location was a round, vertical stack with a diameter of 180 inches. Three points were sampled for each of the four test ports. The test location was located approximately 16.7 diameters downstream and approximately 6.7 diameters upstream from the nearest flow disturbance. A cross section of the sampling location, showing the sample points, can be found in Figure 3 of the Appendix.

### ***Method 2***

Method 2 was used to determine the gas velocity through each test location using a Type-S pitot tube and an incline plane oil manometer. The values measured in Method 2, along with the measurements made in Methods 3 and 4, were used to calculate the volumetric flow rate through the test location. A diagram of the Method 2 apparatus is shown as part of the Methods 5B/202, 26A and 29 sampling trains in Figure 3, 4 and 5 of the Appendix.

The manometer was leveled and “zeroed” prior to each test run. The sample train was leak checked before and after each run by pressurizing the positive side, or “high” side, of the pitot tube and creating a deflection on the manometer of at least three inches H<sub>2</sub>O. The leak check was considered valid if the manometer remained stable for 15 seconds. This procedure was repeated on the negative side by generating a vacuum of at least three inches H<sub>2</sub>O. The velocity head pressure and gas temperature were then determined at each point specified in Method 1. The static pressure of the stack was measured using a water filled U-tube manometer. In addition, the barometric pressure was measured and recorded.

### ***Method 3***

The carbon dioxide and oxygen content of the sample gas was determined at each test location using Method 3. A gas sample was collected into a Tedlar bag from the dry gas meter exhaust of the Method 5B sampling train for the duration of each test run. Analysis was performed using an Orsat gas analyzer.

The gas analyzer was leak checked prior to analysis by raising the liquid levels in each pipette to a reference mark on the capillary tubes and then closing the pipette valves. The burette solution was then raised to bring the meniscus onto the graduated portion of the burette and the manifold valve was closed. After four minutes, the pipette meniscus did not fall below the reference mark and the burette meniscus did not fall by more than 0.2

percent, so the leak check was considered valid. The average of three gas analyses determined the carbon dioxide and oxygen contents.

The carbon dioxide content and oxygen content were used, along with the moisture content determined in Method 4, to calculate the gas stream molecular weight. The molecular weight was then used for the volumetric flow rate calculation. For these calculations, the balance of the gas stream was assumed to consist of nitrogen since other gas stream components are insignificant for the purposes of calculating molecular weight.

#### ***Method 4***

The moisture content at each test location was determined using EPA Method 4 in conjunction with the Methods 5B/202, 26, 26A and 29 test runs. A known volume of sample gas was withdrawn from each source and the moisture was condensed and measured. The dry standard volume of the sample gas was then compared to the volume of moisture collected to determine the moisture content of the sample gas. A diagram of the Method 4 apparatus is shown as part of the Methods 5B/202, 26A and 29 sampling trains in Figure 3, 4 and 5 of the Appendix.

To condense the water vapor the gas sample passed through a series of impingers. The impingers were charged as outlined in each individual method. In all trains, the last impinger contained a known weight of silica gel to absorb any residual water vapor.

After the test run the sample train was leak checked at the highest vacuum encountered during the test run. The amount of water collected in the condenser system and the silica gel weight gain was determined gravimetrically. The net weight gain of water was converted to a volume of wet gas and then compared to the amount of dry gas sampled to determine the moisture content. The moisture content was used, along with the oxygen and carbon dioxide content determined by EPA Method 3, for the calculation of the volumetric flow rate.

#### ***Method 5B/202***

The PM concentrations were determined using EPA Methods 5B/202. In EPA Methods 5B/202, a sample of the gas stream was withdrawn isokinetically from the test location. Non-sulfuric PM was collected in the nozzle, probe, connecting glassware and filter. CPM in the sample gas passed through the filter and collected in a gas condenser system. The weight of non-sulfuric FPM and CPM collected with the sample train combined with the volume of dry gas withdrawn from the stack was then used to calculate PM concentrations. A diagram of the Method 5B/202 sampling train is shown in Figure 3 of the Appendix.

To prevent contamination, all components of the sample trains were constructed of glass with no metal connections. Prior to testing all the components of the Method 5B sampling train were cleaned using detergent and then rinsed with tap water, deionized water and lastly with acetone. For the Method 202 sampling train all the components were cleaned using detergent and then rinsed with tap water, deionized water, acetone and

lastly with hexane. After drying, all components were sealed with parafilm or Teflon tape.

The Method 5B portion of the sampling train consisted of a glass nozzle, a glass (or Teflon) lined sample probe and a glass fiber filter. The probe and filter were maintained at a temperature of 320°F (+/- 25°F).

After exiting the Method 5B portion of the sampling system, the sample gas passed through an EPA Method 23 type glass coil condenser and then through a series of four (4) glass impingers. The condenser was cooled with a water recirculation pump that was placed in a water bath. The recirculation pump and coiled condenser are used to maintain the gas temperature between 65°F and 85°F at the exit of the CPM filter. Impingers 1 and 2 were initially empty. A Teflon fiber CPM filter followed impinger 2. Impinger 3 contained 100ml of water. The fourth impinger contained a known mass of silica gel to absorb any remaining water vapor. The dry gas exiting the moisture condenser system then passed through a sample pump and a dry gas meter to measure the gas volume. After leaving the dry gas meter the sample stream passed through an orifice which was used to meter the flow rate through the sample train. The pressure drop across the orifice was measured with an incline plane oil manometer.

Whatman 934-AH glass fiber filters were used as the substrate for the non-sulfuric PM sampling. The filter was loaded into a glass filter holder with a Teflon support screen that was cleaned and prepared in the same manner as the other components of the Method 5B sample train. Prior to the test run, the filter was baked at 320°F (+/- 25°F) for a minimum of two (2) hours then desiccated for at least 24 hours and then weighed to the nearest 0.0001gram (g) until a constant weight was achieved. The weight of the filter was considered to be constant when two consecutive weights taken at least six hours apart were within 0.0005g of each other.

The probe liner was thoroughly pre-cleaned with acetone and the probe wash was saved as a quality assurance check. The sample train was leak checked prior to the test run by capping the probe tip and pulling a vacuum of at least 15 inches Hg. A leak test was considered valid if the leak rate was below 0.02 cfm. When not in operation or inside the stack, the nozzle was sealed with Teflon tape.

The probe tip was placed at the first of the sample points determined in Method 1. The velocity at the sample point was determined using Method 2 by reading the velocity pressure from the oil manometer. Sample was withdrawn from the source at a rate such that the velocity at the opening of the nozzle matches the velocity of the stack gas at the sample point (isokinetically). During the test run the train was moved to each of the Method 1 sample points. The sample time at each point was calculated based on the number of sample points and the run time. The gas velocity pressure, gas meter reading, gas meter inlet and outlet temperatures, gas meter orifice pressure and pump vacuum were recorded for each sample point.

After the test run the sample train was leak checked at the highest vacuum encountered during the test run. The sampling train was moved to the on-site lab and purged with zero grade nitrogen at a nominal flow rate of at least 14 liters per minute for a period of 60 minutes. The nozzle, probe and front half of the filter holder were washed with acetone and the rinse saved in a 250ml glass jar equipped with a Teflon lid. The glass fiber filter was removed from the filter holder, transferred to a Petri dish and sealed.

Upon completion of the purge, the contents of impingers one and two were transferred to a pre-cleaned 950 ml sample jar equipped with a Teflon lid. The condenser coil and all connecting glassware up to and including the front half of the CPM filter were rinsed twice with deionized ultra filtered (DUIF) water and added to the sample jar. An acetone rinse of the above glassware was performed and saved in a separate pre-cleaned 500ml sample jar equipped with a Teflon lid. Finally, two (2) rinses of the above components were performed with hexane and added to the acetone container. The CPM filter was removed from the filter holder and placed in a 20ml glass sample jar.

Analysis of all sample fractions was performed at the Airtech laboratory located in Bensenville, Illinois. The acetone rinses from the Method 5B portion of the sampling train were transferred to tared beakers, evaporated to dryness under ambient temperature and pressure conditions, baked for six (6) hours, desiccated for 24 hours and weighed to a constant weight. A weight was considered constant when the difference between two consecutive weights, taken a minimum of six hours apart, was less than or equal to 0.0005 grams. The weight gain of the probe rinses and glass fiber filter yield the total weight of filterable non-sulfuric acid particulate collected during sampling.

Inorganic extraction of the CPM filter was performed by placing the filter into an extraction tube with DIUF water and placing it into a sonication bath for a minimum of 2 minutes. This extraction was done a total of 3 times and the water used each time was added to the impinger water container. After inorganic extraction of the CPM filter, an organic extraction of the impinger water was performed. The entire contents of the impinger water sample fraction were placed in a separatory funnel. A 30 ml aliquot of Hexane was added to the funnel and the funnel contents were thoroughly mixed. The organic layer was then allowed to separate from the water and was decanted from the funnel into the acetone and hexane sample jar. This procedure was conducted three (3) times to complete the extraction.

The inorganic contents of the separatory funnel were then transferred into a beaker and evaporated down to not less than 10 ml final volume at an elevated temperature. The remaining liquid was evaporated to dryness at ambient temperature. The beaker was desiccated for 24 hours and then weighed to a constant weight.

Organic CPM extraction of the filter was performed by placing the inorganic extracted filter into an extraction tube with hexane and placing it into a sonication bath for a minimum of 2 minutes. This extraction was done a total of 3 times and the hexane used

was added to the acetone/hexane container. The contents of this container was transferred into a beaker and evaporated to not less than 10 ml. The remaining fraction was then evaporated to dryness at ambient temperature and pressure. The tin was desiccated for 24 hours and then weighed to a constant weight.

The weight differences for the organic and inorganic fractions were combined to determine the total condensible particulate collected. All fractions of the CPM analysis were adjusted for the appropriate blank values.

### ***Method 19***

The equations in EPA Method 19 were used to calculate the emission rates of various pollutants from the test location in units of pounds per million British thermal units (lb/mmBtu). The calculation was based on the oxygen content of the sample gas and an appropriate F factor, which is the ratio of combustion gas volumes to heat inputs.

### ***Method 26A***

EPA Method 26A was used to determine the concentrations of HCl and HF at the Inlets and the Stack Outlet test locations. A sample of the gas stream was withdrawn isokinetically from the stack through a probe, a Teflon mat filter and a series of glass impingers charged with an H<sub>2</sub>SO<sub>4</sub> solution. After each test run, the solution was recovered and analyzed using ion chromatography (IC). The total mass of each target constituent collected, combined with the volume of dry gas withdrawn from the test location was then used to calculate the in-stack concentration of each target constituent. A diagram of the sampling system may be found in Figure 4 of the Appendix.

To prevent contamination, all components of the sample train were constructed of glass or Teflon with no metal connections. Prior to testing the components were cleaned using detergent and then rinsed with tap water, deionized water and lastly with acetone. After drying, all components will be sealed with parafilm or Teflon tape.

The sample probe consisted of a heated liner and glass nozzle. Sample gas passed through the nozzle and probe assembly and then through a heated Teflon fiber filter. All heated components of the sampling train were maintained at a temperature of at least 248°F. After exiting the filter, the sample gas passed through a series of four glass impingers. The first and second impingers each contained 100ml of a dilute sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) solution. The third impinger was initially empty. The fourth impinger contained a mass of silica gel to absorb any residual water vapor. After exiting the impinger system, the gas stream passed through a sample pump and into a dry gas meter, where the gas volume was measured. After leaving the dry gas meter, the sample stream passed through an orifice that was used to meter the flow rate through the sample train. The pressure drop across the orifice was measured with an incline oil manometer.

The sampling train was assembled and leak checked prior to the test run. The leak check was performed by capping the probe nozzle and pulling a vacuum greater than the highest

vacuum expected during the test run. A leak check was considered valid if the leak rate was below 0.02 cubic feet per minute.

The probe tip was then placed at the first of the sample points determined in Method 1. The velocity at the sample point was determined using Method 2 by reading the velocity pressure from the oil manometer. Sample was withdrawn from the source at a rate such that the velocity in the nozzle matched the velocity of the stack gas at the sample point (isokinetically). During the test run the train was moved to each of the Method 1 sample points. The sample time at each point was calculated based on the number of sample points and the run time. Each test run was 120 minutes in duration such that a minimum sample volume of 2.5 dscm was collected. The gas velocity pressure, gas meter reading, gas meter inlet and outlet temperatures, gas meter orifice pressure and pump vacuum were recorded for each sample point.

After the test run the train was leak checked at the highest vacuum encountered during the test run. The impinger contents were recovered and stored in a 500ml high density, polyethylene sample jar. The impingers were rinsed three (3) times each with 0.1N H<sub>2</sub>SO<sub>4</sub> with the rinses added to the sample jar. The resulting samples (including all rinses) were analyzed for HCl and HF using ion chromatography. Analysis for HCl and HF was performed at the Airtech laboratory located in Denver, Colorado.

### ***Method 29***

EPA Method 29 was used to determine the concentration of metallic hazardous air pollutants (HAP) at each test location. Metallic HAPs include antimony (Sb), arsenic (As), beryllium (Be), cadmium (Cd), chromium (Cr), cobalt (Co), lead (Pb), manganese (Mn), nickel (Ni) and selenium (Se). In EPA Method 29, sample gas was withdrawn isokinetically from the test location and the Metallic HAPs in the sample gas was collected in a glass lined probe, on a quartz fiber filter and in a series of chilled impingers charged with a metals absorbing solution. The mass of Metallic HAPs collected with the sample train, combined with the volume of dry gas withdrawn from the test location was then used to calculate the concentration of each Metallic HAPs. A diagram of the sampling system may be found in Figure 5 of the Appendix.

To prevent contamination, all components of the sample train were glass or Teflon with no metal connections. Prior to testing, the components were washed using detergent and then rinsed with tap water and rinsed again with deionized water. All glassware was soaked for a minimum of four (4) hours in a ten percent (10%) nitric acid (HNO<sub>3</sub>) solution. After soaking, the glassware was rinsed with de-ionized, ultra filtered (DIUF) water and finally with acetone. After drying, all components were sealed with parafilm.

The sample probe consisted of a heated glass liner and glass nozzle. Sample gas passed through the nozzle, the probe assembly, and then through a heated quartz fiber filter. The probe and filter were maintained at 248°F (+/- 25°F). After exiting the filter, the sample gas passed through a series of five glass impingers. The first impinge was initially empty. The second and third impingers were each loaded with 100ml of a 5 percent HNO<sub>3</sub>/10

percent H<sub>2</sub>O<sub>2</sub> solution. The fourth impinger was initially empty. The fifth impinger contained a known quantity of silica gel to absorb any residual water vapor. After exiting the impingers, the gas stream passed through a sample pump and into a dry gas meter, where the gas volume was measured. After leaving the dry gas meter, the sample stream passed through an orifice that was used to meter the flow rate through the sample train. The pressure drop across the orifice was measured with an incline oil manometer.

Prior to the test run, the probe was thoroughly cleaned with acetone and a 0.1 N nitric acid solution and the probe washes saved as a quality assurance check. The sampling train was then assembled and leak checked by capping the probe nozzle and pulling a vacuum greater than the highest vacuum expected during the test run. A leak check was considered valid if the leak rate was below 0.02 cubic feet per minute.

The probe tip was then placed at the first of the sample points determined in Method 1. The velocity at the sample point was determined using Method 2 by reading the velocity pressure from the oil manometer. Sample was withdrawn from the source at a rate such that the velocity in the nozzle matched the velocity of the stack gas at the sample point (isokinetically). During the test run the train was moved to each of the Method 1 sample points. The sample time at each point was calculated based on the number of sample points and the run time. Each test run was 120 minutes in duration. The gas velocity pressure, gas meter reading, gas meter inlet and outlet temperatures, gas meter orifice pressure and pump vacuum were recorded for each sample point.

After sampling, the sample train was transferred to the on-site laboratory for recovery. The filter was removed from the holder and placed in a glass petri dish. The front half of the sample train consisting of the nozzle, probe liner and filter holder inlet half was brushed with a non-metallic brush and rinsed with 0.1 N HNO<sub>3</sub>. These rinses were saved in separate 250ml trace clean amber glass sample jars. The contents of the first four impingers were recovered and saved in a 500ml Nalgene sample jar. The impingers and the filter outlet half were then rinsed with 0.1N HNO<sub>3</sub>, and the rinses added to the impinger sample jar. The contents of the fifth (silica gel) impinger was weighed for moisture weight gain and discarded.

The 0.1N HNO<sub>3</sub> front half rinse and filter were digested with HNO<sub>3</sub>. This fraction and the sample fraction acquired from the first three impingers were analyzed separately for all the metals listed using ICP and GFAA. Analysis of the samples was conducted by ElementOne located in Wilmington, North Carolina.

### ***Method 30B***

EPA Method 30B was used to determine the concentration of mercury at each test location. In EPA Method 30B, a sample of the effluent was withdrawn from the test location at a constant rate through an in-situ, glass 10 ml trap. The trap contained multiple stages of sorbent media designed to adsorb both Hg<sup>2+</sup> and Hg<sup>0</sup> forms of vapor-phase mercury. A coil pre-filter preceded the sorbent media sections and collected particle bound mercury. The masses of mercury species collected with the traps was

compared to the volume of dry gas sampled to calculate the various mercury concentrations. A diagram of the sampling system may be found in Figure 6 of the Appendix.

The sample traps for the Method 30B apparatus were quartz in construction. Traps were fitted to the end of the probe and contained in a steel heater block assembly designed to both prevent moisture condensation in the trap as well as provide for a constant temperature during sample collection. Sample gas passed through the trap and probe assembly, then through a condenser system comprised of a series of glass impingers. After exiting the condenser system, the sample gas passed through a metering system to determine the dry volume of gas sampled.

The volume of dry gas exiting the gas condenser system was measured with a dry gas meter. After leaving the dry gas meter the sample stream passed through an orifice, which was used to meter the flow rate through the sample train. The pressure drop across the orifice was measured with an incline plane oil manometer. The gas meter reading, gas meter temperatures, gas meter static pressure and pump vacuum were recorded every five minutes during each test run.

The sample train was leak checked prior to the test run by capping the trap tip and pulling a vacuum greater than the highest vacuum expected during the test run. A leak check was considered valid if the leak rate was less than four (4) percent of the average sampling rate. Sample gas was then withdrawn from the source at a constant rate such that the predetermined sample volume was collected. After the test run the probe was removed from the stack and the sample train was leak checked at the highest vacuum encountered during the test run.

Each test run consisted of a paired set of adsorbent tubes, one spiked with a known mass of Hg and the other unspiked. The spiked tube was a standard Method 30B sampling tube packed with carbon. The unspiked tube contained proprietary sections of adsorbent media designed to collect the different species of mercury separately. A coil pre-filter collected particle bound mercury. This was followed by two sections of adsorbent media designed to catch oxidized, vapor phase mercury. These sections were followed by two additional sections of adsorbent media designed to catch elemental, vapor phase mercury. All tube sections were analyzed separately using an Ohio Lumex, Model RA-915+ mercury analyzer. Quality assurance for the sample trains included spike recoveries, breakthrough checks and duplicate sample agreement. It should be noted that both spike recoveries and duplicate agreement QA is based on total mercury only.

Analysis of the samples was performed at the Airtech Laboratory located in Denver, Colorado. Results for mercury are expressed in units of pounds per million British thermal units (lbs/mmBtu) and pounds per hour (lb/hr).