

Sample Calculations, ESP Unit 1, Method 5B/202, Run 1

Area of Sample Location

$$A_s = \pi \times \left(\frac{d_s}{2 \times 12} \right)^2$$

$$A_s = \pi \times \left(\frac{132}{2 \times 12} \right)^2$$

$$A_s = 95.0 \text{ ft}^2$$

where:

- A_s = area of sample location (ft²)
- d_s = diameter of sample location (in)
- 12 = conversion factor (in/ft)
- 2 = conversion factor (diameter to radius)

Stack Pressure Absolute

$$P_a = P_b + \frac{P_s}{13.6}$$

$$P_a = 28.90 + \frac{-2.0}{13.6}$$

$$P_a = 28.75 \text{ in. Hg}$$

where:

- P_a = stack pressure absolute (in. Hg)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure (in. H₂O)
- 13.6 = conversion factor (in. H₂O/in. Hg)

Volume of Dry Gas Collected Corrected to Standard Temperature and Pressure

$$V_{m(std)} = \frac{17.64(V_m)(Y_d)\left(P_b + \frac{\Delta H}{13.6}\right)}{(T_m + 460)}$$
$$V_{m(std)} = \frac{17.64(54.83)(0.9904)\left(28.90 + \frac{1.24}{13.6}\right)}{(80.3 + 460)}$$
$$V_{m(std)} = 51.40scf$$

where:

$V_{m(std)}$	= volume of gas collected at standard temperature and pressure (scf)
V_m	= volume of gas sampled at meter conditions (ft ³)
Y_d	= gas meter correction factor (dimensionless)
P_b	= barometric pressure (in. Hg)
ΔH	= average sample pressure (in. H ₂ O)
T_m	= average gas meter temperature (°F)
13.6	= conversion factor (in. H ₂ O/in. Hg)
17.64	= ratio of standard temperature over standard pressure (°R/in. Hg)
460	= conversion (°F to °R)

Volume of Water Vapor Collected Corrected to Standard Temperature and Pressure

$$V_{w(std)} = 0.04715 \times (V_{wc} + V_{wsg})$$
$$V_{w(std)} = 0.04715 \times (51.0 + 34.0)$$
$$V_{w(std)} = 4.01scf$$

where:

$V_{w(std)}$	= volume of water vapor at standard conditions (scf)
V_{wc}	= weight of liquid collected (g)
V_{wsg}	= weight gain of silica gel (g)
0.04715	= volume occupied by one gram of water at standard temperature and pressure (ft ³ /g)

Percent Moisture²

$$B_{ws} = 100 \times \left[\frac{V_{w(std)}}{(V_{m(std)} + V_{w(std)})} \right]$$

$$B_{ws} = 100 \times \left[\frac{4.01}{(51.40 + 4.01)} \right]$$

$$B_{ws} = 7.23\%$$

where:

- B_{ws} = moisture content of the gas stream (%)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- $V_{w(std)}$ = volume of water vapor at standard conditions (scf)
- 100 = conversion factor

Molecular Weight of Dry Gas Stream³

$$M_d = \left(44 \times \frac{\%CO_2}{100} \right) + \left(32 \times \frac{\%O_2}{100} \right) + \left(28 \times \frac{(\%N_2)}{100} \right)$$

$$M_d = \left(44 \times \frac{12.0}{100} \right) + \left(32 \times \frac{7.28}{100} \right) + \left(28 \times \frac{(80.7)}{100} \right)$$

$$M_d = 30.21 \text{ lb} / \text{lbmole}$$

where:

- M_d = molecular weight of the dry gas stream (lb/lb-mole)
- $\%CO_2$ = carbon dioxide content of the dry gas stream (%)
- 44 = molecular weight of carbon dioxide (lb/lb-mole)
- $\%O_2$ = oxygen content of the dry gas stream (%)
- 32 = molecular weight of oxygen (lb/lb-mole)
- $\%N_2$ = nitrogen content of the dry gas stream (%)
- 28 = molecular weight of nitrogen and carbon monoxide (lb/lb-mole)
- 100 = conversion factor

² The moisture saturation point is used for all calculations if it is exceeded by the actual moisture content.

³ The remainder of the gas stream after subtracting carbon dioxide and oxygen is assumed to be nitrogen.

Molecular Weight of Wet Gas Stream

$$M_s = \left(M_d \times \left(1 - \frac{B_{ws}}{100} \right) \right) + \left(18 \times \frac{B_{ws}}{100} \right)$$

$$M_s = \left(30.21 \times \left(1 - \frac{7.23}{100} \right) \right) + \left(18 \times \frac{7.23}{100} \right)$$

$$M_s = 29.33 \text{ lb / lbmole}$$

where:

- M_s = molecular weight of the wet gas stream (lb/lb-mole)
- M_d = molecular weight of the dry gas stream (lb/lb-mole)
- B_{ws} = moisture content of the gas stream (%)
- 18 = molecular weight of water (lb/lb-mole)
- 100 = conversion factor

Velocity of Gas Stream

$$V_s = 85.49(C_p)(\sqrt{\Delta P}) \sqrt{\frac{(T_s + 460)}{(M_s) \left(P_b + \frac{P_s}{13.6} \right)}}$$

$$V_s = 85.49(0.84)(0.879) \sqrt{\frac{(324 + 460)}{(29.33) \left(28.90 + \frac{-2.0}{13.6} \right)}}$$

$$V_s = 60.9 \text{ ft / sec}$$

where:

- V_s = average velocity of the gas stream (ft/sec)
- C_p = pitot tube coefficient dimensionless
- $\sqrt{\Delta P}$ = average square root of velocity pressures (in. H₂O)^{1/2}
- T_s = average stack temperature (°F)
- M_s = molecular weight of the wet gas stream (lb/lb-mole)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure of gas stream (in. H₂O)
- 85.49 = pitot tube constant (ft/sec)/[(lb/lb-mole)(in. Hg)]/[(°R)(in. H₂O)]^{1.2}
- 460 = conversion (°F to °R)
- 13.6 = conversion factor (in. H₂O/in. Hg)

Volumetric Flow of Gas Stream - Actual Conditions

$$Q_a = 60(V_s)(A_s)$$

$$Q_a = 60(60.9)(95.0)$$

$$Q_a = 347,156 \text{ acfm}$$

where:

Q_a = volumetric flow rate of the gas stream at actual conditions (acfm)

V_s = average velocity of the gas stream (ft/sec)

A_s = area of duct or stack (ft²)

60 = conversion factor (min/hr)

Volumetric Flow of Gas Stream - Standard Conditions

$$Q_{std} = \frac{17.64(Q_a) \left(P_b + \frac{P_s}{13.6} \right)}{(T_s + 460)}$$

$$Q_{std} = \frac{17.64(347,156) \left(28.90 + \frac{-2.0}{13.6} \right)}{(324 + 460)}$$

$$Q_{std} = 224,494 \text{ scfm}$$

where:

Q_{std} = volumetric flow rate of the gas stream at standard conditions (scfm)

Q_a = volumetric flow rate of the gas stream at actual conditions (acfm)

T_s = average stack temperature (°F)

P_b = barometric pressure (in. Hg)

P_s = static pressure of gas stream (in. H₂O)

13.6 = conversion factor (in. H₂O/in. Hg)

17.64 = ratio of standard temperature over standard pressure (°R/in. Hg)

460 = conversion (°F to °R)

Volumetric Flow of Gas Stream - Standard Conditions - Dry Basis

$$Q_{dstd} = Q_{std} \left(1 - \frac{B_{ws}}{100} \right)$$

$$Q_{dstd} = 224,494 \left(1 - \frac{7.23}{100} \right)$$

$$Q_{dstd} = 208,339 \text{ dscfm}$$

where:

- Q_{dstd} = volumetric flow rate of the gas stream at standard conditions, on a dry basis (dscfm)
- Q_{std} = volumetric flow rate of the gas stream at standard conditions (scfm)
- B_{ws} = moisture content of the gas stream (%)
- 100 = conversion factor

Area of Nozzle

$$A_n = \pi \times \left(\frac{d_n}{2 \times 12} \right)^2$$

$$A_n = \pi \times \left(\frac{0.220}{2 \times 12} \right)^2$$

$$A_n = 0.000264 \text{ ft}^2$$

where:

- A_n = area of nozzle (ft²)
- d_n = diameter of nozzle (in)
- 12 = conversion factor (in/ft)
- 2 = conversion factor (diameter to radius)

Percent Isokinetic

$$I = \frac{0.0945(T_s + 460)(V_{m(std)})}{\left(P_b + \frac{P_s}{13.6}\right)(v_s)(A_n)(\Theta)\left(1 - \frac{B_{ws}}{100}\right)}$$

$$I = \frac{0.0945(324 + 460)(51.40)}{\left(28.90 + \frac{-2.0}{13.6}\right)(60.9)(2.64 \times 10^{-4})(90)\left(1 - \frac{7.23}{100}\right)}$$

$$I = 98.7\%$$

where:

I	= percent isokinetic (%)
T _s	= average stack temperature (°F)
V _{m(std)}	= volume of gas collected at standard temperature and pressure (scf)
P _b	= barometric pressure (in. Hg)
P _s	= static pressure of gas stream (in. H ₂ O)
V _s	= average velocity of the gas stream (ft/sec)
A _n	= cross sectional area of nozzle (ft ²)
Θ	= sample time (min)
B _{ws}	= moisture content of the gas stream (%)
0.0945	= constant (°R/in. Hg)
460	= conversion (°F to °R)
13.6	= conversion factor (in. H ₂ O/in Hg)
100	= conversion factor

Acetone Wash Blank-Particulate

$$W_a = \frac{(m_{ab})(v_{aw})}{v_{awb}}$$

$$W_a = \frac{(0.0000)(120)}{200}$$

$$W_a = 0.0000g$$

where:

- W_a = particulate mass in acetone wash, blank corrected (g)
- m_{ab} = mass collected, acetone wash blank (g)
- v_{aw} = volume of acetone wash (ml)
- v_{awb} = volume of acetone wash blank (ml)

Mass in Front Half, Acetone Blank Corrected

$$m_f = m_{fl} + (m_a - W_a)$$

$$m_f = 0.3531 + (0.1324 - 0.0000)$$

$$m_f = 0.4854g$$

where:

- m_f = mass in front half filter, and acetone wash, blank corrected (g)
- m_{fl} = mass in front half filter (g)
- m_a = mass in acetone wash (g)
- W_a = particulate mass in acetone wash blank (g)

Total Particulate Catch

$$M_n = m_f + m_b$$

$$M_n = 0.4854 + 0.0379$$

$$M_n = 0.5234g$$

where:

- M_n = total mass catch (g)
- m_f = mass in front half filter, and acetone wash, blank corrected (g)
- m_b = mass in back half organic fraction, and inorganic fraction, blank corrected (g)

Total Particulate Concentration, grains/dscf

$$C_{gr/dscf} = \frac{(M_n)(15.43)}{V_{m,std}}$$

$$C_{gr/dscf} = \frac{(0.5234)(15.43)}{51.40}$$

$$C_{gr/dscf} = 0.157 \text{ grains / dscf}$$

where:

- $C_{gr/dscf}$ = particulate concentration (grains/dscf)
- M_n = total particulate catch (g)
- $V_{m(std)}$ = volume of gas collected at standard conditions (scf)
- 15.43 = conversion factor (grains/g)

Calculated F_d Factor, dscf/mmBtu

$$F_d = K((K_{hd} \times H) + (K_c \times C) + (K_s \times S) + (K_n \times N) - (K_o \times O_2)) / GCV_w$$

$$F_d = 10^6 ((3.64 \times 4.90) + (1.53 \times 73.11) + (0.57 \times 2.93) + (0.14 \times 1.58) - (0.46 \times 9.09)) / 13,028$$

$$F_d = 9,779$$

where:

- F_d = calculated fuel factor (dscf/mmBtu)
- K = conversion factor (Btu/million Btu)
- K_{hd} = constant (scf/lb)
- H = weight percent hydrogen in coal (%)
- K_c = constant (scf/lb)
- C = weight percent carbon in coal (%)
- K_s = constant (scf/lb)
- S = weight percent sulfur in coal (%)
- K_n = constant (scf/lb)
- N = weight percent nitrogen in coal (%)
- K_o = constant (scf/lb)
- O_2 = weight percent oxygen in coal (%)
- GCV_w = gross calorific value of fuel, wet (Btu/lb)

Total Particulate Emission Rate, lb/mmBtu ⁴

$$E_{PM} = \frac{(M_n)(F_d)(20.9)}{(V_{m(std)})(453.6)(20.9 - O_2)}$$

$$E_{PM} = \frac{(0.5234)(9,779)(20.9)}{(51.40)(453.6)(20.9 - 7.28)}$$

$$E_{PM} = 0.337 \text{ lb / mmBtu}$$

where:

E_{PM} = total particulate matter emission rate, (lb/mmBtu)

M_n = total particulate catch (g)

F_d = fuel factor (dcsf/mmBtu)

20.9 = oxygen content of ambient air (%)

$V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)

453.6 = conversion factor (g/lb)

% O_2 = oxygen content of the dry gas stream (%)

Total Particulate Emission Rate, lb/hr

$$E_{lb/hr} = \frac{(M_n)(Q_{dstd})(60)}{(V_{m,std})(453.6)}$$

$$E_{lb/hr} = \frac{(0.5234)(208,339)(60)}{(51.40)(453.6)}$$

$$E_{lb/hr} = 281 \text{ lb / hr}$$

where:

$E_{lb/hr}$ = particulate emission rate (lb/hr)

M_n = total particulate catch (g)

$V_{m(std)}$ = volume of gas collected at standard conditions (scf)

Q_{dstd} = volumetric flow rate of the dry gas stream at standard conditions (dscfm)

60 = conversion factor (min/hr)

453.6 = conversion factor (g/lb)

⁴ All particulate emission rates are calculated in a similar manner.

Sample Calculations, Method 26, Run 1

Concentration of Hydrogen Chloride in Flue Gas (lb/dscf)⁵

$$C_{HCl} = \frac{(M_{HCl})}{(V_{m(std)})(10^3)(453.6)}$$

$$C_{HCl} = \frac{(242)}{(120.67)(10^3)(453.6)}$$

$$C_{HCl} = 4.42 \times 10^{-6} \text{ lb / dscf}$$

where:

- C_{HCl} = concentration of hydrogen chloride in flue gas (lb/dscf)
- M_{HCl} = mass of hydrogen chloride collected in sample (mg)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 10^3 = conversion factor (mg/g)
- 453.6 = conversion factor (g/lb)

Concentration of Hydrogen Chloride in Flue Gas (ppmv)⁵

$$C_{ppmv} = \frac{(M_{HCl})(385.3)(10^6)}{(MW_{HCl})(V_{m(std)})(10^3)(453.6)}$$

$$C_{ppmv} = \frac{(242)(385.3)(10^6)}{(36.458)(120.67)(10^3)(453.6)}$$

$$C_{ppmv} = 46.7 \text{ ppmv}$$

where:

- C_{ppmv} = concentration of hydrogen chloride in flue gas (ppmv)
- M_{HCl} = mass of hydrogen chloride collected in sample (mg)
- 385.3 = volume occupied by one pound gas at standard conditions (dscf/lbmole)
- 10^6 = conversion factor (fraction to ppm)
- MW_{HCl} = molecular weight of hydrogen chloride (lb/lb-mole)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 10^3 = conversion factor (mg/g)
- 453.6 = conversion factor (g/lb)

⁵ The concentration of HF is calculated in a similar manner.

Hydrogen Chloride Emission Rate, lb/mmBtu⁶

$$E_{HCl} = \frac{(C_{HCl})(F_d)(20.9)}{(20.9 - O_2)}$$

$$E_{HCl} = \frac{(4.42 \times 10^{-6})(9,808)(20.9)}{(20.9 - 7.28)}$$

$$E_{HCl} = 0.0665 \text{ lb / mmBtu}$$

where:

- E_{HCl} = hydrogen chloride emission rate, (lb/mmBtu)
- C_{HCl} = hydrogen chloride concentration, (lb/dscf)
- F_d = fuel factor (dcsf/mmBtu)
- 20.9 = oxygen content of ambient air (%)
- % O_2 = oxygen content of the dry gas stream (%)

Hydrogen Chloride Emission Rate⁶

$$E_{HCl} = C_{HCl} \times Q_{dstd} \times 60$$

$$E_{HCl} = 4.42 \times 10^{-6} \times 193,099 \times 60$$

$$E_{HCl} = 51.2 \text{ lb / hr}$$

where:

- E_{HCl} = hydrogen chloride emission rate, (lb/hr)
- C_{HCl} = hydrogen chloride concentration, (lb/dscf)
- Q_{dstd} = volumetric flow rate of the dry gas stream at standard conditions (dscfm)
- MW = molecular weight of hydrogen chloride (lb/lbmole)
- 60 = conversion factor (min/hr)
- 385.3 = volume occupied by one pound gas at standard conditions (dscf/lbmole)
- 10^6 = conversion factor (fraction to ppm)

⁶ The emission rate of HF is calculated in a similar manner.

Sample Calculations, Method 29, Run 1

Concentration of Lead in Flue Gas, ug/dscm⁷

$$C_{ug/dscm} = \frac{(M_C)}{(V_{m(std)})} (35.31)$$

$$C_{ug/dscm} = \frac{(28.4)}{(63.85)} (35.31)$$

$$C_{ug/dscm} = 15.7 \text{ ug / dscm}$$

where:

- $C_{ug/dscm}$ = concentration of lead in flue gas (ug/dscm)
- M_C = mass of lead in sample (ug)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 35.31 = conversion factor (ft³/m³)

Emission Rate of Lead in Flue Gas, lb/mmBtu⁸

$$E = \frac{(C_{ug/dscm})(F_d)(20.9)}{(35.31)(20.9 - \%O_2)(453.6)(10^6)}$$

$$E = \frac{(15.7)(9,808)(20.9)}{(35.31)(20.9 - 7.28)(453.6)(10^6)}$$

$$E = 1.48 \times 10^{-5} \text{ mg / dscm@7\%O}_2$$

where:

- E = lead emission rate (lb/mmBtu)
- $C_{ug/dscm}$ = lead concentration (ug/dscm)
- F_d = fuel factor (dcsf/mmBtu)
- 35.31 = conversion factor (ft³/m³)
- 20.9 = oxygen content of ambient air (%)
- $\%O_2$ = oxygen content of the dry gas stream (%)
- 453.6 = conversion factor (g/lb)
- 10^6 = conversion factor (ug/g)

⁷ The concentrations of all MHs and mercury are calculated in a similar manner.

⁸ The emission rates of all MHs and mercury are calculated in a similar manner.

Lead Emission Rate, lb/hr

$$E_{lb/hr} = \frac{(C_{ug/dscm})(Q_{dstd})(60)}{(35.31)(10^6)(453.6)}$$

$$E_{lb/hr} = \frac{(15.7)(208,870)(60)}{(35.31)(10^6)(453.6)}$$

$$E_{lb/hr} = 0.0123 lb/hr$$

where:

- $E_{lb/hr}$ = lead emission rate (lb/hr)
- $C_{ug/dscm}$ = lead concentration (ug/dscm)
- Q_{dstd} = volumetric flow rate of dry gas stream at standard conditions (dscfm)
- 10^6 = conversion factor (ug/g)
- 35.31 = conversion factor (ft^3/m^3)
- 60.0 = conversion factor (min/hr)
- 453.6 = conversion factor (g/lb)