COMMONWEALTH OF KENTUCKY

BEFORE THE PUBLIC SERVICE COMMISSION

In the Matter of:

The Electronic Application of Duke Energy) Kentucky, Inc. for a Certificate of Public) Convenience and Necessity to Convert its Wet Flue) Gas Desulfurization System from a Quicklime Reagent Process to a Limestone Reagent Handling) System at its East Bend Generating Station and for) Approval to Amend its Environmental Compliance) Plan for Recovery by Environmental Surcharge) Mechanism)

Case No. 2024-00152

APPLICATION OF DUKE ENERGY KENTUCKY, INC.

Now comes Duke Energy Kentucky, Inc. (Duke Energy Kentucky or the Company), by and through counsel, pursuant to KRS 278.020(1), KRS 278.183, and 807 KAR 5:001 Sections 14 and 15, and hereby respectfully requests the Kentucky Public Service Commission (Commission) to issue an Order approving: (1) a Certificate of Public Convenience and Necessity (CPCN) for the construction and conversion of its existing Wet Flue Gas Desulfurization (WFGD) from a quicklime handling process to a limestone handling process to continue to meet existing environmental regulations (Limestone Conversion Project); (2) amendment of the Company's Environmental Compliance Plan (ECP) to include the Limestone Conversion Project construction and operation, and reagents; (3) recovery of the Limestone Conversion Project costs through the Company' Environmental Surcharge Mechanism (ESM); and (4) any other necessary relief and approvals. In support of this Application, Duke Energy Kentucky states as follows:

Introduction

1. Duke Energy Kentucky is a Kentucky corporation with its principal office and

principal place of business at 139 East Fourth Street, Cincinnati, Ohio 45202. The Company's local office in Kentucky is Duke Energy Erlanger Operations Center, 1262 Cox Road, Erlanger, Kentucky 41018. The Company further states that its electronic mail address for purposes of this matter is <u>KYfilings@duke-energy.com</u>.

2. Duke Energy Kentucky is a utility engaged in the gas and electric business. Duke Energy Kentucky purchases, sells, stores and transports natural gas in the Boone, Bracken, Campbell, Gallatin, Grant, Kenton, and Pendleton Counties. Duke Energy Kentucky also generates electricity, which it distributes and sells, in the Boone, Campbell, Grant, Kenton, and Pendleton Counties.

3. Pursuant to 807 KAR 5:001, Section 14(2), Duke Energy Kentucky states that it was originally incorporated in the Commonwealth of Kentucky on March 20, 1901, and attests that it is currently in good standing in said Commonwealth. A copy of a certificate of good standing is included as Exhibit 1 to this Application.

4. Pursuant to KRS 278.380, Duke Energy Kentucky waives any right to service of Commission orders by mail for purposes of this proceeding only. Copies of all orders, pleadings, and other communications related to this proceeding should be directed to:

Rocco O. D'Ascenzo Deputy General Counsel Duke Energy Kentucky, Inc. 139 East Fourth Street Cincinnati, OH 45202 rocco.d'ascenzo@duke-energy.com

Larisa Vaysman Associate General Counsel Duke Energy Kentucky, Inc. 139 East Fourth Street Cincinnati, OH 45202 Larisa.vaysman@duke-energy.com

and

Sarah E. Lawler Vice President, Rates and Regulatory Strategy Ohio/Kentucky Duke Energy Kentucky, Inc. 139 East Fourth Street Cincinnati, OH 45202 sarah.lawler@duke-energy.com

Background

5. On or about December 5, 2003, in Case No. 2003-00252, the Commission approved Duke Energy Kentucky's acquisition of three generating stations from Duke Energy Ohio; East Bend Unit 2 (East Bend), Miami Fort Unit 6 and Woodsdale. Effective January 1, 2006, Duke Energy Kentucky completed the acquisition of these three generating stations. Effective December 31, 2014, Duke Energy Kentucky became the sole owner of East Bend, having completed the purchase of The Dayton Power and Light Company's 31 percent interest in the station as authorized by the Commission in Case No. 2014-00201.¹

6. East Bend is a 600 megawatt (MW) (net summer rating) coal-fired steam unit located along the Ohio River in Boone County, Kentucky, which was commissioned in 1981. East Bend is the Company's only baseload and coal-fired generator, providing the majority of the capacity to serve the Company's Northern Kentucky load.

7. There are several environmental programs promulgated by the United States Environmental Protection Agency (U.S. EPA) under the Clean Air Act (CAA) as well as the Commonwealth of Kentucky, that impact all of the Company's generating stations, and

¹ In the Matter of the Application of Duke Energy Kentucky, Inc., for (1) A Certificate of Public Convenience and Necessity Authorizing the Acquisition of the Dayton Power & Light Company's 31% Interest in the East Bend Generating Station; (2) Approval of Duke Energy Kentucky, Inc.'s Assumption of Certain Liabilities in Connection with the Acquisition; (3) Deferral of Costs Incurred as Part of the Acquisition; and (4) All Other Necessary Waivers, Approvals, and Relief, Case No. 2014-00201 (Ky.P.S.C. Dec. 4, 2014).

particularly East Bend. The U.S. EPA regulations are the primary drivers of Duke Energy Kentucky's environmental compliance strategies for its plants. These CAA regulations are as follows: the Mercury and Air Toxics Standard (MATS Rule) and the Cross State Air Pollution Rule (CSAPR) including the U.S. EPA's September 2016 final CSAPR Update Rule. The regulations that most directly impact the Company's ash handling strategy as it pertains to East Bend are the CAA and the CCR Final Rule and ELG Final Rule

8. The major pollution control features at East Bend include a high-efficiency hot side electrostatic precipitator, a selective catalytic reduction control (SCR) system designed to reduce nitrogen oxide (NO_x) emissions by 85 percent, and a WFGD system designed to remove sulfur dioxide (SO₂) emissions to an average of 97 percent. The WFGD currently utilizes a magnesium enhanced lime (MEL) technology to control the station's SO₂ emissions. This MEL technology is unique to the 1980's vintage WFGD and is the only one of its kind within the Duke Energy fleet of coal-fired generation.

9. The MEL technology relies on pebble quicklime containing a small fraction of dolomite as the reagent. Dolomite is comprised of about 50% magnesium oxide which, when added to the absorber with the lime reagent, dissolves and promotes elevated concentrations of sulfite. Sulfite is an effective source of liquid-phase alkalinity, which facilitates high SO₂ removal efficiency for boilers firing high sulfur coal. The primary benefit of scrubbing with MEL is that the required absorber recycle slurry pumping capacity is lower than limestone-based FGD systems – typically in the range of 40 to 50 gallons per 1,000 cubic feet of treated flue gas – and results in smaller pumps with lower power requirements

10. Despite some process advantages, MEL scrubbing has several disadvantages including the production of calcium sulfite (CaSO₃) solids that are typically difficult to dewater.

As a result, significant quantities of fly ash and lime must be added to the filtered solids to produce a stable product, called poz-o-tec, that is suitable for disposal in an onsite landfill. Another disadvantage of the MEL scrubbing process is the reliance on an expensive lime reagent – quicklime, and stabilization additives which in recent years, has detrimentally impacted East Bend's competitiveness in the power generation markets.

11. At the time of its construction, and in years past, the cost of the quicklime was reasonable and was a popular choice for SO₂ removal in the Ohio River Valley. In the early 1980s, when the system at East Bend was designed, the cost of lime was modest; delivered prices were about \$40 per ton. Since then, the price for delivered quicklime has risen dramatically to well over \$100 per ton. The approximate cost at East Bend in 2022 was \$133 per ton. However, with many Midwest power plants retiring or converting to lower cost reagents such as limestone, the availability of supply, number of suppliers, and quality of MEL has been adversely impacted creating exponential increasing costs and risks to the future availability of supply. A request for proposal (RFP) issued in mid-2023 produced a lime cost per ton that is more than double that paid in 2022. East Bend has experienced a 247 percent increase in the mag-lime reagent cost over the last 10 years and a 125 percent increase in in the last two years. Due to the energy intensity to produce the MEL reagent product, the Company expects the reagent to continually escalate at a rate double that of limestone.

12. Duke Energy Kentucky has recently been made aware of additional limitations to MEL supply leading to material cost increases and a risk in availability of supply alternatives creating future availability concerns.

13. If Duke Energy Kentucky is unable to procure the reagents necessary to operate its WFGD, the Company will not be able to comply with the aforementioned environmental

regulations or continue operating East Bend in compliance and would likely be forced to retire the plant prematurely. The reagent supply scarcity and associated price risks for Duke Energy Kentucky must be addressed to continue providing cost-effective, safe and reliable service to our Kentucky customers.

14. The increase in current lime-based reagent costs negatively impacts the dispatch costs for East Bend. As the cost for the existing lime process continues to escalate, the value of the unit in the wholesale market continues to diminish and its capacity factor decreases. This results in Duke Energy Kentucky purchasing more economy power from the market and not generating itself.

15. To address the rising cost of the quicklime reagent, and the risk of an inability to operate the unit absent a viable reagent replacement, Duke Energy Kentucky's fuel sourcing organization has explored several alternatives, including 1) the Lime Stone Conversion project; 2) conducting requests for proposals (RFP) to explore alternative sources for the existing MEL product with the correct chemical composition to operate the WFGD system; and 3) system renovations for onsite mixing of magnesium hydroxide with hi-calcium quicklime to create a replacement mag-lime product that possesses similar chemical composition to operate the existing WFGD system.

16. An RFP alternative is not a viable solution going forward as in its most recent solicitation, the Company did not receive competitive offers, which resulted in significant cost increases.

17. The onsite mixing of chemicals with high-calcium quicklime was a more expensive alternative as it would require the Company to purchase significant amounts of magnesium hydroxide to meet the correct chemical content specifications to operate the WFGD increasing the

Company's reagent costs and further eroding the unit's economics in the competitive markets. Moreover, this strategy did not alleviate the scarcity risk with obtaining a lime-based reagent product. Because this solution does not sufficiently mitigate the risk of a lack of certainty of reagent supplies it was not a reasonable and viable solution.

18. The conversion of the WFGD to a limestone inhibited oxidation process (LSIO) is the most economic and most reasonable solution. The LSIO chemistry will improve the dewatering properties of the calcium sulfite solids by creating larger, more regular, and symmetric crystals and provide a lower cost alternative for reagents going forward. This proposed Limestone Conversion Project process should result in lower reagent costs than the current mag-lime-based process, which in turn should provide downward pressure on East Bend's total dispatch cost in the wholesale energy markets and should result in an increased capacity factor.

19. The Limestone Conversion Project scope includes modifications to existing equipment and is based on a turnkey delivery, including engineering, procurement, and construction. The conversion of the East Bend WFGD system to LSIO operation involves several process, equipment, and system changes including:

- a. Minor modifications to reagent receiving, conveying, and storage systems;
- b. Installation of new reagent feeders and conveying equipment;
- c. Installation of new limestone pre-crushers and grinding mills;
- d. Refurbishment and resheaving of absorber recycle pumps
- e. Installation of new absorber recycle slurry piping, cross-tie piping, spray headers, and spray nozzles;
- f. Operation of all absorber recycle slurry pumps to enhance SO₂ removal performance;
- g. Modification of the absorber trays to enhance SO₂ removal performance;
- h. Installation of a buffer additive storage and feed system to enhance SO₂ removal performance;
- i. Replacement of existing emulsified sulfur storage tank and fees system to improve system reliability and inhibit sulfite oxidation

- j. Upgrade of mist eliminator wash water supply system;
- k. Replacement of waste slurry storage tank, thickener underflow sludge tank and lime slurry tank agitators; and
- 1. Installation of a filtrate purge system to control process chloride levels.

Modeling shows that conversion to a LSIO- limestone reagent process is economic in most future scenarios and produces a reduced variable operational cost and lower dispatch cost reducing the Company's reliance upon market purchases for power. Although the Limestone Conversion Project will likely result in a higher overall reagent expenditure due to the anticipated increased economic dispatch of the plant necessitating a greater need and consumption of the limestone reagent, the cost per ton of reagent is anticipated to be significantly lower due to the Limestone Conversion Project. The current class 4 estimated capital cost for the project is approximately \$125.8 million. As explained in accompanying testimony, the conversion would reduce total variable operating and maintenance and produce estimated benefits to customers in terms of fuel cost savings and additional off system sales revenues as compared to continuing the existing processes. This increased economics of East Bend is a benefit to customers as it will likely reduce the need for replacement power from the market.

Request for Certificate of Public Convenience and Necessity

20. Duke Energy Kentucky requests Commission authorization through a CPCN to construct the Limestone Conversion Project.

21. In accordance with KRS 278.020, No utility may construct or acquire any facility to be used in providing utility service to the public until it has obtained a CPCN from the Kentucky Public Service Commission.² To obtain a CPCN, the utility must demonstrate a need for such facilities and an absence of wasteful duplication.³ "Need" requires:

² KRS 278.020(1)(a).

³ Kentucky Utilities Co. v. Pub. Serv. Comm 'n, 252 S.W.2d 885 (Ky. 1952).

[A] showing of a substantial inadequacy of existing service, involving a consumer market sufficiently large to make it economically feasible for the new system or facility to be constructed or operated. [T]he inadequacy must be due either to a substantial deficiency of service facilities, beyond what could be supplied by normal improvements in the ordinary course of business; or to indifference, poor management or disregard of the rights of consumers, persisting over such a period of time as to establish an inability or unwillingness to render adequate service.⁴

"Wasteful duplication" is defined as "an excess of capacity over need" and "an excessive investment in relation to productivity or efficiency, and an unnecessary multiplicity of physical properties."⁵ To demonstrate that a proposed facility does not result in wasteful duplication, Duke Energy Kentucky must demonstrate that a thorough review of all reasonable alternatives has been performed. Although cost is a factor, selection of a proposal that ultimately costs more than an alternative does not necessarily result in wasteful duplication.⁶ All relevant factors must be balanced.⁷

⁴ *Id*. at 890.

⁵ Id.

⁶ See Kentucky Utilities Co. v. Pub. Serv. Comm'n, 390 S.W.2d 168, 175 (Ky. 1965). See also Case No. 2005-00089, Application of East Kentucky Power Cooperative, Inc. for a Certificate of Public Convenience and Necessity for the Construction of a 138 kV Electric Transmission Line in Rowan County, Kentucky (Ky. PSC Aug. 19, 2005), final Order

⁷ Case No. 2005-00142, Joint Application of Louisville Gas and Electric Company and Kentucky Utilities Company for a Certificate of Public Convenience and Necessity for the Construction of Transmission Facilities in Jefferson, Bullitt, Meade, and Hardin Counties, Kentucky (Ky. PSC Sept. 8, 2005).

22. In accordance with 807 KAR 5:001 Section 12(2)(a)-(i), Duke Energy Kentucky is filing the following financial information in Exhibit 2, which is incorporated herein and made a part of this Application filed in this proceeding:

Exhibit 2	Description 807	KAR 5:001
<u>Page</u>	Section Ref	ference
	Financial Exhibit	12(2)
1	Amount and kinds of stock authorized	12(2)(a)
1	Amount and kinds of stock issued and outstanding	12(2)(b)
1	Terms of preference or preferred stock	12(2)(c)
1	Brief description of each mortgage on property of Duke Energy Kentucky	12(2)(d)
1-2	Amount of bonds authorized and issued and related information	12(2)(e)
2	Notes outstanding and related information	12(2)(f)
2-3	Other indebtedness and related information	12(2)(g)
3	Dividend information	12(2)(h)
3-5	Detailed Income Statement and Balance Sheet	12(2)(i)

construction or extension are set forth in 807 KAR 5:001 § 14 and 15(2) *et seq.*, and include the following requirements:

Additionally, requirements for Applications requesting a CPCN related to a new

Section 14:

23.

- (1) Each application shall state the full name, mailing address, and electronic mail address of the applicant, and shall contain fully the facts on which the application is based, with a request for the order, authorization, permission, or certificate desired and a reference to the particular law requiring or providing for the information.
- (2) If a corporation, the applicant shall identify in the application the state in which it is incorporated and the date of its incorporation, attest that it is currently in good standing in the state in which it is incorporated, and, if it is not a Kentucky corporation, state if it is authorized to transact business in Kentucky.⁸

⁸ 807 KAR 1:005 § 14; Sub sections 2 and 4 are inapplicable as Duke Energy Kentucky is a Kentucky Corporation.

Section 15(2):

- (a) The facts relied upon to show that the proposed construction or extension is or will be required by public convenience or necessity;
- (b) Copies of franchises or permits, if any, from the proper public authority for the proposed construction or extension, if not previously filed with the commission;
- (c) A full description of the proposed location, route, or routes of the proposed construction or extension, including a description of the manner of the construction and the names of all public utilities, corporations, or persons with whom the proposed construction or extension is likely to compete;
- (d) One (1) copy in portable document format on electronic storage medium and two (2) copies in paper medium of:

1. Maps to suitable scale showing the location or route of the proposed construction or extension, as well as the location to scale of like facilities owned by others located anywhere within the map area with adequate identification as to the ownership of the other facilities; and

2. Plans and specifications and drawings of the proposed plant, equipment, and facilities;

- (e) The manner in detail in which the applicant proposes to finance the proposed construction or extension; and
- (f) An estimated annual cost of operation after the proposed facilities are placed into service.
- 24. Section 14- Name, Address, electronic mail address of Applicant, facts upon which

the Application is based, and reference to the particular law: See paragraphs 1 through 23 above, which are incorporated by reference as if fully restated herein.

25. <u>Section 15(2)(a)- Statement of Need:</u> The facts relied upon to demonstrate the

Limestone Conversion Project is required by public convenience and necessity are set forth within this Application and in the Testimony submitted in support thereof. In summary, the existing reagent process needed to operate the Company's East Bend WFGD is insufficient to continue its operation due to unreasonable and uncontrollable increases in reagent prices, a lack of competitive RFP responses, scarcity of supply and an overall risk of an inability to comply and continue operating the station if a suitable replacement is not timely implemented. Duke Energy Kentucky has explored several alternative strategies and has determined that the Limestone Conversion Project is the least-cost and most reasonable solution to continue complying with Federal environmental regulations, including the CAA.

26. <u>Section 15(2)(b)- Copies of Franchises and Permits:</u> The Company has previously filed with the Commission the applicable franchises from the proper public authorities. In addition, because much of the existing equipment will be used as part of the Limestone Conversion, only minor air source permit modifications will be necessary to construct the Limestone Conversion Project. A copy of the minor air source permit application, submitted on July 17, 2012 is attached as Exhibit 3.

27. Section 15(2)(c)- <u>Description of the Proposed Location, Manner of Construction,</u> <u>and Competing Utilities, Companies, or Persons</u>: Exhibit 4 contains maps of the East Bend facility and depicts the approximate location of the Limestone Conversion construction. Exhibit 3 further contains a description of how the construction will occur. Additionally, the direct testimony accompanying this Application further describes the manner of construction. This project will be constructed on the existing East Bend site, which is owned by Duke Energy Kentucky and will be used by the Company to continue to meet environmental regulations impacting the operation of the East Bend station. Consequently, there are no other utilities, persons or corporations competing with the proposed facilities to be constructed.

28. <u>Section 15(2)(d)- Maps and Specifications</u>: Exhibit 3 includes overhead maps of the site showing the location of the East Landfill and closure construction. Exhibit 4 includes the design plans, specifications, and drawings of the East Landfill closure.

29. <u>Section 15(2)(e)- Manner of Proposed Financing</u>: the Company states that the total, fully loaded projected costs for Limestone Conversion Project is \$125.8million, including contingency and escalation. Duke Energy Kentucky seeks to recover these costs through its ESM

as part of its ECP. Duke Energy Kentucky expects to finance the costs of construction with a combination of new debt and equity and through ongoing operations. The mix of debt and equity used to finance the project will be determined so as to allow Duke Energy Kentucky to maintain its investment-grade credit rating.

30. <u>Section 15(2)(f)- Ongoing Cost of Operation</u>: The estimated incremental ongoing costs of operation, will be minimal (<\$10,000 per year, excluding the reagent commodity.

<u>Request for Recovery by Environmental Surcharge and to Amend Duke Energy</u> <u>Kentucky's Environmental Compliance Plan.</u>

31. Duke Energy Kentucky is seeking Commission authorization to amend its Environmental Compliance Plan, (ECP) to include the construction, operation and maintenance of the Limestone Conversion Project as well as the associated reagents. This conversion will enable Duke Energy Kentucky to continue operation of East Bend in compliance with applicable environmental regulations, including but not limited to, the U.S. EPA CAA, MATS, and CSAPR, as well as other environmental regulations.

32. Duke Kentucky's ESM and ECP are governed by KRS 278.183 which provides in relevant part:

(1) . . . [A] utility shall be entitled to the current recovery of its costs of complying with the Federal Clean Air Act as amended and those federal, state, or local environmental requirements which apply to coal combustion wastes and by-products from facilities utilized for production of energy from coal in accordance with the utility's compliance plan . . .

(2) Recovery of costs pursuant to subsection (1) of this section that are not already included in existing rates shall be by environmental surcharge to existing rates imposed as a positive or negative adjustment to customer bills in the

second month following the month in which costs are incurred. Each utility, before initially imposing an environmental surcharge pursuant to this subsection, shall thirty (30) days in advance file a notice of intent to file said plan and subsequently submit to the commission a plan, including any application required by KRS 278.020(1), for complying with the applicable environmental requirements set forth in subsection (1) of this section. The plan shall include the utility's testimony concerning a reasonable return on compliance-related capital expenditures and a tariff addition containing the terms and conditions of a proposed surcharge as applied to individual rate classes. Within six (6) months of submittal, the commission shall conduct a hearing upon the request of a party, and shall, regardless of whether or not a hearing is requested:

(a) Consider and approve the plan and rate surcharge if the commission finds the plan and rate surcharge reasonable and cost-effective for compliance with the applicable environmental requirements set forth in subsection (1) of this section;

(b) Establish a reasonable return on compliance-related capital expenditures; and

(c) Approve the application of the surcharge.

Duke Energy Kentucky submits that the CPCN is necessary to comply with existing environmental regulations affecting its coal-fired generation. The Company is entitled to amend its ECP and ESM because: 1) the need for this Limestone Conversion Project CPCN arises from the need to continue complying with environmental regulations applicable to coal combustion generating facilities and the current method is experiencing and will continue to experience significant price increases and there is a serious risk that the existing reagent process will no longer be able to function due to resource scarcity; 2) the costs of construction and operation of this Limestone Conversion Project CPCN are not already included in existing rates; and 3) the ECP and ESM are reasonable and cost-effective as it results in a lower cost for customers and avoids the risk of not having access to necessary reagents and premature plant closure.

33. This Application and supporting testimony and exhibits are available for public inspection at Duke Energy Kentucky's local Kentucky office located at Duke Energy Erlanger Operations Center, 1262 Cox Road, Erlanger, Kentucky 41018. The Company is giving notice to the public of the proposal to recover the Limestone Conversion Project through its existing environmental surcharge by newspaper publication. The Company is also posting this Application on its website at www.duke-energy.com. An initial Certificate of Notice and Publication is filed with this Application as Exhibit 5. A Certification of Completed Notice and Publication will be filed with the Commission upon completion of same pursuant to 807 KAR 5:001, Section 17(3)(b).

34. Pursuant to KRS 278.183(1), Duke Energy Kentucky is "entitled to the current recovery of its costs of complying with the Federal Clean Air Act as amended and those federal, state, or local environmental requirements which apply to coal combustion wastes and byproducts from facilities utilized for production of energy from coal in accordance with the utility's compliance plan."

35. A detailed summary of the facts and compliance requirements supporting this Application is set forth in the direct testimony and exhibits of the Company's witnesses:

36. The testimony of John A. Verderame, Vice President of Fuels and Systems Optimization, who discusses the need and justification of the Limestone Conversion Project, alternatives considered, and why the Limestone Conversion Project is the least cost and most reasonable solution;

37. The testimony of Chad M. Donner, Project Manager, describes the engineering and construction aspects of the Limestone Conversion Project and the estimated costs;

38. The testimony of J. Michael Geers, P.E., Manager Environmental Services, discusses the environmental regulations that necessitate the Limestone Conversion Project; and

39. The testimony of Sarah E. Lawler, Vice President, Rates and Regulatory Strategy for Ohio/ Kentucky provides an overview of the estimated impact of the Limestone Conversion on Rider ESM, the recovery of the cost of construction and ongoing operation and maintenance, the requested ROE as authorized by the Commission in the Company's most recent electric base rate case proceeding and the estimated monthly bill impact for residential and non-residential customers.

40. Duke Energy Kentucky proposed Environmental Surcharge Mechanism tariff sheet, K.Y.P.S.C. No. 19, Sheet No. 76 is attached as Exhibit 6 to this Application, and reflects changes the issue and effective dates and to include the Limestone Conversion Project and the new limestone reagent. In accordance with KRS 278.183(2), the ESM tariff has an issue date of July 25, 2024, and is proposed to be effective on August 25, 2024, to begin recovery of construction activities following Commission approval of the requested CPCN. The Company projects that bills issued following Commission approval will reflect the revised environmental surcharge.

WHEREFORE, Duke Energy Kentucky respectfully requests the Kentucky Public Service Commission to enter an order: 1) granting Duke Energy Kentucky a Certificate of Public Convenience and Necessity to construct, operate and maintain its Limestone Conversion Project; 2) approving the amendment to Duke Energy Kentucky's ECP to include the construction and operation of the Limestone Conversion Project and associated reagents; 3) approving the proposed ESM tariff for recovery of the costs of for bills rendered following Commission approval; 4)

recovery of the overall ROE requested herein; and 5) granting such other relief as Duke Energy

Kentucky may be entitled under the law.

Respectfully submitted,

DUKE ENERGY KENTUCKY, INC.

/s/ Rocco O. D'Ascenzo Rocco O. D'Ascenzo (92796) Deputy General Counsel Duke Energy Business Services LLC 139 East Fourth Street, 1303-Main Cincinnati, Ohio 45201-0960 Phone: (513) 287-4320 Fax: (513) 287-4385 E-mail: rocco.d'ascenzo@duke-energy.com

CERTIFICATE OF SERVICE

This is to certify that the foregoing electronic filing is a true and accurate copy of the document being filed in paper medium; that the electronic filing was transmitted to the Commission on July 25 2024; and that there are currently no parties that the Commission has excused from participation by electronic means in this proceeding.

John G. Horne, II The Office of the Attorney General Utility Intervention and Rate Division 700 Capital Avenue, Ste 118 Frankfort, Kentucky 40601

> /s/Rocco D'Ascenzo Rocco D'Ascenzo

Commonwealth of Kentucky Michael G. Adams, Secretary of State

Michael G. Adams Secretary of State P. O. Box 718 Frankfort, KY 40602-0718 (502) 564-3490 http://www.sos.ky.gov

Certificate of Existence

Authentication number: 316232

Visit <u>https://web.sos.ky.gov/ftshow/certvalidate.aspx</u> to authenticate this certificate.

I, Michael G. Adams, Secretary of State of the Commonwealth of Kentucky, do hereby certify that according to the records in the Office of the Secretary of State,

DUKE ENERGY KENTUCKY, INC.

DUKE ENERGY KENTUCKY, INC. is a corporation duly incorporated and existing under KRS Chapter 14A and KRS Chapter 271B, whose date of incorporation is March 20, 1901 and whose period of duration is perpetual.

I further certify that all fees and penalties owed to the Secretary of State have been paid; that Articles of Dissolution have not been filed; and that the most recent annual report required by KRS 14A.6-010 has been delivered to the Secretary of State.

IN WITNESS WHEREOF, I have hereunto set my hand and affixed my Official Seal at Frankfort, Kentucky, this 25th day of July, 2024, in the 233rd year of the Commonwealth.



Michael & adam

Michael G. Adams Secretary of State Commonwealth of Kentucky 316232/0052929

FINANCIAL EXHIBIT

(1) <u>Section 12(2)(a) Amount and kinds of stock authorized.</u>

1,000,000 shares of Capital Stock \$15 par value amounting to \$15,000,000 par value.

(2) <u>Section 12(2)(b) Amount and kinds of stock issued and outstanding.</u>

585,333 shares of Capital Stock \$15 par value amounting to \$8,779,995 total par value. Total Capital Stock and Additional Paid-in Capital as of May 31, 2024:

Capital Stock and Additional Paid-in Capital As of May 31, 2024 (\$ per 1,000)

Capital Stock	\$8,780
Premiums thereon	18,839
Total Capital Contributions from Parent (since 2006)	334,311
Contribution from Parent Company for Purchase of Generation Assets	140,061
Total Capital Stock and Additional Paid-in-Capital	<u>\$501,991</u>

(3) <u>Section 12(2)(c) Terms of preference or preferred stock, cumulative or participating, or on dividends or assets or otherwise.</u>

There is no preferred stock authorized, issued or outstanding.

(4) <u>Section 12(2)(d) Brief description of each mortgage on property of applicant,</u> giving date of execution, name of mortgagor, name or mortgagee, or trustee, <u>amount of indebtedness authorized to be secured, and the amount of indebtedness</u> <u>actually secured, together with any sinking fund provision</u>.

Duke Energy Kentucky does not have any liabilities secured by a mortgage.

(5) <u>Section 12(2)(e) Amount of bonds authorized, and amount issued, giving the name</u> of the public utility which issued the same, describing each class separately, and giving the date of issue, face value, rate of interest, date of maturity and how secured, together with the amount of interest paid thereon during the last fiscal year.

The Company has thirteen outstanding issues of unsecured senior debentures issued under an Indenture dated December 1, 2004, between itself and Deutsche Bank Trust Company Americas, as Trustee, as supplemented by eight Supplemental Indentures. The Indenture

Supplemental	Date of	Principal Amount	Principal	Rate of	Date of	Interest Paid
Indenture	Issue	Authorized and Issued	Outstanding	Interest	Maturity	Year 2023
1 st Supplemental	3/7/2006	65,000,000	65,000,000	6.20%	3/10/2036	4,030,000
3 rd Supplemental	1/5/2016	45,000,000	45,000,000	3.42%	1/15/2026	1,539,000
3 rd Supplemental	1/5/2016	50,000,000	50,000,000	4.45%	1/15/2046	2,225,000
4 th Supplemental	9/7/2017	30,000,000	30,000,000	3.35%	9/15/2029	1,005,000
4 th Supplemental	9/7/2017	30,000,000	30,000,000	4.11%	9/15/2047	1,233,000
4 th Supplemental	9/7/2017	30,000,000	30,000,000	4.26%	9/15/2057	1,278,000
5 th Supplemental	10/3/2018	40,000,000	40,000,000	4.18%	10/15/2028	1,672,000
5 th Supplemental	12/12/2018	35,000,000	35,000,000	4.62%	12/15/2048	1,617,000
6 th Supplemental	7/17/2019	40,000,000	40,000,000	4.32%	7/15/2049	1,728,000
7 th Supplemental	9/15/2019	95,000,000	95,000,000	3.23%	10/1/2025	3,068,500
7 th Supplemental	9/15/2019	75,000,000	75,000,000	3.56%	10/1/2029	2,670,000
8 th Supplemental	9/15/2020	35,000,000	35,000,000	2.65%	9/15/2030	927,500
8 th Supplemental	9/15/2020	35,000,000	35,000,000	3.66%	9/15/2050	1,281,000
			605,000,000			24,274,000

allows the Company to issue debt securities in an unlimited amount from time to time. The Debentures issued and outstanding under the Indenture are the following:

(6) <u>Section 12(2)(f) Each note outstanding, giving date of issue, amount, date of maturity, rate of interest, in whose favor, together with amount of interest paid thereon during the last fiscal year.</u>

Duke Energy Kentucky does not have any outstanding notes as of 5/31/2024.

(7) <u>Section 12(2)(g) Other indebtedness, giving same by classes and describing</u> <u>security, if any, with a brief statement of the devolution or assumption of any</u> <u>portion of such indebtedness upon or by person or corporation if the original</u> <u>liability has been transferred, together with amount of interest paid thereon</u> <u>during the last fiscal year.</u>

The Company has two series of Pollution Control Revenue Refunding Bonds issued under a Trust Indenture dated as of August 1, 2006 and a Trust Indenture dated as of December 1, 2008, between the County of Boone, Kentucky and Deutsche Bank National Trust Company as Trustee. The Company's obligation to make payments equal to debt service on the Bonds is evidenced by a Loan Agreement dated as of August 1, 2006 and December 1, 2008 between the County of Boone, Kentucky and Duke Energy Kentucky. The Bonds issued under the Indentures are below. On Nov 1, 2021, the Company bought in the Series 2008A bond, and remarketed the bond in June 2022.

		Principal				
		Amount	Principal			Interest
	Date of	Authorized	Amount	Rate of	Date of	Paid
Indenture	Issue	and Issued	Outstanding	Interest	Maturity	Year 2023
Series 2010	11/24/2010	26,720,000	26,720,000	3.86% (1)	8/1/2027	1,031,392
Series 2008A	12/01/2011	50,000,000	<u>50,000,000</u>	3.70% (2)	8/1/2027	<u>1,850,000</u>
			76,720,000			2,881,392

- ⁽¹⁾ The bonds were issued at a variable-rate and were swapped to a fixed rate of 3.86% for the life of the debt.
- ⁽²⁾ Bonds were remarketed in June 2022 under a fixed-to-maturity interest rate mode (3.70% coupon).

The Company has no outstanding financing leases as of May 31, 2024.

The Company also has \$54,712,000 of money pool borrowings outstanding as of May 31, 2024, \$25,000,000 of which is classified as Long-Term Debt payable to affiliated companies. This obligation, which is short-term by nature, is classified as long-term due to Duke Energy Kentucky's intent and ability to utilize such borrowings as long-term financing.

(8) <u>Section 12(2)(h) Rate and amount of dividends paid during the last five (5)</u> previous fiscal years, and the amount of capital stock on which dividends were paid each year.

DIVIDENDS PER SHARE

Year Ending	Per Share	Total	No. of Shares	Par Value of Stock
31-Dec-19	0	0	585,333	8,779,995
31-Dec-20	0	0	585,333	8,779,995
31-Dec-21	0	0	585,333	8,779,995
31-Dec-22	0	0	585,333	8,779,995
31-Dec-23	0	0	585,333	8,779,995

(9) <u>Section 12(2)(i) Detailed Income Statement and Balance Sheet.</u>

See the attached pages for a detailed Income Statement for the five months ended May 31, 2024 and a detailed Balance Sheet as of May 31, 2024.

DUKE ENERGY KENTUCKY, INC. CONDENSED STATEMENTS OF OPERATIONS

(Unaudited) (In thousands)

	Five Months Ended				
	May 31				
	2024				
Operating Revenues					
Electric	197,850				
Gas	71,385				
Total operating revenues	269,235				
Operating Expenses					
Fuel used in electric generation and purchased power	60,296				
Natural gas purchased	27,125				
Operation, maintenance and other	65,728				
Depreciation and amortization	45,888				
Property and other taxes	9,542				
Goodwill and other impairment charges	-				
Total operating expenses	208,579				
Gains on Sales of Other Assets and Other, net	96				
Operating Income	60,752				
Other Income and Expenses, net	3,365				
Interest Expense	12,152				
Income Before Income Taxes	51,965				
Income Tax Expense	9,945				
Income From Continuing Operations	42,020				
Income From Discontinued Operations, net of tax	-				
Net Income	42,020				

DUKE ENERGY KENTUCKY, INC. Condensed Balance Sheets

(Unaudited)

(in thousands, except share amounts)	May 31, 2024
ASSETS	
Current Assets	
Cash and Cash Equivalents	2,317
Receivables (net of allowance for doubtful accounts)	67,051
Receivables from affiliated companies	90
Notes Receivables from affiliated companies	-
Inventory	70,175
Regulatory Assets	13,888
Other	9,303
Total Current Assets	162,824
Property, Plant and Equipment	
Cost	3,464,273
Less Accumulated Depreciation and Amortization	(1,164,515)
Generation Facilities To Be Retired	-
Net Property Plant and Equipment	2,299,758
Other Noncurrent Assets	
Regulatory Assets	107,742
Operating Lease Right-of-Use assets	5,660
Other	21,972
Total Other Noncurrent Assets	135,374
Total Assets	2,597,956
LIABILITIES AND COMMON STOCKHOLDERS' EQUITY	
Current Liabilities	
Accounts Payable	28,306
Accounts payable to affiliated companies	36,012
Notes payable to affiliated companies	30,268
Taxes Accrued	20,810
Interest Accrued	7,353
Current Maturities of Long-Term Debt	-
Asset Retirement Obligations	6,762
Regulatory Liabilities	13,152
Other	16,072
Total Current Liabilities	158,735
Long-Term Debt	679,701
Notes payable to affiliated companies	25,000
Other Noncurrent Liabilities	
Deferred Income Taxes	304,722
Asset Retirement Obligations	80,163
Regulatory Liabilities	104,727
Operating Lease Liabilities	5,812
Accrued Pension and Other Post-Retirement Benefit Costs	27,467
Other	23,548
Total Other Noncurrent Liabilities	546,439
Commitments and Contingencies	-
Equity	
Common Stock, \$15.00 par value, 1,000,000 shares authorized and 585,333	
snares outstanding	8,780
Additional Paid in Capital	493,211
Retained Earnings	686,090
I otal Duke Energy Corporation Stockholders' Equity	1,188,081
Total Liabilities and Equity	3 507 050
וטנמו בומטווונופא מווע בקעונץ	2,597,950

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Duke Energy Kentucky, Inc. 139 E. 4th Street Cincinnati, OH 45202



July 11, 2024

Commonwealth of Kentucky Energy and Environment Cabinet Department for Environmental Protection Division for Air Quality 300 Sower Boulevard, 2nd Floor Frankfort, Kentucky 40601

RE: Duke Energy East Bend Station Agency Interest No: 176 Title V Operating Permit: V-12-023 Minor Permit Revision

Duke Energy Kentucky LLC, East Bend Station is proposing to convert the wet flue gas desulfurization (FGD) system from lime to limestone. The existing FGD process relies upon magnesium enhanced lime (MEL) to control SO₂ emissions. Recent issues with lime supply, quality, and price escalation pose additional risks to the East Bend Station from a reliability, compliance, and economic perspective. As a result, Duke Energy is proposing to convert the FGD system from lime to limestone, which will lower the operating cost and enhance unit reliability and compliance. The FGD process modifications will be designed to maintain an SO₂ removal efficiency of at least 98% for the design fuel.

The proposed project will require some minor changes to the existing reagent handling system, removal of some existing process equipment and the addition several new transfer points, a limestone pre-crusher, vertimill and a new wet scrubber.

Minor Changes to Existing Equipment

The existing unloading system, receiving hopper and main reagent storage silo will be repurposed for limestone. The existing unloading system will be equipped wear plates to accommodate limestone. Conveyors 1 and 3A will be equipped with restrictor plates on the tail end of conveyor to ensure the maximum hourly throughput capacity remains the same. Duke Energy is not proposing any changes to the hourly throughput or control devices associated with emitting units 14-01 thru 14-07 and 14-13 thru 14-16.

New Equipment

The proposed project will require installation of the following new equipment.

- 1) Two weigh belt feeders (WBFs) at the existing day bin discharge points.
- 2) One belt conveyor to transport limestone from the WBFs to the new reagent preparation system.
- 3) Pre-crusher to reduce the limestone to $< \frac{1}{4}$ inch.
- 4) Vertimill to grind the limestone down to achieve the final slurry.
- 5) One 29,000-gallon FGD buffer additive tank and feed pumps.
- 6) Modifications to the existing FGD scrubber to increase the liquid to gas ratio and improve the spray coverage.
- 7) Wet scrubber to control emissions from new emitting units associated with limestone handling.
- A process flow diagram is included in Attachment A.



Removal of Existing Permitted Equipment

Existing emitting units 14-8 thru 14-12 will be removed to accommodate the conversion of the FGD to limestone. Duke Energy will submit a separate request the remove of this equipment once the limestone conversion project is completed. Emitting units 14-17 thru 14-23 are no longer in service and can be removed from the permit.

Emissions Quantification

The particulate emissions from the following new limestone handling equipment will be controlled by a new wet scrubber.

- transfer of limestone from the day silo to the weigh belt feeders, identified as 14-26,
- transfer of limestone from the WBF to the conveyor 4A, identified as 14-27,
- transfer of limestone from conveyor 4A to the pre-crusher, identified as 14-28 and
- pre-crusher, identified as 14-29.

The wet scrubber will be designed to achieve compliance with the applicable PM emission standard from NSPS subpart OOO. The new vertimill is a wet process and will is not a source of particulate emissions. The potential to emit (PTE) for the new emitting units 14-26 thru14-29 is included in Attachment B Table 1.

As a result of the project the PTE from the existing equipment will be revised to reflect the emission factors for limestone handling, which result in a lower particulate emission. The PTE calculations for the existing equipment identified as 14-01 thru 14-07 and 14-13 thru14-16 are included in **Attachment B Table 2**.

Regulatory Review

The following subsections discuss the applicability of regulatory requirements for the conversion of the FGD to limestone.

Prevention of Significant Deterioration [401 KAR 51:017 and 40 CFR Part 52.21]

The Prevention of Significant Deterioration (PSD) rule is applicable to the construction of new major sources and major modification at existing major sources for pollutants which are in attainment or unclassifiable for the National Ambient Air Quality Standards (NAAQS). East Bend is located in Campbell County Kentucky which is designated as attainment or unclassifiable for all criteria pollutants. Consequently, the proposed project was reviewed for applicability to the PSD rule. Since the project involves both new and existing equipment the project was evaluated for PSD applicability using a Hybrid Test.

For the new equipment the increase in emissions was based on the uncontrolled potential to emit (PTE). The PTE for the new equipment identified as 14-26 thru 14-29 was calculated using emissions factors from AP-42 section 11.19.2 for Crushed Stone Processing and Pulverized Mineral Processing assuming maximum operating capacity and continuous hours of operation.

For the existing coal fired boiler, identified as Unit 2, the emissions increase associated with the proposed project was determined using the past actual to future projected analysis. The past actual emissions, in tons per year, are the emissions the unit emitted during any consecutive 24-month period on a pollutant-by-pollutant basis within the 60-month baseline period. The baseline period starts on October 1, 2019, and ends on March 31, 2025. The future projected emissions in tons per year, are the projected actual emissions at which the unit emitted the pollutant during any consecutive 12-month period selected within



the 60-month period immediately following the start of normal operation. The future projected emissions begin on January 1, 2027, and end on December 31, 2031.

The PSD regulation is applicable to projects which result in emissions increase which exceeds the PSD significance threshold, excluding demand growth. Demand growth is that portion of the unit's projected actual emissions that is unrelated to the particular project and due solely to the projected increase in utilization of the unit to meet customer demand.

Pollutants	SO2 (tons)	NOx (tons)	CO2e (tons)	VOC (Tons)	PM (tons)	PM2.5 (tons)	PM10 (tons)	PB (tons)	H2SO4 (tons)	CO (tons)
Baseline	1,832.42	1,893.63	3,259,191.59	47.27	171.48	362.03	425.38	0.03	126.77	338.83
Future W - Limestone	1,801.07	1,746.54	3,649,814.70	53.09	43.36	366.53	383.01	0.03	131.00	380.60
Future W/O -Quicklime	1,061.22	991.56	2,150,547.71	31.32	25.58	216.21	225.93	0.02	77.27	224.51
Demand Growth (DG)	0	0	0	0	0	0	0	0	0	0
New Equipment ¹			-		2.21	0.40	0.87			I.C.
Emissions Increase (EI)			390,623	6	1.2	4.90	-		4.22	42
EI - DG	22.2		390,623	6		4.90	-		4.22	42
Significant Emissions Threshold	40	40	75,000	40	25	10	15	0.6	7	100
PSD Applies	No	No	No	No	No	No	No	No	No	No
Reasonable Possibility Reporting	No	No	No	No	No	No	No	No	Yes	No

¹ Emission increase from new equipment is based on the uncontrolled potential to emit.

The PSD regulation is not applicable to this project since the emissions increase is below the PSD significant emissions rate for all NSR regulated pollutants, except for carbon dioxide equivalence (CO_{2e}). CO_{2e} is a measure of the total greenhouse gas emitted and was calculated using the equations in 40 CFR Part 98. CO_{2e} is only subject to the PSD rule when the project is subject to PSD for another NSR regulated pollutant and the emission increase in CO_{2e} exceeds the significant emissions threshold. Since the project does not trigger PSD for any other pollutant, PSD is not applicable to CO_{2e} .

The reasonable possibilities recordkeeping and reporting requirements applies to projects which have an emission increase excluding demand growth which exceeds 50% of the significance emissions threshold, on a pollutant by pollutant basis. Since H_2SO_4 exceeds the 50% of the significant emission threshold excluding demand growth, the proposed project triggers the reasonable possibilities reporting requirements for H_2SO_4 . Pursuant to 40 CFR Part 52.21(r)(6)(v) and 401 KAR 51:017(16)(5), East Bend Generating Station will report the annual emissions of H_2SO_4 for a period of 5 years following the resumption of normal operation after the change.

NSPS for Electric Utility Steam Generating Units 40 CFR Part 60 Subpart Da

The proposed project will not result in an increase in the maximum hourly emissions rate from Unit 2 for any pollutant regulated under subpart Da. Consequently, NSPS subpart Da is not being triggered because of this project.

NSPS for Nonmetallic Mineral Processing Plants, 40 CFR Part 60 Subpart OOO

The new conveyor/weight feeders, pre-crusher, and vertimill will be subject to NSPS subpart OOO, since this equipment is affected equipment pursuant to 60.670(a)(1) and is being constructed after effective date



of 8/3/1983. The exiting affected equipment being repurposed for limestone are not subject to NSPS Subpart OOO, since conversion to limestone will not result in an increase in the maximum hourly emission rate and this equipment was installed prior to 8/3/1983.

The following requirement under Subpart OOO are applicable.

- Pursuant to 40 CFR Part 60.672(a) the PM emissions from the wet scrubber, identified as C14-10, used to control emissions from 14-26 thru 14-30 will be subject to the PM emissions limit of 0.014 gr/dscf.
- Compliance shall be demonstrated based on an initial stack test to be conducted within 60 days of reaching maximum operating capacity but not longer than 180 days after initial startup using the procedures specified in 60.675(b).
- Pursuant to 40 CFR Part 60.674(a), the Permittee shall install, calibrate, maintain, and operate a continuous monitor the following monitoring devices on the wet scrubber identified as C14-10.
 - A device for the continuous measurement of the pressure loss of the gas stream through the wet scrubber. The monitoring device must be certified by the manufacturer to be accurate within ± 250 pascals ± 1 inch water gauge pressure and must be calibrated on an annual basis in accordance with the manufacturer's specification.
 - A device for the continuous measurement of the scrubbing liquid flow rate to the wet scrubber. The monitoring device must be certified by the manufacturer to be accurate within ±5 percent of design scrubbing liquid flow rate and must be calibrated on an annual basis in accordance with manufacturer's instructions.
- Pursuant to 40 CFR Part 60.676(c) during the initial performance test of a wet scrubber, and daily thereafter, the Permittee shall record the measurements of both the change in pressure of the gas stream across the wet scrubber and the scrubbing liquid flow rate.
- Pursuant to 40 CFR 60.676(d) and (e), after the initial performance test of the wet scrubber, the Permittee shall submit semiannual reports to the Administrator of occurrences when the measurements of the wet scrubber pressure loss and liquid flow rate decrease by more than 30 percent from the average determined during the most recent performance test. The reports shall be postmarked within 30 days following end of the second and fourth calendar quarters.
- Pursuant to 40 CFR 60.676(i), notification of the actual date of initial startup of each affected facility shall be submitted to the Administrator. The notification shall be postmarked within 15 days after such date and shall include a description of each affected facility, equipment manufacturer, and serial number of the equipment, if available.

Requested Changes to the Title V Permit

401 KAR 52:020, Section 14(3)(d), specifies that a modified version of the existing Title V permit with new text to reflect the proposed modification should be included with a minor revision application. This requirement is satisfied through the inclusion of the suggested permit in **Attachment C**.



Qualifications for Treatment as a Minor Permit Revision

This permit application seeks to revise the current Title V permit to reflect the installation as described in this application letter and its attachments. 401 KAR 52:020, Section 14 provides procedures for existing Title V sources to obtain minor permit revisions for modifications that meet certain criteria. An analysis of these criteria for this permit action is provided as follows:

- The proposed permit revision does not violate any applicable requirements contained within the existing Title V permit.
- The proposed permit revision does not involve significant changes to existing monitoring, reporting, or recordkeeping requirements in the permit.
- The proposed permit revision does not require or change a case-by-case determination of an emission limit, a source-specific determination for temporary sources, or a visibility or increment analysis. No PSD avoidance limits are necessary for this project.
- The proposed permit revision does not seek to establish or change a permit term or condition for which there is no corresponding underlying applicable requirement, and which the source has assumed to avoid an otherwise applicable requirement.

This permit action is not a modification under Title I of the Clean Air Act as this term is defined at 401 KAR 52:001 Section 1(52). Section 14(4) of 401 KAR 52:020 allows an applicant to proceed with the proposed modifications upon filing of an administratively complete minor revision application.

The application Forms DEP7007AI, 7007L, 7007N, 7007V and 7007GG are included in Attachment D.

Please contact Patrick Coughlin at 317-838-2108 if you should have any questions regarding this minor permit revision application.

I certify that, based on information and belief formed after reasonable inquiry, the statements and information contained in the following documents are true, accurate, and complete.

Sincerely,

Brett Riggins GM III – Regulated Stations

Enclosures

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Attachment A Process Flow Diagram





Proprietary Information – Subject to Duke Energy/AECOM Confidentiality Agreement

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Attachment B Emissions Quantification

Attachement B Emissions Quantification

Table 1- Potential to Emit for existing units being re-purposed to handel Limestone.

					Control	Control				Potential Lime Op	to Emit peration							Potential to Limestone Op	Emit eration				Change from	In Potential to Lime to Limes	o Emit stone
Emission		Control		Control	Efficeincy	Efficeincy	PM	PM10 ^(a)	PM2.5 ^(b)	Emission	Thurput	PM	PM10	PM2.5	PM	PM10	PM2.5	Emission Factor	Thurput	PM	PM10	PM2.5	PM	PM10	PM2.5
Unit ID	Description	Description	Stack ID	Device ID	PM	PM10/PM2.5	lbs/ton	lbs/ton	lbs/ton	Factor	ton/hr	tons/yr	tons/yr	tons/yr	lbs/ton	lbs/ton	lbs/ton	SCC#	ton/hr	tons/yr	tons/yr	tons/yr	tons/yr	tons/yr	tons/yr
ID: 14-01	Clamshell Unloader Digging from a Barge	Partial Enclosure	S14-01	Fugitive	90	81	2.2	1.1	1.1	3-05-016-15	600	578.16	549.25	549.25	0.003	0.0011	0.00007	3-05-020-06	600	0.788	0.734	0.035	-577.37	-548.52	-549.22
ID: 14-02	Clamshell Unloader to Receiving	Partial Encl & Baghouse	\$14-02	C14-04	75	74.6	2.2	11	11	3-05-016-15	600	1445.40	734.26	734.26	0.003	0.0011	0.00007	3-05-020-06	600	1 971	0.043	0.047	-1443.43	-734.26	-734.26
ID: 14 02		Declaration	514.02	C14.04	00	09.5	2.2	1.1	1.1	2.05.016.15	600	57.90	42.20	42.20	0.003	0.0011	0.00007	2 05 020 00	600	0.070	0.043	0.007	57.74	12.20	12.20
ID: 14-03	Receiving Hopper to Beit Feeder	Bagnouse	514-02	C14-04	99	98.5	2.2	1.1	1.1	3-03-010-13	600	57.82	43.30	43.30	0.005	0.0011	0.00007	5-05-020-06	600	0.079	0.045	0.003	-37.74	-43.30	-43.30
ID: 14-04	Belt Feeder to Conveyor "1"	Baghouse	\$14-02	C14-04	99	98.5	2.2	1.1	1.1	3-05-016-15	600	57.82	43.36	43.36	0.003	0.0011	0.00007	3-05-020-06	600	0.079	0.043	0.003	-57.74	-43.36	-43.36
ID: 14-05	Conveyor "1" to Unit 2 Main Silo	Baghouse	S14-03	C14-05	99	98.5	2.2	1.1	1.1	3-05-016-15	600	57.82	43.36	43.36	0.003	0.0011	0.00007	3-05-020-06	600	0.079	0.043	0.003	-57.74	-43.36	-43.36
ID: 14-06	Unit 2 Main Silo to Conveyor "3- A"	Baghouse	S14-04	C14-06	99	98.5	2.2	1.1	1.1	3-05-016-15	120	11.56	8.67	8.67	0.003	0.0011	0.00007	3-05-020-06	120	0.016	0.009	0.001	-11.55	-8.67	-8.67
ID: 14-07	Conveyor "3-A" to Day Bin (previously transferred to vibrating screen)	Baghouse	S14-05	C14-07	99	98.5	2.2	1.1	1.1	3-05-016-15	120	11.56	8.67	8.67	0.003	0.0011	0.00007	3-05-020-06	120	0.016	NA	0.001	-11.55	-8.67	-8.67
ID: 14-13	Dump Truck to Dumper House Hopper	Baghouse	S14-06	C14-08	99	98.5	2.2	1.1	1.1	3-05-016-15	25	2.41	1.81	1.81	0.003	0.0011	0.00007	3-05-020-06	25	0.003	0.002	0.000	-2.41	-1.80	-1.81
ID: 14-14	Hopper to Belt Feeder	Baghouse	S14-06	C14-08	99	98.5	2.2	1.1	1.1	3-05-016-15	25	2.41	1.81	1.81	0.003	0.0011	0.00007	3-05-020-06	25	0.003	0.002	0.000	-2.41	-1.80	-1.81
ID: 14-15	Belt Feeder to Conveyor "3"	Baghouse	S14-06	C14-08	99	98.5	2.2	1.1	1.1	3-05-016-15	25	2.41	1.81	1.81	0.003	0.0011	0.00007	3-05-020-06	25	0.003	0.002	0.000	-2.41	-1.80	-1.81
ID: 14-16	Conveyor "3" to Conveyor "3-A"	Baghouse	S14-04	C14-06	99	98.5	2.2	1.1	1.1	3-05-016-15	25	2.41	1.81	1.81	0.003	0.0011	0.00007	3-05-020-06	25	0.003	0.002	0.000	-2.41	-1.80	-1.81

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Attachement B Emissions Quantification

Table 2 - Potential to Emit for new emission units for the conversion to Limestone.

								Emissi	on Factors			Uncontrolled PTE		ГЕ	Controlled PTE		
					Control	Control				Emission							
Emission		Control		Control	Efficeincy	Efficeincy		PM10	PM2.5	Factor	Thurput	PM	PM10	PM2.5	PM	PM10	PM2.5
Unit ID	Description	Description	Stack ID	Device ID	$PM^{(1)}$	PM10/PM2.5 ⁽¹⁾	PM lbs/ton	lbs/ton	lbs/ton	SCC#	ton/hr	tons/yr	tons/yr	tons/yr	tons/yr	tons/yr	tons/yr
ID: 14-26	Transfer from day bin to wiegh belt feeders	Scrubber	S14-10	C14-10	90	90	0.003	0.0011	0.00007	3-05-020-06	35	0.460	0.169	0.011	0.0460	0.0169	0.0011
ID: 14-27	Transfer from wiegh belt feeders to belt conveyor 4A	Scrubber	S14-10	C14-10	90	90	0.003	0.0011	0.00007	3-05-020-06	35	0.460	0.169	0.011	0.0460	0.0169	0.0011
ID: 14-28	Transfer from conveyor 4A to pre- crusher	Scrubber	S14-10	C14-10	90	90	0.003	0.0011	0.00007	3-05-020-06	35	0.460	0.169	0.011	0.0460	0.0169	0.0011
ID: 14-29	Limestone pre-crusher	Scrubber	S14-10	C14-10	90	90	0.0054	0.0024	0.0024	3-05-030-03	35	0.828	0.368	0.368	0.0828	0.0368	0.0368

 Total Emissions Increase, tons/yr
 2.21
 0.87
 0.40
 0.22
 0.09
 0.04

⁽¹⁾ Scrubber will be designed to achieve compliance with the NSPS Subpart OOO PM standard of 0.014 gr/dscf and was conservatively estimated to achieve 90% control efficiency for PM/PM10/PM2.5.

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Attachment C Suggested Permit Conditions

SECTION B - EMISSION POINTS, EMISSION UNITS, APPLICABLE REGULATIONS, AND OPERATING CONDITIONS (CONTINUED)

Emissions unit: 14 (01-2529) - Lime Handling Operations (Fugitive Emissions)

Description:

DUSUI	ipuon.	
Equip	ment includes:	

Unit:Rate (tonsh)14-01Lime-Barge Loader600Short Drop Heights14-02Lime-Barge Unloader Hopper600Part Encl & Baghouse14-03Lime-Hopper to belt Feeder600Total Encl & Baghouse14-04Belt Feeder to Conveyer 1600Total Encl & Baghouse14-05Conveyer 1 to Main Lime Silo600Total Encl & Baghouse14-06Main Lime-Silo to Conveyer 3-A120Total Encl & Baghouse14-07Prior to conversion of FGD to limestone, conveyer 3-A to Day bin.120Total Encl & Baghouse14-09Vibrating Screen120Total Encl & Baghouse14-09Vibrating Screen120Total Encl & Baghouse14-10Day bin to screw Conveyer32Total Encl & Baghouse14-11Screw Conveyer to vert-Mill32Total Encl & Baghouse14-13Dump Crush Lime to Dumper House25Part Encl & Baghouse14-14Dumper House Hopper to belt Feed25Total Encl & Baghouse14-15Belt Feed to Conveyer 325Total Encl & Baghouse14-14Dumper House Hopper to belt Feed25Total Encl & Baghouse14-14Dumper House Hopper to belt Feeder25Total Encl & Baghouse14-14Dumper House Hopper to belt Feeder25Total Encl & Baghouse14-14Dumper House Hopper to belt Feeder25Total Encl & Baghouse14-15Belt Feed to Conveyer 3-A25Total Encl & Baghouse14-14Dumper House Hopper to belt	Emission	Description:	Process	Control Method:
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14-28Conveyer 4 to Pre-crusher35Total Encl & Scrubber14-29Limestone Pre-crusher35Total Encl & Scrubber	14-27	Weigh Feeder to Conveyer 4	35	Total Encl & Scrubber
14-29Limestone Pre-crusher35Total Encl & Scrubber	14-28	Conveyer 4 to Pre-crusher	35	Total Encl & Scrubber
	14-29	Limestone Pre-crusher	35	Total Encl & Scrubber

Construction commenced: 1976

Applicable Regulations:

401 KAR 63:010, Fugitive emissions

401 KAR 60:005, New Source Performance Standards for Nonmetallic Mineral Processing Plant **401 KAR 51:017**, Prevention of significant deterioration of air quality
SECTION B - EMISSION POINTS, EMISSION UNITS, APPLICABLE REGULATIONS, AND OPERATING CONDITIONS (CONTINUED)

1. **Operating Limitations:**

- a) Reasonable precautions shall be taken to prevent particulate matter from becoming airborne. Such reasonable precautions shall include, when applicable, but not be limited to the following [401 KAR 63:010, Section 3]:
 - 1. Application and maintenance of asphalt, application of water, or suitable chemicals on roads, material stockpiles, and other surfaces which can create airborne dusts;
 - 2. Installation and use of hoods, fans, and fabric filters to enclose and vent the handling of dusty materials, or the use of water sprays or other measures to suppress the dust emissions during handling.
 - 3. The maintenance of paved roadways in a clean condition;
 - 4. The prompt removal of earth or other material from a paved street which earth or other material has been transported thereto by trucking or other earth moving equipment or erosion by water.
- b) No person shall cause or permit the discharge of visible fugitive dust emissions beyond the lot line of the property on which the emissions originate [401 KAR 63:010, Section 3].
- c) No one shall allow earth or other material being transported by truck or earth moving equipment to be deposited onto a paved street or roadway [401 KAR 63:010, Section 4].
- d) Upon completion of the conversion of the FGD from lime to limestone, emission units 14-08 thru 14-12 will be decommissioned and emission unit 14-07 will transfer limestone from conveyor 3-A directly to the Day bin.

2. <u>Emission Limitations:</u>

Upon completion of the conversion of the FGD from lime to limestone the following emission limit shall apply.

a) The scrubber identified as C14-10 used to control particulate emissions from the emitting units 14-26 and 14-29 is subject to the PM emissions limit of 0.014 gr/dscf. [40 CFR Part 60.672(a)]

3. Testing Requirements:

Upon completion of the conversion of the FGD from lime to limestone stack tests for particulate matter on scrubber C14-10 shall be conducted within 60 days of reaching maximum operating capacity but not longer than 180 days after initial startup. [40 CFR 60.672(a) and 40 CFR 60.675(b)].

4. Specific Monitoring Requirements:

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SECTION B - EMISSION POINTS, EMISSION UNITS, APPLICABLE REGULATIONS, AND OPERATING CONDITIONS (CONTINUED)

The Permittee shall install, calibrate, maintain, and operate the following monitoring devices on the wet scrubber identified as C14-10. [40 CFR Part 60.674(a)]

- a) a device for the continuous measurement of the pressure loss of the gas stream through the scrubber. The monitoring device must be certified by the manufacturer to be accurate within ±250 pascals ±1 inch water gauge pressure and must be calibrated on an annual basis in accordance with the manufacturer's specification.
- b) A device for the continuous measurement of the scrubbing liquid flow rate to the wet scrubber. The monitoring device must be certified by the manufacturer to be accurate within ±5 percent of design scrubbing liquid flow rate and must be calibrated on an annual basis in accordance with manufacturer's instructions.

5. Specific Record Keeping Requirements:

- a) During the initial performance test of a wet scrubber, and daily thereafter, the Permittee shall record the measurements of both the change in pressure of the gas stream across the scrubber and the scrubbing liquid flow rate. [40 CFR 60.676(c)]
- b) Records of the lime and limestone received and processed (tonnages) shall be maintained on a weekly basis for emission inventory purposes [401 KAR 52:020, Section 10].

6. Specific Reporting Requirements:

- a) After the initial performance test of the scrubber, the Permittee shall submit semiannual reports to the Administrator of occurrences when the measurements of the scrubber pressure loss and liquid flow rate decrease by more than 30 percent from the average determined during the most recent performance test. The reports shall be postmarked within 30 days following end of the second and fourth calendar quarters. [40 CFR 60.676(d) and (e)]
- b) A notification of the actual date of initial startup of each affected facility shall be submitted to the Administrator. The notification shall be postmarked within 15 days after such date and shall include a description of each affected facility, equipment manufacturer, and serial number of the equipment, if available. [40 CFR 60.676(i)]

Refer to Section F, Monitoring, Recordkeeping and Reporting Requirements.

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SECTION B - EMISSION POINTS, EMISSION UNITS, APPLICABLE REGULATIONS, AND OPERATING CONDITIONS (CONTINUED)

7. Specific Control Equipment Operating Conditions:

- 1. Watering shall be used to maintain compliance with applicable requirements, in accordance with standard operating practices [401 KAR 63:010].
- 2. Records regarding the maintenance and use of the control measures in Subsection 7(a) shall be maintained [401 KAR 52:020, Section 10].
- 3. Refer to Section E, Source Control Equipment Requirements.

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Attachment D Permit Application Forms

KyPSC Case No. 2024-00152 Exhibit 3 Page 17 of 39

Division	for Air Qua	lity	DEP7 (Administrative	007AI	Addi	tional Documentation
300 So	ower Boulevard		Section AI.1: S	ource Information	Additio	nal Documentation attached
Frank	fort, KY 40601		Section AI.2: A	pplicant Information		
(50	2) 564-3999		Section AI.3: C Section AI.4: T			
	_		Section AI.5: C Section AI.6: S	Other Required Informa	tion	
			Section AI.7: N	lotes, Comments, and I	Explanations	
Permit #: Agency Interest (A) Date:	() ID:	V-12-023 176 11-Jul-24				
Section AI 1. S	Source Info	mation				
Section 1. A.A.	Street: City:	Union	County:	Boone	Zip Code:	40191
Physical Location Address:		6293 Beaver Road				
Physical Location Address:	Street or P.O. Box:					
Physical Location Address: Mailing Address:	Street or P.O. Box: City:	Union	State:	Kentucky	Zip Code:	40191
Physical Location Address: Mailing Address:	Street or P.O. Box: City:	Union	State: ard Coordinates fo	Kentucky r Source Physical Loc	Zip Code:	40191
Physical Location Address: Mailing Address: Longitude:	Street or P.O. Box: City:	Union Stand 38.904 (decimal de	state:	Kentucky r Source Physical Loc Latitude:	Zip Code: ation -84.851	40191 (decimal degrees)

Classification (SIC) C	ategory:	Electric Power Generat	ion	Primary SIC #:	4931	
Briefly discuss the typ conducted at this site:	oe of business	Electric Generating Utility	,			
Description of Area Surrounding Source:	✓ Rural Area ☐ Urban Area	Industrial Park Industrial Area	Residential Area Commercial Area	Is any part of the source located on federal land?	Yes	Number of Employees: 160 approx
Approximate distance to nearest residence o commercial property:	r 2200 feet (e:	timate d)	Property Area: 17	77 acers	Is this source portable?	Yes No
	What othe	r environmental permi	s or registrations doe	es this source currently hold	or need to obtain in Ker	ntucky?
NPDES/KPDES:	Currently Ho	old 🗌 Need	🗌 N/A		*	
Solid Waste:	Currently Ho	old 🗌 Need	🗌 N/A			· · · · · · · · · · · · · · · · · · ·
RCRA:	Currently Ho	old 🗌 Need	✓ N/A			
UST:	Currently Ho	old 🗌 Need	🗹 N/A			
Type of Regulated	Mixed Wast	e Generator	Generator		☑ Other:	
Waste Activity:	U.S. Importe	er of Hazardous Waste	Transporter	Treatment/Storage/Dispose	al Facility 🛛 N/.	A

1/2018						DEP							
Section AI.2: Ap	plicant Information	1											
Applicant Name: Title: (if individual)	Duke Energy Kentucky Inc., East Bend Station												
Mailing Address:	Street or P.O. Box: City:	6293 Beaver Road Union	State:	Kentucky	Zip Code:	40191							
Email: (if individual)	·												
Phone:	·)												
Technical Contact													
Name:	Patrick Coughlin												
Title:	Environmental Specialis	st											
Mailing Address:	Street or P.O. Box: City:	1000 East Main St. Plainfield	State:	Indiana	Zip Code:	46168							
Email:	patrick.coughlin@duke	-energy.com	2										
Phone:	317-838-2108												
Air Permit Contact for	Source				And the state of t								
Name:	Patrick Coughlin				and the second								
Title:	Environmental Speciali	st											
Mailing Address:	Street or P.O. Box: City:	1000 East Main St. Plainfield	State:	Indiana	Zin Code	46168							
Email:	patrick.coughlin@duke	-energy.com		111116116		40100							
Phone:	317-838-2108		all and a state	a an	· · · · · · · · · · · · · · · · · · ·								

DEP7007AI

Section AI.3: Ov	vner Information			etter et
🗹 Owner same	as applicant			
Name:	4	- 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	17 132 - 14 14 14 14 14 14 14 14 14 14 14 14 14	//statistics
Title:	5			
Mailing Address	Street or P.O. Box:			
Maning Address:	City:	State:	Zip Code:	
Email:		KK 0.00-0 0		
Phone:		1010-2015 Coloradore		52 2000
list names of owners a	nd officers of the company who have an	interest in the company of 5% or more.		
	Name	a naga ayan da	Position	
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KyPSC Case No. 2024-00152 Exhibit 3 Page 21 of 39

11/2018									DEP70
Section AI.4: Type	of Application								
Current Status:	✓ Title V 📋 Conditio	onal Major 🗌 State-Origin				General Permit		tion	☐ None
	Name Change	Initial Re	gistration		Significant Revis	ion	Adminis	trative Permi	t Amendment
	Renewal Permit	Revised I	Registration	-	Minor Revision		Initial Se	ource-wide O	peratingPermit
(check all that apply)	502(b)(10)Change	Extension	n Request		Addition of New	Facility	Dertable	Plant Reloca	tion Notice
	Revision	Off Perm	it Change		Landfill Alternate	e Compliance Submittal	✓ Modific	ation of Exist	ing Facilities
	Ownership Change								
Requested Status:	🗹 Title V 🔲 Condition	onal Major	State-O	Drigin	D PSD	□ NSR	Other		_
Pollutant: Particulate Matter Volatile Organic C Carbon Monoxide Nitrogen Oxides Sulfur Dioxide Lead	ompounds (VOC)	Requested	Limit:		Po	Ilutant: Single HAP Combined HAPs Air Toxics (40 CFR 68, S Carbon Dioxide Greenhouse Gases (GHG Other	Subpart F))	Requested	Limit:
Proposed Start (M	on: Date of Construction: (M/YYYY)		03/2025		Proposed Op	peration Start-Up Date:	(MM/YYYY)		01/2027
For Modifications: Proposed Start (M	Date of Modification: (M/YYYY)		Proposed Operation Start-Up Date: 03/2025			peration Start-Up Date:	(MM/YYYY)		01/2027
Applicant is seeking	coverage under a permit s	shield.	Ves		✓ No	Identify any non-applica sought on a sepa	able requirem arate attachm	ents for which ent to the ap	ch permit shield i plication.

Indicate the documents attached as part of this application:							
DEP7007A Indirect Heat Exchangers and Turbines	DEP7007CC Compliance Certification						
DEP7007B Manufacturing or Processing Operations	DEP7007DD Insignificant Activities						
DEP7007C Incinerators and Waste Burners	DEP7007EE Internal Combustion Engines						
DEP7007F Episode Standby Plan	DEP7007FF Secondary Aluminum Processing						
DEP7007J Volatile Liquid Storage	DEP7007GG Control Equipment						
DEP7007K Surface Coating or Printing Operations	DEP7007HH Haul Roads						
J DEP7007L Mineral Processes	Confidentiality Claim						
DEP7007M Metal Cleaning Degreasers	Ownership Change Form						
JDEP7007N Source Emissions Profile	Secretary of State Certificate						
DEP7007P Perchloroethylene Dry Cleaning Systems	✓ Flowcharts or diagrams depicting process						
DEP7007R Emission Offset Credit	Digital Line Graphs (DLG) files of buldings, roads, etc.						
DEP7007S Service Stations	Site Map						
DEP7007T Metal Plating and Surface Treatment Operations	Map or drawing depicting location of facility						
DEP7007V Applicable Requirements and Compliance Activities	Safety Data Sheet (SDS)						
DEP7007Y Good Engineering Practice and Stack Height Determination	Emergency Response Plan						
DEP7007AA Compliance Schedule for Non-complying Emission Units	Other:						
DEP7007BB Certified Progress Report							

I, the undersigned, hereby certify under penalty of law, that I am a responsible official*, and that I have personally examined, and am familiar with, the information submitted in this document and all its attachments. Based on my inquiry of those individuals with primary responsibility for obtaining the information, I certify that the information is on knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false or incomplete information, including the possibility of fine or imprisonment.

Authorized Signature

Brett Riggins

Type or Printed Name of Signatory

*Responsible official as defined by 401 KAR 52:001.

Date

GM III- Reg Stations

Title of Signatory

11/2018

Section AI.7: Notes, Comments, and Explanations

DEP7007AI

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	Divis	tion for	Air Oua						DEP70 ()7N						
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	Fra	ankfort, l	KY 4060	1			Section N.2: Stack Information						Complete DEP7007AI			
		(502) 56	4-3999					Sectio	n N.3: Fugit	ive Information	r		_			
								Sectio	n N.4: Notes	s, Comments, a	nd Explar	nations				
Source N	ame:	nergy Kentu	icky LLC., Eas	st Bend Gen	erating Statio	n										
KY EIS ((AFS) #:	29														
Permit #	:	R1														
Agency I	nterest (AI) ID:															
Date:																
N.1: Er	nission Summary															
Emission	Emission Process Process Control					Stock ID	Maximum Design	Dollutont	Uncontrolle d Emission	Emission Factor Source	Capture	Control	Hourly Emissions		Annual Emissions	
Unit #	Emission Unit Name	ID	Name	Name	Device ID	Stack ID	Capacity (SCC Units/hour)	Fonutant	Factor (lb/SCC Units)	(e.g. AP-42, Stack Test, Mass Balance)	(%)	(%)	Uncontrolled Potential (<i>lb/hr</i>)	Controlled Potential (lb/hr)	Uncontrolled Potential (tons/yr)	Controlled Potential (tons/yr)
14	Transfer from day bin to weigh belt feeders	26	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	РМ	0.003	AP-42 Section 11.19.2	100%	9 0%	0.105	0.01050	0.460	0.0460
14	Transfer from day bin to weigh belt feeders	26	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	PM10	0.0011	AP-42 Section 11.19.2	100%	9 0%	0.039	0.00385	0.169	0.0169
14	Transfer from day bin to weigh belt feeders	26	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	PM2.5	0.00007	AP-42 Section 11.19.2	100%	9 0%	0.002	0.00025	0.011	0.0011
14	Transfer from wiegh belt feeders to belt conveyor 4A	27	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	РМ	0.003	AP-42 Section 11.19.2	100%	9 0%	0.105	0.01050	0.460	0.0460
14	Transfer from wiegh belt feeders to belt conveyor 4A	27	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	PM10	0.0011	AP-42 Section 11.19.2	100%	<mark>90</mark> %	0.039	0.00385	0.169	0.0169
14	Transfer from wiegh belt feeders to belt conveyor 4A	27	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	PM2.5	0.00007	AP-42 Section 11.19.2	100%	<mark>90</mark> %	0.002	0.00025	0.011	0.0011
14	Transfer from conveyor 4A to pre-crusher	28	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	РМ	0.003	AP-42 Section 11.19.2	100%	9 0%	0.105	0.01050	0.460	0.0460
14	Transfer from conveyor 4A to pre-crusher	28	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	PM10	0.0011	AP-42 Section 11.19.2	100%	90%	0.039	0.00385	0.169	0.0169
14	Transfer from conveyor 4A to pre-crusher	28	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	PM2.5	0.00007	AP-42 Section 11.19.2	100%	90%	0.002	0.00025	0.011	0.0011

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Emission Unit # Emission Unit 1	Emission Unit Nama	Process	Process	Process Name Control Device Name	Contro l Device ID	Stack ID	Maximum Design Capacity (SCC Units/hour)	Uncontrolle d Emission	Emission Factor Source	Capture Efficiency	Control	Hourly Emissions		Annual Emissions		
	Emission Unit Name	ID	Name					1 onutant	Factor (lb/SCC Units)	(e.g. AP-42, Stack Test, Mass Balance)	(%)	(%)	Uncontrolled Potential (<i>lb/hr</i>)	Controlled Potential (lb/hr)	Uncontrolled Potential (tons/yr)	Controlled Potential (tons/yr)
14	Limestone precrusher	29	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	РМ	0.0054	AP-42 Section 11.19.2	100%	90%	0.189	0.01890	0.828	0.0828
14	Limestone precrusher	29	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	PM10	0.0024	AP-42 Section 11.19.2	100%	90%	0.084	0.00840	0.368	0.0368
14	Limestone precrusher	29	Limestone Handling	Wet Scrubber	C14-10	S14-10	35	PM2.5	0.0024	AP-42 Section 11.19.2	100%	90%	0.084	0.00840	0.368	0.0368

Section N UTM Zor	.2: Stack Informa ne:	tion								
	Identify all Emission	Sta	ack Physical Da	ata	Stack UTM	Coordinates	Stack Gas Stream Data			
Stack ID	ID) and Control Devices that Feed to Stack	Equivalent Diameter (ft)	Height (ft)	Base Elevation (ft)	Northing (m)	Easting (m)	Flowrate (acfm)	Temperature (°F)	Exit Velocity (ft/sec)	
S14-10	14-26. 14-27, 14-28 and 14- 29	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	

Section N.3: F	Section N.3: Fugitive Information													
U I M Zone:			Area Physic	al Data	Area UTM	Coordinates	Area Rele	ease Data						
Emission Unit #	Emission Unit Name	Process ID	Length of the X Side (fi)	Length of the Y Side (ft)	Northing (m)	Easting (m)	Release Temperature (°F)	Release Height (ft)						

Section N.4: Notes, Comments, and Explanations							

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Di	ivision fo	r Air Qı	DEP7007GG Additional Documentation Diality Control Equipment Complete Sections GG.1 through GG.12, as and the complete Sections GG.1 the complete Sections GG.1 through GG.12, as and the compl					DEP7007GG Control Equipment					tion 3.12, as app	licable				
	300 Sowe	r Boulev	ard									Attach manufacturer's specifications for each control device						
	Frankfort	KY 406	01		Complete DEP7007AI													
	(502) 5	64-3999																
Source N	ame:		Duke Energy K	Kentucky LLC	C., East Be	nd Generating	Station											
KY EIS (AFS) #:	21-	015-00029															
Permit #:			V-12-023															
Agency I	nterest (Al) ID:	176															
Date:			8-Jul-24															
Section G	G.1: Gene	ral Info	rmation - Co	ntrol Equip	ment							~ ~ ~		r				
Control Dovice ID	Control	Cost	Model	Model	Date	Inlet Gas Stream Data For <u>All</u> Control Devices				Inlet Gas Stream Data For Condensers, Adsorbers, Afterburners, Incinerators, Oxidizers Only Equipment Operational Data All Control Devices			al Data For vices					
#	Name	Cost	Manufacturer	Serial #	Serial #	Serial #	Name/ Installed	Temperature (°F)	Flowrate (scfm @ 68 °F)	Average Particle Diameter (µm)	Particle Density (lb/ft ³) or Specific Gravity	Gas Density (lb/ft ³)	Gas Moisture Content (%)	Gas Composition	Fan Type	Pressure Drop Range (in. H ₂ O)	Pollutants Collected/ Controlled	Pollutant Removal (%)
C14-10	TBD	TBD	TBD	TBD	TBD	ambient	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD	90%		

Section GG.11: Other Control Equipment								
sions)	Type of Control Equipment (provide description and a diagram with dimensions)	Identify all Emission Units and Control Devices that Feed to Control Equipment	Control Device ID #					
	Wet Scrubber	14-26, 14-27, 14-28 and 14-29	C14-10					
	Wet Scrubber	14-26, 14-27, 14-28 and 14-29						

Scrubber will be designe stimated to achieve 90	d to achieve compliance with the NSPS Subpart OOO PM standard of 0.014 gr/dscf and was conservativel % control efficiency for PM/PM10/PM2.5.

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11/2018		DEP7007
	DEP7007L	Additional Documentation
Division for Air Quality	Mineral Processes	Complete DEP7007AI,
Division for the Quanty	Section L.1: Source Operating Information	DEP7007N, DEP7007V, and DEP7007CC
300 Sower Boulevard	Section L.2: Concrete Operations	DEI 700700.
Frankfort KY 40601	Section L.3: Asphalt Operations	Attach flow diagram
(502) 564-3999	Section L.4: Coal Operations	
	Section L.5: Aggregate Processing Operations	
	Section L.6: Feed, Corn, and Flour Operations	
	Section L.7: Grain Elevators	
	Section L.8: Fertilizer Operations	
	Section L.9: Notes, Comments, and Explanations	
Source Name:	uke Energy Kentucky IIC East Bend Generating Station	
	15 00000	
$\mathbf{KI} \mathbf{EIS} (\mathbf{AFS}) #: 21-\underline{0}$	15-00029	
Permit #: V	-12-023 R1	
Agency Interest (AI) ID: <u>1</u>	76	
Date: 8	-Jul-2024	
Section L.1: Source Operatin	g Information	
Type of Plant: Concrete	Asphalt Coal Fertilizer Feed Corn Flour Grain E	evators Aggregate Processing
Operating Schedule:	24 Hours/Day: 7 Days/Week:	52 Weeks/Year:
Percent Annual Throughput:	DecFeb.: 25 % MarMay: 25 % JunAug.: 25	% SepNov.: <u>25</u> %
Maximum Rated Source Capacity:	35tons/hour306,600tons/year	

Combustion Equipment:									
Is there a generator located on site?	es 🗌 No								
Is it possible for the generator to remain at one site longer than twelve months?									
Is there a hot water heater located on site?	✓ Yes	□ No							
Is there a dryer located on site?	Yes	☑ No							
Is there a hot oil heater (asphalt heater) located	on site?	Yes V No							
Describe briefly the disposal of particulates coll- and/or other waste generated at the site:	Describe briefly the disposal of particulates collected in the baghouse and/or other waste generated at the site: The existing lime handling equipment will repurposed to handle limestone 14-1 thru 14- identified as units 14-26 thru 14-30 will be installed.								
Is there additional information attached to support the data required in this form? Yes No Brief description of additional information included: flow diagram, draft language, emissions calculations									

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Section	Section L.5: Aggregate Processing Operations											
New Source Performance Standard Applicability												
Are any emission units for the operation subject to: 🗹 NSPS, Subpart OOO 🗌 None 🗌 Other:												
Complete t	Complete the Table:											
Emission	Affected Facility	Maximu Cap	ım Rated acity	Control Mathad on	Control Efficiency (% removal)	800 G J	Pollutant	Emission Factor (lb/SCC unit)	Source of	Proposed/Actual Date of Construction Commencement (MM/YYYY)	Installation Date of Each Unit	Is the Unit Subject to NSPS? (Yes or No)
Unit #		(tons/hr)	(tons/yr)	Method or Equipment		SCC Code			Factor			
14-26	Transfer Limestone from day bin to weigh belt feeders	35	306600	Scrubber	90	30502006	PM	lb/ton	AP-42	25-Mar	NA	Yes
14-27	Tansfer of Limestone from weigh belt feeder to conveyor 4A	35	306600	Scrubber	90	30502006	PM	lb/ton	AP-42	25-Mar	NA	Yes
14-28	Transfer of Limestone from conveyor 4A to pre-crusher	35	306600	Scrubber	90	30502006	PM	lb/ton	AP-42	25-Mar	NA	Yes
14-29	Pre-crusher	35	306600	Scrubber	90	305003003	PM	lb/ton	AP-42	25-Mar	NA	Yes

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				DEP7	Ad	Additional Documentation				
Divisi	ion for Air Quali	ty App	olicable I	Requirem	nce					
Activities							omplete DEP7007AI			
300) Sower Boulevard		Section	on V.1: Emis	sion and Operating Lim	itation(s)				
Fr	ankfort, KY 40601		Sectio	on V.2: Moni	toring Requirements	·				
	(502) 564-3999		Section	on V.3: Reco	rdkeeping Requirement					
			Section V.4: Reporting Requirements							
			Sectio	on V.5: Testi	ng Requirements					
			Sectio	on V.6: Notes	s, Comments, and Expla	inations				
Source Nan	ne: Duke E	nergy Kentucky LL	C. East Ben	d Generating	s Station					
KY EIS (Al	FS) #: 21- 015-000	129								
Permit #:	V-12-02	23 R1								
Agency Inte	erest (AI) ID:	176								
Date:	8-Jul-24	4								
Section V	1: Emission and	d Operating Lin	nitation(s	5)						
Emission Unit #	Emission Unit Description	Applicable Regulation or Requirement	Pollutant	Emission Limit (if applicable)	Voluntary Emission Limit or Exemption (if applicable)	Operating Requirement o Limitation (if applicable)	Method of Determining r Compliance with the Emission and Operating Requirement(s)			
14-26 thru 14- 29	New Limestone Handling	60.672(a), 60.674(a)	PM	0.014 gr/dscf			Method 5			
			l							

Section V.	.2: Monitoring Re	quirements			
Emission Unit #	Emission Unit Description	Pollutant	Applicable Regulation or Requirement	Parameter Monitored	Description of Monitoring
14-26,14-27, 14- 28 and 14-29	Limestone Handling and pre-crusher	PM	60.674 (a) (1)	Monitor pressure across the scrubber	Continuous measurement of the pressure loss of the gas stream through the scrubber. The monitoring device must be certified by the manufacturer to be accurate within ± 250 pascals ± 1 inch water gauge pressure and must be calibrated on an annual basis in accordance with the manufacturer's specification.
14-26,14-27, 14-28 and 14-29	Limestone Handling and pre-crusher	РМ	60.674 (a)(2)	Monitor scrubber liquid flow rate	Continuous measurement of the scrubbing liquid flow rate to the wet scrubber. The monitoring device must be certified by the manufacturer to be accurate within ±5 percent of design scrubbing liquid flow rate and must be calibrated on an annual basis in accordance with manufacturer's instructions.

Section V.3: Recordkeeping Requirements										
Emission Unit #	Emission Unit Description	Pollutant	Applicable Regulation or Requirement	Parameter Recorded	Description of Recordkeeping					
14-26, 14-27, 14-28 and 14-29	Limestone Handling and pre-crusher	РМ	60.676(b)	Daily pressure change across the scrubber and scrubber liquid flow rate.						

Section V.4: Reporting Requirements										
Emission Unit #	Emission Unit Description	Pollutant	Applicable Regulation or Requirement	Parameter Reported	Description of Reporting					
14-26,14-27, 14-28 and 14-29	Limestone Handling Pre-crusher	NA	60.676(i)	Date of initial startup	Notification of actual startup The notification shall be postmarked within 15 days after such date and shall include a description of each affected facility, equipment manufacturer, and serial number of the equipment, if available.					
14-26,14-27, 14-28 and 14-29	Limestone Handling Pre-crusher	РМ	60.676(d)(e)	Change in pressure across the scrubber and scrubber liquid flow rate	Submit semiannual reports to the Administrator of occurrences when the measurements of the scrubber pressure loss and liquid flow rate decrease by more than 30 percent from the average determined during the most recent performance test.					
Unit 2	Coal Fired Boiler	H ₂ SO ₄	401 KAR 51:017(16)(5) 40 CFR Part 52:21(r)(6)(v)	Annual emissions of H2SO4	Report annual emissions of H ₂ SO ₄ wiithin 60 days after the end of the calendar year for a period of 5 years following resumpsion of normal operation after the change.					

11/2018

Section V.5: Testing Requirements						
Emission Unit #	Emission Unit Description	Pollutant	Applicable Regulation or Requirement	Parameter Tested	Description of Testing	
14-26, 14-27, 14-28 and 14-29	Limestone Handling and Pre-crusher	РМ	60.674(c)	РМ		

Section V.6: Notes, Comments, and Explanations			



Duke Energy East Bend Station

Wet FGD Conversion to a Limestone Inhibited-Oxidation Process Preliminary Engineering Report

Duke Energy

Project number: 60724995

July 12, 2024

Quality information

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Revision History

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Revision	Revision date	Details	Authorized	Name	Position
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1. Introduction and Project Basis

1.1 Project Basis

Duke Energy's East Bend Station currently operates a wet flue gas desulfurization (FGD) process that relies upon magnesium-enhanced lime (MEL) to control SO₂ emissions. However, the expenses associated with lime reagent, stabilization additives and disposal of the waste sludge produced by the process result in very high FGD operating costs which adversely affect the competitiveness of the East Bend Station in today's power markets. Furthermore, recent issues with lime supply, quality, and price escalation pose additional risks to the East Bend Station from a reliability, compliance, and economic perspective.

As a result, Duke Energy approached AECOM to assess the technical feasibility of converting the FGD system to use lower-cost limestone reagent in an inhibited oxidation process (LSIO) while still meeting all environmental and reliability requirements, and whether the required capital investment is economically justified.

1.2 **Project Background**

AECOM completed a Phase 1 Engineering Study (the Study) in 2022 which evaluated the technical and economic feasibility of converting the East Bend FGD system to a LSIO process. The Study identified the required scope items to convert the East Bend FGD system from MEL operation to LSIO operation, which are detailed in Section 3.

The Study report included the design basis, scope, and assumptions for a complete conversion of the existing FGD system to LSIO operation. The following preliminary documents formed the basis for the project scope:

- Process design basis, PRISM modeling, material balances, and process flow diagrams (PFDs),
- P&IDs,
- General arrangements, equipment layouts, and Power Distribution Center (PDC) arrangement,
- Equipment list, load list, one-line diagrams, and net IO summary,
- Contract and procurement approach,
- EPC schedule, and
- Class 3 cost estimate.

1.3 **Objectives**

The objectives of the Study were to determine the technical requirements, capital investment, and operating cost savings associated with converting the East Bend wet FGD process to LSIO operation. The Study established the following preliminary information:

- Design basis for the FGD conversion from MEL to LSIO,
- Process modifications to existing systems,
- Major equipment and infrastructure for new systems,
- System and equipment arrangements and configurations,
- Project schedule,
- Cost estimate, and
- Contract and procurement approach.

2. Technology Overview

The Wet FGD system at East Bend uses MEL scrubbing technology, which relies on pebble quicklime containing a small fraction of dolomite as the reagent. Dolomite is comprised of about 50% magnesium oxide which, when added to the absorber with the lime reagent, dissolves and promotes elevated concentrations of sulfite. Sulfite is an effective source of liquid-phase alkalinity, which facilitates high SO₂ removal efficiency for boilers firing high sulfur coal. The primary benefit of scrubbing with MEL is that the required absorber recycle slurry pumping capacity is lower than limestone-based FGD systems – typically in the range of 40 to 50 gallons per 1,000 cubic feet of treated flue gas – and results in smaller pumps with lower power requirements.

A key disadvantage of the MEL technology is the production of calcium sulfite (CaSO₃) solids that are typically difficult to dewater. As a result, significant quantities of fly ash and lime must be added to the filtered solids to produce a stable product suitable for disposal in a landfill. Conversion to LSIO chemistry will improve the dewatering properties of the calcium sulfite solids by creating larger, more regular, and symmetric crystals. A comparison of calcium sulfite crystals produced by MEL and LSIO scrubbing is provided in Figure 2-1.



Figure 2-1: Comparison of Crystal Shapes from MEL and LSIO FGD Systems

The FGD waste solid crystals in the left image were collected from an MEL FGD system of similar design and vintage to East Bend; oxidation was approximately 11%. The irregular shape of the crystals causes them to trap water between the solids such that dewatering is not easily achieved. The FGD waste solid crystals in the right image were collected from another utility that converted from MEL to LSIO operation. Due to the sulfite oxidation inhibiting properties of thiosulfate and sodium formate, oxidation in that unit was approximately 5%. The flatter, cubic, and larger LSIO crystals enable more efficient water removal from between the solid crystals in the slurry. As a result of the LSIO conversion at East Bend, a significant improvement in dewatering characteristics of the FGD solids is expected, resulting in much drier filter cake, less water landfilled, and reduced fixation lime requirements.

Another disadvantage of note with MEL scrubber technology is the loss of liquid-phase alkalinity due to oxidation of sulfite to sulfate during periods of low load operation or if an FGD absorber is out of service. Liquid-phase alkalinity must be re-established when load increases or the system is returned to service before the FGD process can achieve required efficiency. The degradation in performance has become a greater concern as more coal-fired units operate at lower capacity factors in the current market while emission limits and compliance requirements become more stringent.

The following process modifications are needed to convert an existing MEL scrubber to LSIO operation:

- Reagent Unloading. Due to differences in their molecular weight, more limestone by mass is required than MEL to scrub the same quantity of SO₂. Further, the bulk density of limestone is roughly double the bulk density of lime. As a result, the existing reagent unloading and material handlings systems, designed for MEL, often require modification to accommodate new operating conditions and higher density material.
- Reagent Preparation. The reagent preparation system for a MEL scrubber consists of a lime slaking device. Generally, slakers cannot be repurposed to grind limestone to the required fineness due to overall mechanical configuration issues or capacity issues. New grinding mills are often required to produce the necessary quantity and quality of reagent slurry sufficient for the FGD process. New equipment enclosures or enclosure additions are also often required to house the new grinding systems.
- Liquid-phase Alkalinity. Liquid-phase alkalinity provides the main driving force for SO₂ removal in MEL scrubber systems. Limestone scrubbers rely predominately on solid-phase alkalinity with dissolution of limestone in the absorber replenishing alkalinity to facilitate SO₂ scrubbing. Due to this fundamental difference, MEL scrubbers require less interaction between the scrubber liquor and flue gas to achieve the required removal efficiency and are designed to operate at lower liquid-to-gas (L/G) ratios. To compensate for this difference while minimizing the capital investment associated with increasing the L/G, a performance additive such as sodium formate (NaFo) is used to provide equivalent alkalinity following an LSIO conversion. However, since performance additives will not degrade in the slurry as the reaction tank sits idle during outages and can also be added directly to the scrubbers following an outage in which the absorber reaction tanks are drained, the FGD system is able to maintain consistent SO₂ removal performance under all operating scenarios.
- Mist Eliminator Wash System. The mist eliminator (ME) wash systems for MEL scrubbers were typically designed as general flush systems to remove slurry carryover from the front surfaces of the ME stages to prevent accumulation of calcium sulfite. However, the slurry carryover in LSIO FGD slurry also contain residual limestone solids that react with SO₂ remaining in the flue gas passing through the ME. As such, the ME wash system for a limestone based FGD system should be more robust in design with respect to wash intensity (gpm/ft2) and wash pressure to provide effective removal of the FGD slurry from the ME surfaces.

3. **Project Scope and Design Information**

AECOM developed a preliminary design and layout for the conversion of the East Bend FGD process to LSIO operation. This section provides a general overview of the design basis and preliminary design for the system. Preliminary drawings are included in the appendices of this report.

3.1 Design Basis

The FGD process modifications are designed to maintain an SO_2 removal efficiency of at least 98% for the design fuel (5.66 lb SO_2 / MMBtu). Table 3-1 provides key design basis inputs.

Parameter	Unit	Value
Site Elevation	Ft above MSL	515
Number of Generating Units	-	1
Unit Load, Net	MW	600
Unit Heat Rate, Net	Btu/kWh	10,760
Unit Heat Input	MMBtu/hr	6,456
Annual Capacity Factor	%	69
Coal Heating Value	Btu/lb	11,778
Coal Ash Content	wt%	9.02
Fly Ash Portion of Total Ash	% by weight	80
Coal Sulfur Content	%-wet	3.20
SO ₂ Removal Requirement (Design)	%	98
Lime Reagent CaO Purity	%	90.3
Limestone CaCO ₃ Purity	%	92
Limestone size (received)	-	1"x0
Limestone size (product)	-	90% passing 325 mesh

Table 3-1: Preliminary Design Basis

3.2 Scope Overview

The LSIO conversion project scope includes modifications to existing equipment and is based on the turnkey delivery, including engineering, procurement, and construction. The conversion of the East Bend FGD system to LSIO operation involves several process, equipment, and system changes including:

- Minor modifications to reagent receiving, conveying, and storage systems.
- Installation of new reagent feeders and conveying equipment.
- Installation of new limestone pre-crushers and grinding mills.
- Refurbishment and resheaving of absorber recycle pumps.
- Installation of new absorber recycle slurry piping, cross-tie piping, spray headers, and spray nozzles.
- Operation of all absorber recycle slurry pumps to enhance SO₂ removal performance.
- Modification of the absorber trays to enhance SO₂ removal performance.
- Installation of a buffer additive storage and feed system to enhance SO₂ removal performance.
- Replacement of existing emulsified sulfur storage tank and feed system to improve system reliability and inhibit sulfite oxidation.

- Upgrade of mist eliminator wash water supply system.
- Replacement of waste slurry storage tank, thickener underflow sludge tank, and lime slurry tank agitators.
- Installation of a filtrate purge system to control process chloride levels.

3.3 System Descriptions and Scope

3.3.1 Material Handling System

The material handling system includes infrastructure and equipment required for the receiving, unloading, conveying, processing, and storage of the limestone reagent (currently magnesium-enhanced lime). Limestone will be received by barge at the barge unloading area where it is offloaded and then conveyed to the storage silo area. From here, the limestone will be conveyed to the day bin area where it will be temporarily stored for distribution to the reagent prep system by way of a new belt conveyor system.

- 1. Limestone Flowability Studies will be performed on the Unloading Hopper, Storage Silo, modified Day Bin, and the pre-crusher outlet chute. The primary objective of the studies is to confirm the assumption that no geometry modifications are required on the Unloading Hopper or the Storage Silo, guide the detail design on the Day Bin outlet modifications, and provide design parameters for the pre-crusher outlet chute.
- 2. Barge Unloading Area The existing barge unloader and unloading hopper will be repurposed for limestone service. The following modifications are planned at the barge unloading area:
 - a. Install a new, smaller, barge unloading clamshell bucket to account for the higher density of limestone and stay within the system design parameters.
 - b. Modify existing 30-day storage silo inlet chute to extend below maximum fill level for level control.
- 3. Storage Silo Area The existing lime storage silo will be repurposed for limestone service. The following modifications will be performed at the storage silo:
 - a. Install a profile plate on the tail end of Conveyor 3A to limit the conveyor's limestone tonnage throughput to match the existing lime throughput on the conveyor.
 - b. The high-level alarm(s) setpoint will be lowered so that the weight capacity of the existing silo is not exceeded due to the higher density of the limestone (relative to lime) stored in the silo. The existing level transmitter and cabling will be reused.
 - c. Demolish existing metal detector and install a new manual magnetic separator at the head end of LH1.
- 4. Day Bin Area The following modifications will be made to convert the existing lime day bin to limestone service:
 - a. A new feed chute on the discharge of Conveyor 3A will be installed down to the day bin. The chute will be equipped with AR liners.
 - b. Bin Outlet Modifications The eight existing day bin outlets will be modified to four discharge points. Outlet slopes will be equipped with AR liners. Design of the modifications to the bottom of the bin to accommodate the new discharge points will take into consideration the need to reduce the allowable storage volume of the bin to prevent exceeding the weight capacity of the equipment.
 - c. Four new weigh belt feeders (WBFs) will be installed at the day bin discharge points. Each WBF will be equipped with a slide gate to isolate the WBF from the day bin material. Each limestone material handling train (two trains total) will be equipped with two 100% WBFs, one operating and one spare.
 - d. Supplemental steel and platform modifications will be designed and provided for new WBF installations.
 - e. The high-level alarm(s) setpoints will be lowered so that the weight capacity of the existing day bin is not exceeded due to the higher density limestone being stored in the day bin. The existing level transmitter and cabling will be reused.
- 5. Limestone Conveying System A new belt conveyor system will be installed to transport limestone from the WBFs to the new reagent preparation system. The conveying system includes:
- a. Two 24" wide belt conveyors (one per train) that collect material from the discharge of the WBFs and feed it into the limestone preparation system. The conveyors will be equipped with a walkway on both sides and have ladder access to the WBF deck. The conveying systems will be equipped with manual screw take-ups on the tail pulleys and a tramp metal detection system that is interlocked with the transfer conveyors to prevent damage to the pre-crushing and grinding systems.
- b. New AR lined chutes will be installed between the WBFs and the transfer conveyors. New AR lined chutes will be installed at the discharge of the transfer conveyor and feed into the reagent preparation system.
- c. Limestone transfer points (WBF discharge, transfer conveyor discharge) and the pre-crusher will have connections to a new dust collection system.
- d. Supplemental steel will be designed and installed to support the limestone conveying and tensioning system.
- e. Foundations will be installed for some conveyor support structures that cannot be supported from building steel.
- 6. Instrumentation and Controls New control devices for the material handling system that will be installed include:
 - a. Conveyor belt control devices will include pullcord switches the full length of the transfer conveyor, belt misalignment switches, and zero speed switches. The weigh belt feeders will include scales, VFDs, other devices to control limestone feed rate and devices to protect the weigh belt feeders.
 - b. New chutes will be equipped with plugged chute switches.
 - c. The new dust collector system will include level switches and automated valves for cleaning the new dust collection system.
- 7. Cabling and Raceways New cables and raceways will be installed to energize and control new equipment.
 - a. Power cabling will be installed from a new 480V lineup in the new limestone grinding building to new conveying system equipment.
 - b. New instrument and control cabling will be installed from material handling equipment to a new RIO cabinet in the new Power Distribution Center (PDC).
 - c. New cable trays will be installed for power, instrument, and control cabling. Metal conduit and flex conduit will be used for final drops to equipment and other end users.
 - d. Supplemental steel for raceway supports will be designed and installed.
 - e. Foundations for raceway support steel will be installed at grade.
- 8. Demolition The existing metal detector at the top of the 30-day lime silo will be removed. The day bin vibrating screen (and associated chute work), day bin bottoms, lime screw feeders, and the day bin outlet gates will be removed to accommodate the new limestone conversion equipment. Penetrations will be made on the existing reagent preparation building for transfer conveyor access. Other equipment no longer used and not interfering with the new equipment will be abandoned in place.

3.3.2 Reagent Prep System

The reagent prep system includes unit operations for crushing and grinding limestone received from the material handling system. The limestone received will first pass through a pre-crusher system where the product will be crushed before it is sent to the limestone grinding system. From the pre-crushing system, the pre-crushed product will be sent to Vertimills for final slurry product sizing. Final slurry product will be stored in the existing lime transfer storage tank.

- 1. Limestone Pre-crushing System Two 100% pre-crushing systems will be installed to size the limestone down to an acceptable top size for the grinding systems (<1/4"). The pre-crushing system is summarized below:
 - a. A pre-crusher will be installed between each limestone transfer conveyor (two pre-crushers total) and each grinding system.

- b. A new discharge chute will be installed on the outlet of the pre-crusher. Each chute will feed into its respective grinding system and will be lined with AR material.
- 2. Limestone Grinding System Two 100% limestone grinding trains will be installed to achieve the final slurry product sizing of 90% passing 325 mesh. The grinding system consists of the following equipment.
 - a. Two 100% vertical mill systems (VTMs) rated for 35 TPH will be installed. Each VTM will be equipped with a 1000 HP motor, a separation tank and a recycle pump. The lower portions of the VTMs are lined with magnetic tiles and the upper portion is lined with abrasion resistant material. The VTM bearings will be automatically lubricated with a grease pump and accessories. The VTM gearbox will be lubricated via a forced lubrication skid which includes duplex oil filters, temperature control, and sample valves. The mills are equipped with a door jacking system to assist with clearing the door jamb. A single portable hydraulic pump will be provided. A single common screw transporter will be provided to facilitate major maintenance activities. The screw transporter includes a hydraulic jacking system to raise/lower the screw in/out of the mill body. Two screw stands will be provided to facilitate maintenance activities. A single, 2-ton electric ball charge hoist will be provided for adding grinding media to both mills. The initial ball charge will be provided. Vendor support including field installation, process commissioning, and operator training.
 - b. Each grinding system will include a classification system to perform the final slurry product sizing. Each classification system will include a hydrocyclone feed tank, feed tank agitator, hydrocyclone cluster, outlet distribution box (for feed tank level control), and two feed pumps. A single, 1-ton electric hoist will be installed for servicing the hydrocyclone clusters. 200' of' 8" diameter AR FRP piping is included in the design to transfer slurry from both classifier feed tanks to the classifiers. The hydrocyclone underflow will be routed via gravity drain using 6" AR FRP piping to the Vertimill for further processing. An allowance of 400' of piping is included in the design for both underflow and overflow systems.
 - c. Each hydrocyclone overflow will be routed via gravity drain to the existing lime transfer storage tank or returned to the hydrocyclone feed tank via the outlet distribution box using 6" AR FRP piping.
 - d. The pre-crushing and VTM equipment along with ancillary components will be installed in a steel enclosure with structural steel framing and aluminum-zinc coated steel panels for roofing and siding southeast of the existing slaker building. A 35-ton bridge crane will be provided for servicing the VTMs. The enclosure will be equipped with man-doors to provide sufficient ingress/egress for plant staff, two roll-up doors, lighting, convenience power, insulation, and heating/ventilation equipment. The vertical mill hydrocyclones and launders will be installed on an elevated concrete deck and a building sump will be provided with two sump pumps and an agitator. Two tempered eye wash stations will be provided. Fire detection hardware will interface with an existing fire detection monitoring panel.
 - e. New utility and process piping for the grinding systems will be provided and installed. Service water will be utilized for grinding water and flush water. Approximately 240' of 6" piping and 130' of 4" is included in the design for service water. Service water and service air piping will be carbon steel. One-hundred and fifty feet of copper piping will be used for the eye wash stations. Slurry piping will be equipped for automated flushing slurry from the piping prior to system shutdowns. Slurry isolation valves will be knife gate valves and flush water valves will be butterfly valves. Utility valves will be ball valves or gate valves. Water piping located outdoors will be heat traced and insulated. Pipe supports for process and utility piping will be provided and installed.
 - f. Supplemental steel for pipe supports will be designed and installed. An allowance of 17 tons for supplemental steel is included in the design.
 - g. Foundations for the mills, tanks, pumps, and enclosure will be designed and installed. Final site grading will be performed. A Geotechnical investigation will be performed.
 - h. A new 20 HP agitator will be installed in the existing reagent slurry tank. It is assumed the existing agitator power cables are at least #10 conductors and adequate for the new service. The existing agitator starter will be reused.
 - i. The lining system of the reagent slurry tank will be replaced with a flake glass lining.
- 3. FGD Additive System A new FGD additive system will be installed to enhance the liquid phase alkalinity of limestone slurry. The features of the additive system include:

- a. A new double wall 29,000-gallon shop fabricated FRP tank will be provided for storing FGD system additive. The tank will be located indoors in the existing slaker building. The tank will include a heating system and insulation installed to maintain a product temperature of 100 deg F.
- b. A new pump skid equipped with two 100% capacity 1.2 gpm positive displacement chemical pumps will be installed indoors in the adjacent slaker building. The additive pumps will pump the FGD additive to the existing lime/limestone slurry storage tank. The pumps will be heat traced and equipped with removable blanket insulation.
- c. New 304 SS tubing from the additive storage tank up to the existing limestone slurry storage tank will be installed. Approximately 100' of new 3/8" SS tubing will be designed and installed. The piping system will include manual valves, check valves, heat tracing, insulation, and pipe supports.
- d. Foundations for the new additive tanks, pumps, pipe supports, and raceways will be designed and installed.
- e. A truck unloading system will be installed to fill the additive tank. It is assumed the tank will be close enough to the unloading station so that the tank truck pumps can be used for filling the new additive tank. The unloading station will be equipped with an eyewash station and containment system. The containment will be equipped with manual drain valve and HDPE piping to drain storm water into the existing reagent preparation building trench system.
- f. Area lighting and convenience power at the FGD Additive system is included. Local panels for distributing power, lighting, and heat tracing will be installed.
- g. Supplemental steel for pipe and raceway supports will be provided. An allowance of 5 tons of supplemental steel is included in the design.
- 4. Instrumentation and Controls New instrumentation, control devices, and automated valves will be installed for the new reagent preparation systems.
 - a. Instrumentation to monitor, control, and protect the pre-crushing and grinding process equipment will be provided.
 - b. New instrumentation will be provided to monitor the additive tank levels and temperatures. The additive feed pumps will include remote start capabilities.
 - c. A new remote I/O (RIO) cabinet will be installed in the PDC. The new RIO cabinet will interface with the existing DCS via a fiber optic link. An allowance for 500' of fiber optic cable for interfacing with the existing DCS is included in the design.
- Power Supply The power supply to the reagent preparation area will be fed from spare compartments in the existing 4160V lineups (24SR-1 and 24SR-2) to support the new power supply system, the following scope will be performed.
 - a. Electrical studies (load flow, short circuit analysis, relay coordination, and arc flash) will be performed to support detail design and engineering activities. New arc flash labeling will be provided where personnel protection levels are higher than existing labeling.
 - b. Two spare 4160V compartments will be utilized to energize each reagent handling and preparation system. Two compartments will be utilized from 24SR-1 and two spare compartments will be utilized from 24SR-2. One of the compartments on each existing lineup will be utilized to power a 1000HP VTM motor and the other compartment will feed a 4160V x 480V transformer that will supply the remaining power distribution requirements in the reagent handling and preparation areas. Each 4160V compartment (four compartments total) will have new 4160 breakers and SEL relays installed (feeder protection or motor protection as required).
 - c. The 480V and under power distribution system will be installed in a prefabricated Power Distribution Center (PDC) to be located adjacent the new VTM enclosure. The primary lineup will include outdoor 4160V x 480V liquid filled step down transformers and an open transition tie breaker between each train's 480V equipment. Transformers will be installed per NEC code and applicable regulations (e.g., fire detection/protection). The low voltage power distribution system will include LV MCCs, load centers, and lighting panels. The PDC will be equipped with HVAC, lighting, convenience outlets, and two doors.

- d. New foundations for the transformers will be installed. The PDC will sit on elevated piers to allow for bottom entry and exit of cabling.
- 6. Cabling and Raceways New cables and raceways will be installed to energize, monitor, and control new equipment that will be installed. Connections to the existing plant ground grid are included.
 - a. Medium voltage power cabling will be installed overhead from the FGD electrical room to the new PDC. The VTM motor cables will be routed overhead in the new VTM enclosure. Low voltage (LV) duct banks will be installed from the transformers to the PDC and from the PDC to the VTM enclosure. Low voltage power cabling will be installed from the PDC to the new reagent handling equipment, the new reagent preparation area users, and the FGD Additive system. A new ground grid will tie into the existing grid.
 - b. New instrument and control cabling will be installed from reagent preparation area equipment to a new RIO cabinet in the PDC.
 - c. New cable trays will be installed for power, instrument, and control cabling. Metal conduit and flex conduit will be used for final drops to equipment and other end users.
 - d. Supplemental steel for raceway supports will be designed and installed.
 - e. Foundations for raceway support steel will be installed at grade.
- 7. Demolition The existing reagent preparation building will be cleaned of lime dust accumulations. The Lime slurry tank agitator and two tank baffles will be removed.

3.3.3 FGD Area

The recycle slurry system receives the limestone slurry product from the reagent prep system where it is sprayed into the absorbers for SO_2 removal. Recycle slurry pumps recycle the limestone slurry in a closed loop spray tower. Absorber trays installed in the cross-section of the towers create pressure drop (dP) for enhanced SO2 removal as the limestone slurry collected on these trays passes through the perforations in the tray.

The mist eliminator system installed above the recycle slurry spray nozzles is designed to remove carryover (moisture) from the exiting flue gas. The mist eliminator system includes an integrated wash header system designed to clean the surfaces of the mist eliminators with wash water.

- 1. Recycle Slurry System To achieve the desired SO₂ removal objectives, the following modifications will be made to increase the system L/G ratio and overall absorber slurry spray coverage.
 - Absorber recycle pump refurbishments (overhaul) to restore pumps to like-new conditions. Modifications (e.g., resheaving) to recycle pumps to optimize flow and pressure on the lower spray headers. Automated flush controls will be added for the recycle pumps.
 - Two new 316L spray headers will be installed on each module (six headers total). The main inlet trunk diameter will be 30" and each header will be equipped with 128 silicon carbide slurry nozzles. A new 30" 316L penetration spool will be provided for each header.
 - c. A new 316L internal support truss will be designed and installed to support the lower recycle header trunk. The existing truss will be used to support the upper recycle header trunk. New 316L box beam supports will be designed and installed for the upper and lower header branches.
 - d. The existing 20" external recycle piping will be replaced with 30" FRP piping and a new cross-tie (manifold) to allow four pumps to feed both spray elevations. New pipe supports are included.
 - e. Supplemental steel for the new external recycle piping supports will be designed and installed.
 - f. New 316L absorber tray dP taps will be installed on each absorber (six taps total) so that the tray dP can be manually measured during system startup. The taps will be 2" diameter and will include a manual ball valve.
 - g. 316L strips of 11-gauge sheet metal will be welded onto the existing tray to reduce the open area of tray surface. The strips will be installed as evenly/symmetrically as possible across the tray surface to promote even gas/liquid distribution.

- h. Replace existing emulsified sulfur system as the existing has reached the end of its serviceable life.
- 2. Mist Eliminator (ME) System The ME system will be modified to improve the wash intensity on the MEs by increasing the wash water pressure from 20-30 psi to 40-50 psi.
 - a. The two existing service water pumps will be replaced to achieve desired wash conditions at the ME wash nozzles. The new pump duty point will be approximately 2000 gpm at 250' TDH. The new pump motor horsepower is estimated to be 250 HP. Two additional Lakos filters and six filter pods will be added to improve reliability and availability of the service water filtration system. Associated piping and isolation, flush, and drain valves are included. The additional filters will be installed in the location of the existing ME wash water blend station (adjacent to the two existing Lakos Filters). The new arrangement will have three operating filters and one spare filter.
 - b. The existing 5" ME wash piping sections will be replaced with approximately 210' of 6" 316L SS piping. New pipe supports are included.
 - c. Supplemental steel for the new ME wash pipe supports will be designed and installed. An allowance of 5 tons of supplemental steel is included in the design.
 - d. The two existing service water pump foundations will be modified to accommodate the new service water pumps. Foundations for the new Lakos filters and associated pipe supports will be installed.
 - e. New ME wash nozzles will be installed on the upper "C" module wash header after the existing nozzle extensions are removed. 248 nozzles will be installed. The nozzles will be replaced in kind.
 - f. The existing ME wash logic and sequencing will be modified.
 - g. Upgrade and replacement of portions of existing Lakos filter blowdown piping due to excessive erosion.
 - h. Three new on/off isolation valves will be installed for each wash zone header for improved operational and maintenance flexibility.
 - i. A new Gravity Filter Bank for the ME system is included. The new filters will be used to support filtering stability to the ME wash station, preserve FGD chemistry and density.
- 3. Slurry Bleed and Level Control The control logic for the absorber density and level controls will be modified so that reaction tank density will be controlled by batch operation (on/off) with the existing bleed valves. New automated flush valves, piping, and restriction orifices will be installed. In addition, controls will be modified such that reaction tank liquid level will be maintained by addition of CRW makeup water (see section 3.3.4.3 for more CRW makeup water details).
- 4. Instrumentation and Controls The following instrumentation, devices, and services will be provided for the FGD area.
 - a. The absorber recycle density meters on each module (three meters total) will be removed prior to demolition of external recycle piping. After the new 30" recycle piping is installed, the existing density meters will be reinstalled near the original location using new mounting hardware. Existing instrument cabling will be reused. If additional cabling is necessary to access density meter terminations, a junction box and new instrument cabling will be installed (no cable splices).
 - b. New 6" magnetic flow meters (three flow meters total) and 6" ME wash valves (twelve valves total) will be installed in each absorber's new 6" mist eliminator wash piping near their original location. Existing instrument cabling will be reused. If additional cabling is necessary to access flow meter and valve terminations, a junction box and new instrument cabling will be installed (no cable splices).
 - c. New recirculation valves will be installed on each service water pump (two recirculation valves total). It is assumed the existing pipe support system is adequate for the valve addition.
 - d. A new pressure transmitter will be installed in the common service water pump discharge piping for recirculation valve control.
 - e. One portable ship loose differential pressure gauge will be provided for each module (three gauges total). The gauges will be utilized for monitoring absorber tray dP during startup post limestone conversion.

- 5. Cabling and Raceways New cables and raceways will be installed to energize, monitor, and control new equipment that will be installed. Connections to the existing plant ground system are included.
 - a. New cabling will be installed for the service water pump recirculation valves and the pressure transmitter.
 - b. Cabling for the service water pump recirculation (automated valves and pressure transmitter) will be ran in new conduit.
- Power supply Existing service water pump cabling will be reused based on the one-line drawing (SLD20D27) stating the existing infrastructure is designed for 250 HP. If additional cabling is necessary to access pump motor terminations, a junction box and new power and control cabling will be installed (no cable splices).
- 7. Demolition The existing 316L recycle headers, penetration nozzles, and internal box beams will be removed from the absorbers. Portions of the external FRP recycle piping (20" diameter sections) will be removed along with associated pipe supports and supplemental steel. The 5" ME wash piping, flow meters, and automated valves will be removed to accommodate the new 6" ME wash piping. The 248 ME wash riser extensions on the "C" module upper wash header will be removed. The existing service water pumps and recirculation restriction orifices will be removed. The existing ME wash water blending station valves and piping will be demolished and the CRW and service water piping reworked to make room for the two new Lakos filters and Zero Gravity filter pods.

3.3.4 Dewatering Area

Solids accumulated in the absorber tower sumps are pumped to the dewatering area for removal from the FGD system by means of two-step dewatering. Primary dewatering is achieved by means of a thickener which receives the slurry blowdown from the FGD area. Solids accumulated in the center well of the thickener (thickener underflow) are pumped to the secondary dewatering area and the thickener overflow is collected in the CRW tank.

Secondary dewatering is achieved by means of drum filters. Thickener underflow is first received and stored in the existing WSP surge tank, then pumped to drum filters for dewatering. The filter cake is stabilized in existing pugmills where the filter cake is blended with fly ash, lime, and water from a chloride purge stream. Final blended cake is disposed of consistent with current operations.

- 1. Primary Dewatering The primary dewatering will be modified as below for the conversion to limestone reagent.
 - a. The existing FGD Sludge Tank (thickener underflow tank) mixer will be replaced with a new agitator. The agitator oil pump will be a shaft driven style oil pump to allow for agitator lubrication when the agitator is required to operate on essential power.
 - b. The existing mixer support structure will be reinforced with additional supplemental steel and two baffles will be installed in the tank.
 - c. The thickener underflow pump controls will be modified to facilitate consistent, automatic control of the underflow slurry density at the desired operational setpoint.
 - d. The lining system of the FGD Sludge Tank will be replaced with a flake glass lining.
 - e. Automated flush control valves will be added for flushing the thickener underflow pumps and piping.
- 2. Secondary Dewatering The secondary dewatering system will be modified as below for reagent conversion project.
 - a. The existing WSP Surge Tank mixer will be replaced with a new agitator.
 - b. The existing mixer support structure will be reinforced with additional supplemental steel and two baffles will be installed in the tank.
 - c. New 316L chloride purge piping will be installed on the discharge of each filtrate pump (four pumps total). The piping will be manifolded together and routed to a new chloride purge spray bar at the pug mill for blending with waste disposal product material. Each purge line will be equipped with an automated valve and a downstream block valve. Approximately 140' of 2.5" and 60' of 1.5" piping will be installed.

- 3. Instrumentation and Controls
 - a. The following devices will be installed as part of the chloride purge addition: A new automated valve will be installed in the discharge piping of each of the four existing filtrate pumps (four valves total). A flow meter will be installed to control a modulating valve on the chloride purge header to the pug mill.
 - b. Eight new automated valves and associated piping will be installed as part of the absorber density using CRW.
- 4. Power Supply, Cabling and Raceways New motor starters, cables, and raceways will be installed to energize, monitor, and control new equipment that will be installed.
 - a. Space in existing dewatering area MCCs (thickener and WSP) will be configured for Size 4 MCC buckets to power the new dewatering area agitators. The WSP MCC will not require any loads to be relocated to accommodate a size 4 bucket. The thickener area MCC will require relocating some loads to accommodate a size 4 bucket. New size 4 starters will be provided. New power and control cabling will be installed from the new motor starters to new agitators.
 - b. New instrument and control cables will be installed for the new chloride purge devices and the CRW density control.
 - c. New raceways will be installed for power, instrument, and control cabling. Metal conduit and flex conduit will be used for final drops to end users.
 - d. Supplemental steel will be designed and installed for the new cable trays.
- 5. Demolition The Sludge Tank Mixer and the WSP Surge Tank Mixers will be removed to accommodate the new agitators.

3.3.5 Balance of Plant (BOP)

- 1. A laser scan will be performed of selected project areas to optimize pipe routing and equipment arrangements.
- 2. A geotechnical investigation will be performed in the area of the new vertical milling system to identify the foundation design requirements for this area.
- 3. An English Language Control Description (ELCD) for the DCS supplier (Emerson Ovation) to make programming changes to existing systems and programming for new systems.

4. System Operations

The concept AECOM developed for LSIO operation reuses some existing equipment and infrastructure where possible to minimize the capital cost associated with a process retrofit. A process flow diagram (PFD) of the proposed configuration is provided in Figure 4-1. The process lines and equipment in red represent new scope and construction items. All other process lines and equipment in black reflect existing equipment or piping that will be reused or repurposed. The PFD with associated material balance for limestone operation is provided as Appendix B.





4.1 LSIO Operation

LSIO operation will require an increase in L/G to achieve the desired SO₂ removal efficiency of 98% without requiring excessively high sodium formate usage. All four of the existing slurry pumps will operate at an approximate flow of 12,500 gpm each (50,000 gpm total per absorber) to achieve an L/G of 64 gal/kacf. Modifications to pump speed via new belts and sheaves and modifications to the existing recycle piping to reduce system friction losses will be required to allow the existing pumps to achieve these flows.

New spray headers designed with improved spray coverage will be installed to distribute the slurry over the absorber cross section at each of the two existing spray levels. Comparison of the existing spray coverage to the proposed new spray coverage is illustrated in Figure 4-2. The images represent spray coverage at 18-inches below the nozzles. A schematic of the new spray header design is provided in Appendix A. Tray strips will also be added to the existing tray to achieve a pressure drop across the tray of approximately 3.0 IWG at design conditions. Improvements to spray coverage and an increase in tray pressure drop will both provide mass transfer benefits that appropriately balance capital investments with operational expenditures.



Figure 4-2: Current Versus Proposed Absorber Recycle Spray Pattern

Calcium sulfite solids will continue to be produced with LSIO operation. These solids will be purged from the individual reaction tanks based on density feedback control to target 15% suspended solids in the reaction tanks rather than the current control scheme that uses tank level as the control variable. To maintain slurry velocity in the existing bleed piping, the bleed will operate on a batch rather than continuous basis at roughly the same flow rate. The existing bleed valves will open when a high density set point has been reached in the reaction tank and will remain open until a low density setpoint has been achieved. The bleed piping will be flushed with clarified recirculating water (CRW) after the bleed valve has closed. At full load operation, the bleed will operate for approximately 20 minutes of every hour. The existing density meters will be used to control the batch bleed process. Tank level will be used to control the addition of CRW as makeup to the reaction tank.

The solids purged from the reaction tank will be transported in the existing bleed piping to the thickeners for primary dewatering. Consistent with current operations, overflow from the thickener will be collected in the CRW tank along with FGD system makeup water. The thickener will be operated such that the underflow slurry contains nominally 30% suspended solids. The underflow will be collected in the existing thickener underflow (TUF) sludge tanks for subsequent transfer via the waste slurry processing (WSP) sludge tank to the drum filters. The improved dewatering properties of the sodium sulfite solids associated with the LSIO conversion (as described in Section 2.0) will result in improved performance for the drum filters. Based on LSIO conversions at other facilities, AECOM predicts the drum filter cake to contain nominally 65% solids. The existing filtrate pumps that transfer filtrate to the filtrate storage tank appear to have marginal capacity for the increased filtrate production associated with the reduced cake moisture. AECOM will perform an assessment during detailed design, but at this time assumes the filtrate pumps have adequate capacity for the new duty. As such, the only modifications necessary for the secondary dewatering system are replacement agitators in the TUF and WSP Sludge Tanks to keep the more readily dewatered calcium sulfite solids in suspension. Operation with 2 or 3 drums in service will continue, dependent upon cleaning and maintenance schedules.

Stabilization operations will continue with use of the existing pugmill to combine filter cake from the drum filters with fly ash and lime. A chloride purge stream will be added to the pugmill to control chlorides within FGD system metallurgical limits. A slipstream of drum filter filtrate will be diverted to the pugmill and distributed via spray bar to promote mixing with the filter cake, lime, and fly ash. AECOM estimates a chloride purge flow of approximately 75 gpm will be required to maintain FGD system chloride concentration below 7,000 ppm. The blended cake will be collected and disposed consistent with current operations.

4.2 Reagent Prep and Storage

The existing barge unloading system will undergo minor modification to be repurposed for limestone unloading. The existing lime conveyance equipment and storage silos will also undergo modifications to be repurposed for limestone handling and storage.

The existing vertical ball mill slaking system will be demolished. New feeders and transfer conveyors will transport limestone rock to a new grinding building constructed to the southeast of the existing slaker building. A new precrusher will reduce the size of the incoming limestone to 80% passing 5 mesh (4.25mm); the resulting product will gravity feed new vertical ball mills (VTMs). The VTMs are designed to reduce the size of the pre-crushed limestone to 90% passing 325 mesh. The limestone slurry from the VTMs will be discharged to the existing lime slurry storage tank. The lime slurry storage tank will be outfitted with a new agitator to keep the limestone slurry in suspension while stored in the tank. The remainder of the reagent storage and delivery system will be reused as is.

4.3 Chemical Additive and Storage

An FGD buffer additive will be required to meet the desired SO₂ removal efficiency upon converting to use of limestone reagent. For LSIO operation, sodium formate is the most cost-effective performance additive. Approximately 1,000 ppm of sodium formate will be required at design fuel conditions when targeting 98% SO₂ removal with three absorber towers in service.

Addition of sodium formate will require the addition of one new sodium formate tank and two additive feed pumps. The storage tank will be installed outdoors adjacent to the existing slaker building while the feed pumps will be installed within the existing slaker building. The tank is sized with a nominal capacity of 29,000 gallons equivalent to 14 days of use at full load operation. An alternative location for the storage tank inside the existing slaker building is under evaluation by Duke Energy and AECOM. The existing emulsified sulfur storage and delivery system will be replaced as it has reached end of service.

4.4 Mist Eliminator Wash System

The ME wash system will be upgraded to improve the quality of the wash with respect to wash intensity, wash pressure and wash duration. The existing ME wash headers will be reused as is. The design of the headers provides greater than 150% wash coverage across the ME surfaces, which is adequate for LSIO operation. However, the existing service water pump can only provide about 20-30 psig of wash pressure at the mist eliminator elevation. Typically, ME wash is delivered at 40-50 psig to ensure adequate force is applied with the wash water to dislodge solids that accumulate. Operation of the existing East Bend ME wash headers at around 50 psig will provide approximately 1,000 gpm of flow per header and increase wash intensity (gpm/ft2) to nearly 1.5 gpm/ft2 which is consistent the Electric Power Research Institute (EPRI) recommendations.

A new service water pump will be provided to generate at least 40-50 psig and approximately 1,000 gpm at the ME elevation for improved wash pressure and intensity. Piping of larger diameter will be retrofit to the ME wash supply to minimize friction loses with the increased flow. The ME wash sequence will also be modified to achieve a 60 second wash for each ME zone once per hour at full load conditions. These control system modifications are necessary to maintain the FGD system water balance. ME wash system reliability will also be improved with the addition of two new Lakos filters installed in parallel with the existing Lakos filters to create a 3+1 arrangement (4 x 33% capacity) filtration system.

5. Contract and Procurement Execution Approach

The project contracting and procurement execution approach assumes one entity providing execution of the scope of work under and EPC contract. The procurement and subcontracting WBS is provided in Table 5-1.

Table 5-1: Procurement and Subcontracting WBS

WBS Area	Package Number	Description
Common	81.112	Site Laser Scan
Common	81.110	Site Survey
Common	81.115	Geotechnical Investigation
Common	81.010	General Construction
Material Handling	63.000	Flowability Study
Material Handling	72.252	Conveyor System
Limestone Prep	71.114	Cranes and Hoists
Limestone Prep	72.250.1	Vertimill
Limestone Prep	72.250.2	Pre-Crusher
Limestone Prep	72.272	Dust Collector
Limestone Prep	73.300	Power Distribution Center (PDC)
FGD	81.008	Absorber Recycle Pump Refurbishment
FGD	72.229	Mist Eliminator Wash Filters (Lakos and Pods)
FGD	72.214	Recycle Piping, FRP (External)
FGD	72.200	Mist Eliminator Wash Nozzles
FGD	72.202	Recycle Spray Nozzles
FGD	72.212	Alloy Material, Recycle Spray Headers (Internal)
FGD	72.216	Recycle Pipe Supports (External)
Dewatering	72.246	Agitators

The division of responsibilities for the EPC works is outlined in Table 5-2 to establish various stakeholders' roles and responsibilities throughout the project.

Table 5-2: LSIO Conversion Project Division of Responsibility

ltem	Description	Engineering and Design Services	Equipment and Material Supply	Installation and Erection
1	Site Laser Scan	SUB	N/A	N/A
2	Site Survey	SUB	N/A	N/A
3	Geotechnical Investigation	SUB	N/A	N/A
4	General Construction (GC)	AECOM	AECOM	AECOM
5	Flowability Study	SUB	N/A	N/A
6	Conveyor System	CS	AECOM	GC
7	Vertimill	VTM	AECOM	GC
8	Pre-Crusher	PC	AECOM	GC
9	Power Distribution Center	PDC	AECOM	GC
10	Recycle Piping	Recycle Piping AECOM / PIPE AECOM Ge		GC

Project number: 60724995

ltem	Description	Engineering and Design Services	Equipment and Material Supply	Installation and Erection
11	Recycle Pumps (Refurbishment)	PUMP	PUMP	Duke
12	Recycle Pumps (New Sheaves)	AECOM	GC	GC
13	Recycle Spray Nozzles	NZL	AECOM	GC
14	Recycle Pipe Supports	PIPE	AECOM	GC
15	Agitators	AGIT	AECOM	GC
17	Balance of Plant	AECOM	GC	GC
18	Site Road Improvements	DUKE	DUKE	DUKE
19	Demolition	AECOM	GC	GC
20	Commissioning	AECOM	N/A	N/A
21	Startup	AECOM	N/A	N/A
22	Performance Testing	AECOM	N/A	N/A

Prepared for: Duke Energy 60724995-East Bend LSIO Project_Rev3.docx

Duke Energy East Bend Station

Appendix A - General Arrangement Drawings



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PROJECT

East Bend WFGD Limestone Conversion Phase 1 Engineering Study EAST BEND STATION RT 338, 6233 Baever Rd Union, KY 41091-0142

CLIENT

Duke Energy 525 South Tryon Charlotte, NC 28202

http://www.duke-energy.com

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GENERAL ARRANGEMENT SITE PLAN

SHEET NUMBER



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PROJECT

East Bend WFGD Limestone Conversion Phase 1 Engineering Study EAST BEND STATION RT 338, 6293 Beaver Rd Union, KY 41091-0142

CLIENT

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60724995 SHEET TITLE

GENERAL ARRANGEMENT VERTIMILL ENCLOSURE

SHEET NUMBER

43'-0" 5'-2 13/16" 6'-6 1/8" 6'-6 1/8" 6'-6 1/8" 6'-6 1/8" 5'-2 13/16" 6'-6" ⊐∎¢-∎¢ -01 Þ ⊒⊫⇔ ≢₽ **-**Þ∎⊅ **⊨**∎⊕ -**d** ⊐⊫¢ ╞╋ € ¢ ∎¢ **₽**₽ - Call ⊨⊫⊅ ⊨ ╘╧╧ Ħ ¢ ╘╪ Ш ╺╋╋┥ ₩ ≢⇔ NEW 30" DIA PENETRATION SPOOL - TRUSS HSS 18"x6"x1/2" TYP. ⊨∎o -0= i 🔤 l∎o ¢∎ Þ ¢∎ ₽ **⊨**∎⇔-⊨∎¢ Þ∎⊅ **■** ∎¢ l 🔤 ⊯⇔ -de ⊧≣₽ -01 -¢∎ ⊒₽⊅ -01 Seff. - H Last saved by: RYAN RASMUSSEN(2024-03-21) Last Plotted: 2024-03-21 Filename: C:\USERS\RYAN RASMUSSEN\ONEDRIVE - AECOM\Z1_EXTRA ABSORBER INTERNAL SPRAY HEADER PLAN VIEW Scale 3/8"=1'-0

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NOTES: 1. PIPING MATERIAL SPECIFICATION PN01SD1B02 2. QTY 1 SHOWN; 6 REQUIRED



PROJECT

East Bend WFGD Limestone Conversion Phase 1 Engineering Study EAST BEND STATION RT 336, 6293 Beaver Rd Union, KY 41091-0142

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PROJECT

East Bend WFGD Limestone Conversion Phase 1 Engineering Study EAST BEND STATION RT 338, 6293 Beaver Rd Union, KY 41091-0142

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KEY PLAN

PROJECT NUMBER

60724995 SHEET TITLE

GENERAL ARRANGEMENT SECONDARY DEWATERING

SHEET NUMBER



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Appendix B - PFD and Material Balance



Proprietary Information – Subject to Duke Energy/AECOM Confidentiality Agreement

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Duke East Bend Unit 2

Mass Balance - Limestone, Full Load, 600MW

5.67 lb SO2/MMBtu Inlet, 0.113 lb SO2/MMBtu Stack Outlet

Refer to PFD drawing #101

	Stream No.	101	102	103	104				
	Description	Booster Fan Outlet	Inlet Flue Gas per Abs.	Outlet Flue Gas per Abs.	Total Gas Out				
Flow, acfm		2,749,086	916,362	745,253	2,244,767				
Flow, lb/hr		8,327,832	2,775,944	2,915,141	8,745,424				
H2O, lb/hr		372,535	124,178	275,896	827,689				
SO2, lb/hr		36,579	12,193	244	732				
SO2, ppmd		2,179	2,179	44	44				
HCl, lb/hr		506	169	0	0				
HCl, ppmd		53	53	0	0				
Ash, lb/hr		394	131	26	79				
O2, lb/hr		685,120	228,373	228,075	684,225				
O2, % dry		8.2	8.2	8.2	8.2				
Temperature, F		330	330	126	126				
Pressure, IWCG (psig)		8	8	5	3				

	Stream No.	200	201	202	301	303	305	306	308	400	401	402
	Description	Dry Reagent	Concentrated Additive	Reagent Feed	ME Wash	FGD Makeup Water	Make-up Water To Reagent Prep	Misc Seal Water	Vacuum Pump Seal Water	Absorber Bleed Stream	Primary OF to CRW Tank	Primary Dewatering UF
Flow, gpm	•		1.1	356	214	493	301	20	50	1,024	829	452
Flow, lb/hr		69,396	719	218,552	107,190	246,661	150,678	10,006	25,014	552,566	414,562	271,600
Total SS, lb/hr		67,384	0	65,436	5	25	6	0	1	82,885	1,538	81,480
Total SS, %		97.10%	0.00%	29.94%	0.00%	0.01%	0.00%	0.00%	0.00%	15.00%	0.37%	30.00%
pH			0.00	7.48	8.10	7.80	8.10	8.10	8.10	5.80	5.80	5.80
Specific gravity			1.26	1.23	1.00	1.00	1.00	1.00	1.00	1.09	1.01	1.22
H2O, lb/hr		2,012	431	153,116	107,185	246,636	150,672	10,005	25,013	469,681	413,023	190,120
CaCO3, lb/hr		59,031	0	59,037	5	0	6	0	1	2,383	44	2,342
CaSO4-2H2O, lb/hr		0	0	0	0	0	0	0	0	0	0	0
CaSO3-1/2H2O, lb/hr		0	0	0	0	0	0	0	0	73,636	1,367	72,388
Fly Ash, lb/hr		0	0	0	0	0	0	0	0	321	6	316
Inerts, lb/hr		6,399	0	6,399	0	25	0	0	0	6,545	121	6,434
Cl, lb/hr		0	0	4	3	3	4	0	1	3,273	2,770	1,325
Cl, mg/L		0 ppm	0	27	27	14	27	27	27	6,938	6,728	6,938
Mg, lb/hr		291	0	293	1	22	2	0	0	2,063	1,746	835
Mg, mg/L		4325 ppm	0	1,921	12	90	12	12	12	4,373	4,241	4,373
Sodium Formate, lb/hr		0	288	288	0	0	0	0	0	472	399	191
Sodium Formate, mg/L		0 ppm	500,530	1,884	0	0	0	0	0	1,000	970	1,000

	Stream No.	501	502	503	511	512	520	602	604	700	
	Description	Total Filtrate Water	Secondary Dewatering Product	Filtrate Purge	Fly Ash to Blending	Lime to Blending	Blended Product	CRW Pump Discharge	CRW to Absorber	Recycle Slurry Flow	
Flow, gpm		341		75				1,325	1,325	46,000	
Flow, lb/hr		171,523	125,092	37,927	39,039	4,372	206,430	661,223	661,223	24,825,225	
Total SS, lb/hr		172	81,310	38	39,039	4,372	124,759	1,563	1,563	3,723,784	
Total SS, %		0.10%	65.00%	0.10%	100.00%	100.00%	60.44%	0.24%	0.24%	15.00%	
pH		6.07		6.07				6.55	6.55	5.80	
Specific gravity		1		1.01				1.01	1.01	1.09	
H2O, lb/hr		171,351	43,782	37,889	0	0	81,671	659,660	659,660	21,101,441	
CaCO3, lb/hr		5	2,338	1	0	4,372	6,712	44	44	107,042	
CaSO4-2H2O, lb/hr		0	0	0	0	0	0	0	0	0	
CaSO3-1/2H2O, lb/hr		152	72,236	34	0	0	72,269	1,367	1,367	3,308,259	
Fly Ash, lb/hr		1	315	0	39,039	0	39,354	6	6	14,441	
Inerts, lb/hr		14	6,420	3	0	0	6,423	146	146	294,042	
Cl, lb/hr		1,056	270	233			503	2,774	2,774	145,959	
Cl, mg/L		6,180	2156 (ppm)	6,180			2438 (ppm)	4,218	4,218	6,938	
Mg, lb/hr		665	170	147		-	317	1,768	1,768	92,005	
Mg, mg/L		3,895	3,895	3,895			3,895	2,689	2,689	4,373	
Sodium Formate, lb/hr		152	39	34			72	399	399	21,037	
Sodium Formate, mg/L		890	890	890			890	607	607	1.000	

Appendix C - P&IDs





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PROJECT

East Bend WFGD Limestone Conversion Phase 1 Engineering Study EAST BEND STATION RT 338, 6293 Beaver Rd Union, KY 41091-0142

CLIENT

Duke Energy 525 South Tryon Charlotte, NC 28202

http://www.duke-energy.com

CONSULTANT

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PROJECT NUMBER

60724995

SHEET TITLE

WFGD LIMESTONE CONVERSION P&ID

MATERIAL HANDLING SHEET NUMBER



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NOTES: 1. DETAILS NOTED ON THIS SHEET TYPICAL FOR TWO PROVIDED SYSTEMS. 2. TRAMP METAL DETECTOR WILL BE INTERLOCKED WITH TRANSFER CONVEYOR MOTOR.

LIMESTONE DUST TBD TBD TO LIME SLAKER BLDG DUST COLLECTION SYSTEM

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LIMESTON	E DUST					
TBD	TBD					
TO VERTIMILL DUST COLLECTION SYSTEM						
	LIMESTONE					
TO VERTI	MILL GRINDING MILL 1					

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PROJECT

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PROJECT NUMBER

60724995

SHEET TITLE

WFGD LIMESTONE CONVERSION P&ID

MATERIAL HANDLING

SHEET NUMBER 60724995-DI-SK-111



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NOTES: 1. THE DUST COLLECTOR IS COMMON TO BOTH MATERIAL HANDLING TRAINS. 2. DUST COLLECTOR SHOWN FOR EXISTING LIME SLAKER BUILDING. DRAWING SIMILAR FOR SECOND DUST COLLECTOR REQUIRED FOR PROPOSED VERTIMILL BUILDING

BUILDING. 3. VERTIMILL BUILDING DUST COLLECTOR WILL DRAIN TO VERTIMILL BUILDING SUMP.

AECOM

PROJECT

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PROJECT NUMBER

60724995

SHEET TITLE

WFGD LIMESTONE CONVERSION P&ID

DUST COLLECTION SHEET NUMBER



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PROJECT

East Bend WFGD Limestone Conversion Phase 1 Engineering Study EAST BEND STATION RT 338, 6293 Beaver Rd Union, KY 41091-0142

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PROJECT NUMBER

60724995

SHEET TITLE

WFGD LIMESTONE CONVERSION P&ID REAGENT PREP

SHEET NUMBER



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LIMESTON	E SLURRY	
F8	M-2814-2	
TO STOR	AGE TANK	

LIMESTONE SLURRY FLUSH 009 60724995-DI-SK-122 TO VERTIMILL BUILDING SUMP

LIMESTONE SLURRY FLUSH 008 60724995-DI-SK-122

PROJECT

East Bend WFGD Limestone Conversion Phase 1 Engineering Study EAST BEND STATION RT 338, 6293 Beaver Rd Union, KY 41091-0142

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SHEET TITLE

WFGD LIMESTONE CONVERSION P&ID REAGENT PREP

SHEET NUMBER



KyPSC Case No. 2024-00152 Exhibit 4 Page 39 of 78



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LIMESTO	NE SLURRY FLUSH	
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TO STOR	AGE TANK	



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PROJECT NUMBER

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WFGD LIMESTONE CONVERSION P&ID REAGENT PREP

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KyPSC Case No. 2024-00152 Exhibit 4 Page 53 of 78 Duke Energy

Project number: 60724995

Appendix D - Electrical Load List

Duke East Bend Reagent Conversion Study Preliminary Load List

	REV NO.	REVISION	DATE	DOC:			ELECTRICA	L LOAD LIST				CONNEC	CTED HP				3725.50						
	A	Review	6/17/2022	CLIENT:			Duke	Energy				CONNEC	TED KVA				3554.40						
	В	Preliminary	7/18/2022	PROJECT:		Eas	t Bend Lime	stone Conver	rsion			CONNEC	TED KW				3198.96						
				JOB NUMBER:			606	80586				OPERAT	ING KVA				1553.43						
												vo	DLT				480						
												OPERATII	NG AMPS				1868						
					-																		
				TYPE (Motor,	CONT.			CONN	FULL			STATIC	CONN	CONN		OPERATING	VED	STARTER	BREAKER	CONTROL	DCS		
ITEM	ADEA	SYSTEM	DESCRIPTION	Feeder or	LOAD	1 or 3 PH	Voltage		LOAD	EFF	PF	JIANC KVA	K1/A	KW/	EACTOR		(V or NI)	SIZE	SIZE	STATION (HOA,	(V or NI)	FED FROM	COMMENTS
				Actuator)	AMPS				AMPS			KVA	NA	IX V V	TACION	KVA	(10114)	JIZE	JIZE	ETC)	(1011)		
1	Reagent	Reagent Prep	Vertimill A Drive Motor			3	4160	1000	121.1	0.95	0.9		871.5	784.3	0.8	697.2	N				Y	24-SR1	Existing breaker
2	Reagent	Reagent Prep	Vertimill B Drive Motor			3	4160	1000	121.1	0.95	0.9		871.5	784.3	0.0	0.0	N				Y	24-SR2	Existing breaker
3	Reagent	Reagent Prep	4160V x 480V TFMR1			3	4160		0.0	0.95	0.9				0.8		N				Y	24-SR1	Existing breaker - Feeds LS-MCC1
4	Reagent	Reagent Prep	4160V x 480V TFMR2			3	4160		0.0	0.95	0.9				0.8		N				Y	24-SR2	Existing breaker - Feeds LS-MCC2
5	Reagent	Reagent Prep	A Mill Recycle Pump	FVNR		3	480	25	34.0	0.95	0.9		28.2	25.4	0.8	22.6	N	2	50		Y	LS-MCC1	
6	Reagent	Reagent Prep	B Mill Recycle Pump	FVNR		3	480	25	34.0	0.95	0.9		28.2	25.4	0.8	22.6	N	2	50		Y	LS-MCC2	
7	Reagent	Reagent Prep	A Mill Product Tank Agitator	FVNR		3	480	15	21.0	0.95	0.9		17.4	15.7	0.8	14.0	N	2	40		Y	LS-MCC1	
8	Reagent	Reagent Prep	B Mill Product Tank Agitator	FVNR		3	480	15	21.0	0.95	0.9		17.4	15.7	0.8	14.0	N	2	40		Y	LS-MCC2	
9	Reagent	Reagent Prep	A1 Classifier Feed Pump	FVNR		3	480	50	65.0	0.95	0.9		54.0	48.6	0.8	43.2	N	3	150		Ŷ	LS-MCC1	
10	Reagent	Reagent Prep	A2 Classifier Feed Pump	FVNR		3	480	50	65.0	0.95	0.9		54.0	48.6	0.0	0.0	N	3	150		Y	LS-MCC1	
11	Reagent	Reagent Prep	B1 Classifier Feed Pump	FVNR		3	480	50	65.0	0.95	0.9		54.0	48.6	0.0	0.0	N	3	150		Y	LS-IVICC2	
12	Reagent	Reagent Prep	B2 Classifier Feed Pump	FVINK		3	480	50	65.0	0.95	0.9		54.0	48.6	0.0	0.0	N	3	150		Y V	LS-IVICC2	
13	Reagent	Reagent Prep	VTM-1 Lube System	FDR		3	480	3	4.8	0.95	0.9		4.0	3.0	1.0	4.0	N N		15	-	Y	LS-IVICCI	
14	Reagent	Reagent Prep	Pro Crusher 1			2	460	200	4.0	0.95	0.9		4.0	170 /	0.0	150.4	IN N	5	250	-	v v	LS-IVICCI	
15	Reagent	Reagent Pren	Pre-Crusher 2	EVNR		3	400	200	240.0	0.55	0.5		100.3	179.4	0.0	0.0	N	5	350		v	LS-MCC2	
10	Reagent	FGD Additive	FGD Additive Tank Heater	FUR		3	480	10	14.0	0.95	0.9		199.5	10.5	1.0	11.6	N	5	30		v v	LS-MCC1	7kW heater
18	Reagent	FGD Additive	FGD Additive Feed Pump 1	FDR		3	480	10	21	0.95	0.5		17	16	0.8	14	N		15		Y	LS-MCC1	Skid control panel
19	Reagent	FGD Additive	FGD Additive Feed Pump 2	FDR		3	480	1	2.1	0.95	0.9		1.7	1.6	0.0	0.0	N	-	15		Ŷ	LS-MCC1	Skid control panel
20	Reagent	Reagent Prep	Reagent Prep Lighting TFMR	FDR		3	480	100	124.0	0.95	0.9		103.0	92.7	0.7	72.1	N		200		N	LS-MCC1	
21	Reagent	Reagent Prep	Reagent Prep Convenience Power	FDR		3	480	100	124.0	0.95	0.9		103.0	92.7	0.5	51.5	N		200		N	LS-MCC2	
22	Reagent	Reagent Prep	Bridge Crane	FDR		3	480	20	27.0	0.95	0.9		22.4	20.2	0.5	11.2	N		50		N	LS-MCC2	
23	Reagent	Reagent Prep	Hydroclone Hoist	FDR		3	480	7.5	11.0	0.95	0.9		9.1	8.2	0.5	4.6	N		20		N	LS-MCC2	
24	Reagent	Reagent Prep	Ball Charge Hoist	FDR		3	480	7.5	11.0	0.95	0.9		9.1	8.2	0.7	6.4	N		20		N	LS-MCC1	
25	Reagent	Reagent Prep	Misc VTM Auxilaries 1	FDR		3	480	10	14.0	0.95	0.9		11.6	10.5	1.0	11.6	N		30		N	LS-MCC1	
26	Reagent	Reagent Prep	Misc VTM Auxilaries 2	FDR		3	480	10	14.0	0.95	0.9		11.6	10.5	0.3	2.9	N		30		Ν	LS-MCC2	
27	Reagent	Matl. Handling	Day Bin MOV1	ACT		3	480	3	4.8	0.95	0.9		4.0	3.6	1.0	4.0	N		15		Y	LS-MCC1	
28	Reagent	Matl. Handling	Day Bin MOV2	ACT		3	480	3	4.8	0.95	0.9		4.0	3.6	0.0	0.0	N		15		Y	LS-MCC1	
29	Reagent	Matl. Handling	Day Bin MOV3	ACT		3	480	3	4.8	0.95	0.9		4.0	3.6	0.0	0.0	N		15		Y	LS-MCC2	
30	Reagent	Matl. Handling	Day Bin MOV4	ACT		3	480	3	4.8	0.95	0.9		4.0	3.6	0.0	0.0	N		15		Y	LS-MCC2	
31	Reagent	Matl. Handling	Weigh Belt Feeder 1	FDR		3	480	1.5	3.0	0.95	0.9		2.5	2.2	0.8	2.0	N		15		Y	LS-MCC1	
32	Reagent	Matl. Handling	Weigh Belt Feeder 2	FDR		3	480	1.5	3.0	0.95	0.9		2.5	2.2	0.0	0.0	N		15		Y	LS-MCC1	
33	Reagent	Matl. Handling	Weigh Belt Feeder 3	FDR		3	480	1.5	3.0	0.95	0.9		2.5	2.2	0.0	0.0	N		15		Ŷ	LS-MCC2	
34	Reagent	Matl. Handling	Weigh Belt Feeder 4	FDR		3	480	1.5	3.0	0.95	0.9	+	2.5	2.2	0.0	0.0	N	2	15		Y	LS-MCC2	
35	Reagent	Matt Handling	Transfer Conveyor 1	FVNR		3	480	15	21.0	0.95	0.9	-	17.4	15./	0.8	14.0	N	2	40		Y	LS-IVICC1	l
30	Reagent	FGD Additivo	Heat Tracing			1	480	15	21.0	0.95	0.9		17.4	15.7	0.0	0.0	N N	2	40		ř N	LS-IVICC2	Lice existing shares
37	Reagent	Reagent Prop	Limestone Slurry Tank Agitator			2	400	20	27.0	0.95	0.9	+	22.4	20.2	0.0	17.0	IN N	2	50		IN V	25B2 2 (D2)	Replacing 10HP agitator
20	Dewater	Thickener	THE Sludge Tank Agitator			2	400	20	96.0	0.95	0.9	+	70.7	71.7	0.0	63.8	N N	2	200		r V	Existing MCC	Replacing 15HP agitator
40	Dewater	Filter Feed	WSP Surge Tank Agitator	FVNR		3	480	60	77.0	0.95	0.9	+	63.9	57.5	0.8	51.2	N	4	200	<u> </u>	Y	Existing MCC	Replacing 10HP agitator
24	Reagent	Reagent Prep	Limestone Slurry Tank Agitator - GB Heater	FDR		3	480	5	7.6	0.95	0.9	-	6.3	5.7	0.7	4.4	N	-	15		Ŷ	Existing MCC	Reuse existing cabling and breaker
25	Dewater	Thickener	Sludge Tank Agitator - GB Heater	FDR		3	480	5	7.6	0.95	0.9		6.3	5.7	0.7	4.4	N	-	15		Ŷ	Existing MCC	Reuse existing cabling and breaker
26	Dewater	Filter Feed	WSP Surge Tank Agitator - GB Heater	FDR		3	480	5	7.6	0.95	0.9		6.3	5.7	0.7	4.4	N		15		Ŷ	Existing MCC	Reuse existing cabling and breaker
27	Reagent	Reagent Prep	Limestone Slurry Tank Agitator - Lube Pump	FVNR		3	480	1.5	3.0	0.95	0.9	1	2.5	2.2	0.8	2.0	N	0	15		Ŷ	Existing MCC	Reuse existing cabling and starter
28	Dewater	Thickener	Sludge Tank Agitator - Lube Pump	FVNR		3	480	1.5	3.0	0.95	0.9		2.5	2.2	0.8	2.0	N	0	15		Y	Existing MCC	Reuse existing cabling and starter
29	Dewater	Filter Feed	WSP Surge Tank Agitator - Lube Pump	FVNR		3	480	1.5	3.0	0.95	0.9		2.5	2.2	0.8	2.0	N	0	15		Y	Existing MCC	Reuse existing cabling and starter
30	Reagent	Reagent Prep	PDC Auxilaries	FDR		3	480	25	34.0	0.95	0.9		28.2	25.4	0.7	19.8	N		50		N	-	Lighting, HVAC, etc
31	Reagent	ME Wash	Service Water Pump 2-1	FVNR		3	480	250	302.0	0.95	0.9		250.8	225.7	0.8	200.6	Ν	6	400		Y	2SR1-4B	Upgrade existing 200 HP pump
32	Reagent	ME Wash	Service Water Pump 2-1	FVNR		3	480	250	302.0	0.95	0.9		250.8	225.7	0.0	0.0	N	6	400		Y	2SR2-3C	Upgrade existing 200 HP pump
33	Reagent	Reagent Prep	Sump Pump A	FVNR		3	480	10	14.0	0.95	0.9		11.6	10.5	0.5	5.8	N	1	30		Y	LS-MCC1	
34	Reagent	Reagent Prep	Sump Pump B	FVNR		3	480	10	14.0	0.95	0.9		11.6	10.5	0.0	0.0	N	1	30		Y	LS-MCC2	
35	Reagent	Reagent Prep	Sump Agitator	FVNR		3	480	5	7.6	0.95	0.9		6.3	5.7	0.8	5.0	N	1	15		Y	LS-MCC1	
			TOTALS		ļ	L		3725.50					3554.40	3198.96		1553.43				I			Į

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KyPSC Case No. 2024-00152 Exhibit 4 Page 55 of 78 Duke Energy

Project number: 60724995

Appendix E - One Line Diagrams







WIRING DIAG. REFEFENCE	E2292	1. 5565 15	E2292 13	E 2292-14
SCHEMATIC REF. E2240 PAGE	AP098 - A & B		AB009-A & B	
KVA OR MOTOR RATING H.P.	7/5/10 MVA	<u> </u>	450	(1000) (65
BREAKER FRAME SIZE LAMPSI	2000	1200	1200	~ 1280
SERVICE	FODS AUX.TRANSF.2SR-1 INCOMING LINE	TRANSFORMER	ABSORBER Pump 2C-1	MCTOR

- 1		DITAN	- B 15/6 1 · 1											
	REV	DATE	JOB NO.	PROJECT TYPE	DES	DFTR	снкр	ENGR	APFD	DESCRIPTION		CALE: N	NONE	DES:
	2	12-21-12	EB201348AB-E	A\$-BUILT	MSA	GUV	DLM	DRC	DRC	FGD CONTROLS REPLACEMENT		WG TYPE:	WL	DFTR:
ľ										REVISED BY A&A	ENFRGY 🖉	OB NO:		CHKD:
ł	3	9-10-13	EB\$01343AB-E	A\$-BUILT	DLM	DLM	DLM	DRC	DRC	REPLACE ABS PUMP BREAKER PH1		ATE:		ENGR:
ľ	4A	3-1-24	60724995	PERMIT APP.		ww		DA		PERMIT APPLICATION	FILENAME: ebs_02_cge_s1d20b1.dgn			APPD:





KEY-	DIAGRAM: 11-2247-2	

RE	/ DATE	JOB NO.	PROJECT TYPE	DES	DFTR	снкр	ENGR	APPD	DESCRIPTION		ALE: NO	INE	DES:
2	12-21-12	EB201348AB-E	A\$-BUILT	MSA	GUV	DLM	DRC	DRC	FGD CONTROLS REPLACEMENT		G TYPE:	WL	DFTR:
									REVISED BY A&A	T TENERGY 🗠	B NO:		CHKD:
3	9-10-13	EB\$01343AB-E	A\$-BUILT	DLM	DLM	DLM	DRC	DRC	REPLACE ABS PUMP 3REAKER PH1		ATE:		ENGR:
4/	3-1-24	60724995	PERMIT APP.		ww		DA		PERMIT APPLICATION	⊣ FILENAME: ebs_02_cge_s1d20b2.dgn			APPD:



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NO.



PROJECT

Duke Energy East Bend Limestone Conversion East Bend

CLIENT

Duke Energy

CONSULTANT

AECOM Process Technologies 13640 Briarwick Dr Suiet 200, Building A Austin, TX 78729 512,454,4797 tel 512,419,6004 fax www.aecom.com



SK-E-100



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NOTES: 1. ALL WORK SHALL BE INSTALLED IN ACCORDANCE WITH PROJECT STANDARDS AND THE LATEST EDITION OF THE NATIONAL ELECTRICAL CODE.



PROJECT

Duke Energy East Bend Limestone Conversion East Bend

CLIENT

Duke Energy

CONSULTANT

AECOM Process Technologies 9400 Ambergien Boulevard Austin, Tx 78729 512.454.4797 tel 512.419.6004 fax www.aecom.com

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Project number: 60724995

Appendix F - Demolition Drawings



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Level46=entire bdr&tags; Level47=rev blk; Level=48=CG&E; Level49=PSI



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1 30X



1	E
NOTES	
NUTES:	
ITS: SLUDGE	
CODE: API-650 111H EL	THON ADD. 2
METAL TEMPERATURE 5"	
OAD: 90 MPH	
I: 1.25	
EXPOSURE: C	
DESIGN:	
SHE GLASS: D I = 1.25	-
USE GROUP: IL	
Ss VALUE: 20%	
S1 VALUE: 8%	
SION ALLOWANCE:	
1/10	
: 1/10 N/A	4
STRUCTURE: 0	
J. N/A	
TOP ANGLE: 0	
AL PRESSURE: ATMOS	PHERIC
AL PRESSURE: ATMOS	PHERIC
M ROOF LOAD: N/A	
LOAD: N/A	
WELD INSPECTION SPOT	PAY DEP ADI-650 SEC 812
FEICIENCY: 1.0	TAT FER AFT-050 SEC 0.1.2
HYDRO	STATIC
MATERIAL: A36 M	DD 3
I MATERIAL: A36 M	
TIPAL MATERIAL A36	
N: NONE	
IRDER: A36	
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HT TANK (NO ROOF)	CUNSTRUCTORS
HT TANK (NO ROOF) PROJECT: SLUDGE TANK REPLAC TANK # 2	EMENT

Anthony Pruske Project Engineer T: 512-924-7268 (c) E: anthony.pruske@aecom.com

AECOM 13640 Briarwick Dr. Suite 200 Austin, TX 78729 aecom.com

COMMONWEALTH OF KENTUCKY

BEFORE THE PUBLIC SERVICE COMMISSION

In The Matter of:

The Electronic Application of Duke Energy)Kentucky, Inc. for a Certificate of Public)Convenience and Necessity to Convert its Wet Flue)Gas Desulfurization System from a Quicklime)Reagent Process to a Limestone Reagent Handling)System at its East Bend Generating Station and for)Approval to Amend its Environmental Compliance)Plan for Recovery by Environmental Surcharge)Mechanism)

Case No. 2024-00152

<u>CERTIFICATE OF NOTICE AND PUBLICATION</u>

Pursuant to the Kentucky Public Service Commission's Regulation 807 KAR 5:001, Section 16(1)(b)(5), I hereby certify that I am Amy B. Spiller, President of Duke Energy Kentucky, Inc. (Duke Energy Kentucky or Company), a utility furnishing retail electric and gas service within the Commonwealth of Kentucky, which, on the 25th day of July 2024, will file an application with the Kentucky Public Service Commission requesting an order granting Duke Energy Kentucky a Certificate of Public Convenience and Necessity for the construction, and conversion of its existing Wet Flue Gas Desulfurization (WFGD) from a quicklime-based handling process to a limestone based handling process in order to continue to meet existing environmental regulations (Limestone Conversion Project). The Limestone Conversion Project will be located at the Company's East Bend Generating Station. Additionally, the Company is requesting an order authorizing Duke Energy Kentucky to recover the environmental compliance costs of the construction, conversion and operation of the Limestone Conversion Project through amending its Environmental Compliance Plan and its environmental surcharge through its Rate Schedule ESM as required by KRS 278.183, and as applicable KRS 278.020(1). Duke Energy Kentucky is proposing changes to its Environmental Surcharge Mechanism tariff sheet, K.Y.P.S.C. No. 19, Sheet No. 76 and notice

to the public of the filing of the application is being given in all respects as required by 807 KAR 5:001, Section 17 and 807 KAR 5:001, Sections 8(2)(c) and 9(2), as follows:

On the 25th day of July 2024, the notice to the public was delivered for exhibition and public inspection at Duke Energy's Erlanger Ops Center, 1262 Cox Road, Erlanger, Kentucky 41018 and the same will be kept open to public inspection at said office in conformity with the requirements of 807 KAR 5:001, Section 17(1)(a) and 807 KAR 5:011, Section 8(1)(a).

I further certify that more than twenty (20) customers will be affected by said change by way of an increase in their rates or charges, and that on the 10th day of July 2024, there was delivered to the Kentucky Press Association, an agency that acts on behalf of newspapers of general circulation throughout the Commonwealth of Kentucky in which customers affected reside, a notice of the Company's Application, including proposed rates for publication therein once a week for three consecutive weeks beginning on July 19, 2024. A copy of said notice is attached hereto as Exhibit A, and a list of newspapers of general circulation throughout the Commonwealth of Kentucky in which customers affected reside, is being attached hereto as Exhibit B. A certificate of publication of said notice will be furnished to the Kentucky Public Service Commission upon completion of same pursuant to 807 KAR 5:001, Section 17(3)(b).

Also, beginning on July 25, 2024, Duke Energy Kentucky posted on its website a complete copy of the Company's application and a hyperlink to the location on the Kentucky Public Service Commission's website where the case documents and tariff filings are available.

Given under my hand this 25th day of July 2024.

5 Miler

Amy B. Spiller President, Duke Energy Kentucky, Inc. 139 E. 4th Street Cincinnati, Ohio 45202

Subscribed and sworn to before me, a Notary Public, in and before said County and State,

this 25th day of July 2024.

Notary Public

My Commission expires: July 8,2027



EMILIE SUNDERMAN Notary Public State of Ohio My Comm. Expires July 8, 2027
CERTIFICATE OF SERVICE

This is to certify that the foregoing electronic filing is a true and accurate copy of the document being filed in paper medium; that the electronic filing was transmitted to the Commission on July 25^{th} , 2024; and that there are currently no parties that the Commission has excused from participation by electronic means in this proceeding.

John G. Horne, II The Office of the Attorney General Utility Intervention and Rate Division 700 Capital Avenue, Ste 118 Frankfort, Kentucky 40601

> /s/Rocco D'Ascenzo Counsel for Duke Energy Kentucky, Inc.

KyPSC Case No. 2024-00152 Exhibit 5 Page 5 of 8

Exhibit A

Notice of the Filing

NOTICE TO CUSTOMERS OF DUKE ENERGY KENTUCKY, INC.

RECOVERY BY ENVIRONMENTAL SURCHARGE OF DUKE ENERGY KENTUCKY, INC.'S AMENDMENT TO ITS 2021 AMENDED ENVIRONMENTAL COMPLIANCE PLAN

PLEASE TAKE NOTICE that Duke Energy Kentucky, Inc. ("Duke Energy Kentucky" or "Company") is filing with the Kentucky Public Service Commission ("Commission") on or about July 19, 2024 in Case No. 2024-00152, an Application pursuant to Kentucky Revised Statute 278.183 for approval of the construction of the Limestone Conversion Project (Project) located at its East Bend Generating Station ("East Bend") and an amendment of the Company's Environmental Compliance Plan to include the Project for the purpose of recovering the capital and operations and maintenance (O&M) costs associated with the Project through an increase in the environmental surcharge on customers' bills beginning March 1, 2025 under the Company's existing Rider ESM, also known as the environmental surcharge mechanism. The total capital cost of the Limestone Conversion Project in the Company's Amended Environmental Compliance Plan is estimated to be \$125.8 million.

Federal and state environmental regulations require Duke Energy Kentucky to build and upgrade equipment and facilities that produce energy from coal to operate in an environmentally sound manner. Specifically, the Company is seeking Commission approval of a Certificate of Public Convenience and Necessity for the construction and operation of the Project. This construction project requires an amendment of Duke Energy Kentucky's Amended Environmental Compliance Plan that was approved by the Commission in 2022.

Additionally, Duke Energy Kentucky is seeking an order approving the recovery of the costs of the Project through its Environmental Surcharge tariff. The Project is required for the Company to continue to comply with the U.S. Environmental Protection Agency's federal Clean Air Act, and other environmental requirements that apply to Duke Energy Kentucky facilities used in the production of energy from coal. The total capital cost of the Project for which the Company is seeking recovery at this time is estimated to be \$125.8 million. O&M costs related to the Project will be similar to O&M costs incurred today and are not distinguishable.

The impact on Duke Energy Kentucky's customers is estimated to be an increase of 1.0% for residential customers and 1.0% on average for nonresidential customers in 2025, 2.8% for residential customers and 2.7% on average for non-residential customers in 2026, 2.1% for residential customers and 2.1% on average for non-residential customers in 2027, 1.8% for residential customers and 1.7% on average for non-residential customers in 2028, and 1.8% for residential customers and 1.8% on average for non-residential customers in 2029. For a Duke Energy Kentucky residential customer using 1000 kilowatt hours per month (kWh/mo.), the initial monthly increase is expected to be \$1.32 during 2025, \$3.63 in 2026, \$2.72 in 2027, \$2.25 in 2028, and \$2.33 in 2029.

The rates contained in this notice are the rates proposed by Duke Energy Kentucky; however, the Kentucky Public Service Commission may order rates to be charged that differ from the proposed rates contained in this notice. Such action may result in rates for consumers other than the rates in this notice.

Any corporation, association, body politic or person with a substantial interest in the matter may, by written request within thirty (30) days after publication of this notice of the proposed rate changes, request leave to intervene; intervention may be granted beyond the thirty (30) day period for good cause shown. Such motion shall be submitted to the Kentucky Public Service Commission, P.O. Box 615, 211 Sower Boulevard, Frankfort, Kentucky 40602-0615, and shall set forth the grounds for the request including the status and interest of the party. If the Commission does not receive a written request for intervention within thirty (30) days of the initial publication the Commission may take final action on the application.

Intervenors may obtain copies of the application and other filings made by the Company by requesting same through email at <u>DEKInquiries@dukeenergy.com</u> or by telephone at (513) 287-4366. A copy of the application and other filings made by the Company are available for public inspection through the Commission's website at <u>http://psc.ky.gov</u>, at the Commission's office at 211 Sower Boulevard, Frankfort, Kentucky, Monday through Friday, 8:00 a.m. to 4:30 p.m., and at the following Company office: Erlanger Ops Center, 1262 Cox Road, Erlanger, Kentucky 41018. Comments regarding the application may be submitted to the Public Service Commission through its website, or by mail at the following Commission address.

For further information contact:

PUBLIC SERVICE COMMISSION COMMONWEALTH OF KENTUCKY P.O. BOX 615 211 SOWER BOULEVARD FRANKFORT, KENTUCKY 40602-0615 (502) 564-3940 DUKE ENERGY KENTUCKY 1262 COX ROAD ERLANGER, KENTUCKY 41018 (513) 287-4366

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Exhibit **B**

Listing of Newspapers Publishing Notice

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List of Newspapers in Duke Energy Kentucky Territory

Covington Kentucky Enquirer Falmouth Outlook Link NK Warsaw Gallatin County News Williamstown Grant County News

KyPSC Case No. 2024-00152 Exhibit 6 Page 1 of 2 KY. P.S.C. Electric No. 2 FourthThird Revised Sheet No. 76 Cancels and Supersedes ThirdSecond Revised Sheet No.

Duke Energy Kentucky, Inc. 1262 Cox Road 76 Erlanger, Kentucky 41018

Page 1 of 2

ENVIRONMENTAL SURCHARGE MECHANISM RIDER

APPLICABILITY

This rider is applicable to all retail sales in the Company's electric service area beginning with the billing month June 2018. Rate RTP program participants utilize the applicable portions of the Baseline Charge and Program Charge, as those terms are defined in Rate RTP, for this rider.

Standard electric rate schedules subject to this schedule are: Residential: Rate Schedules RS and RS-TOU-CPP Non-Residential: Rate Schedules DS, EH, SP, DP, DT, GSFL, TT, SL, TL, UOLS, NSU, SC, SE, and LED

RATE

The monthly billing amount under each of the schedules to which this rider is applicable, shall be increased or decreased by a percentage factor according to the following formula:

Environmental Surcharge Billing Factor = Jurisdictional E(m) / R(m)

DEFINITIONS

For all Plans:

- E(m) = RORB + OE EAS + Prior Period Adjustment + (Over)Under Recovery
- RORB = (RB/12)*ROR
- RB = the Environmental Compliance Rate Base, defined as electric plant in service for applicable environmental projects adjusted for accumulated depreciation, accumulated deferred taxes, accumulated investment tax credits, CWIP and emission allowance inventory.
- ROR = the Rate of Return on the Environmental Compliance Rate Base, designated as the cost of debt and pretax cost of equity for environmental compliance plan projects approved by the Commission.
- OE = the Operating Expenses, defined as the monthly depreciation expense, taxes other than income taxes, amortization expense, emission allowance expense and environmental reagent expense.
- EAS = proceeds from Emission Allowance Sales.

Issued by authority of an Order of the Kentucky Public Service Commission dated <u>October 12, 2023</u> in Case No. <u>2024-001522022-00372</u>. Issued: <u>October 27, 2023 July 25, 2024</u> Effective: <u>October 13, 2023 August 26, 2024</u>

Issued by Amy B. Spiller, President /s/ Amy B. Spiller

(N)

	KY. P.S.C. Electric No. 2 Fourth Third Revised Sheet No. 76
Duke Energy Kentucky Inc	Cancels and Supersedes
1262 Cox Road	Third Second Revised Sheet No.
76	<u></u>
Erlanger, Kentucky 41018	Page 2 of 2

DEFINITIONS (Contd.)

Prior Period Adjustment is the amount resulting from the amortization of amounts determined by the Commission during six-month and two-year reviews.

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(Over) or Under Recovery is a one-month "true-up" adjustment.

Plans are the environmental surcharge compliance plans submitted to and approved by the Kentucky Public Service Commission.

- (1) Total E(m), (the environmental compliance plan revenue requirement), is multiplied by the Jurisdictional Allocation Factor. Jurisdictional E(m) is adjusted for any (Over)/Under collection or prior period adjustment to arrive at Adjusted Jurisdictional E(m). Adjusted Jurisdictional E(m) is allocated to Residential and Non-Residential on the basis of Revenue as a Percentage of Total Revenue for the 12 months ending with the Current Month.
- (2) Residential R(m) is the average of total monthly residential revenue for the 12 months ending with the current expense month. Total revenue includes residential revenue, including all riders, but excluding environmental surcharge mechanism revenue.
- (3) Non-Residential R(m) is the average of total monthly non-residential revenue for the 12 months ending with the current expense month. Total revenue includes non-residential revenue, including all riders, but excluding environmental surcharge mechanism revenue, base fuel revenue and FAC revenue.
- (4) The current expense month (m) shall be the second month proceeding the month in which the Environmental Surcharge is billed.

SERVICE REGULATIONS, TERMS AND CONDITIONS

The supplying and billing for service and all conditions applying thereto, are subject to the jurisdiction of the Kentucky Public Service Commission, and to Company's Service Regulations currently in effect, as filed with the Public Service Commission of Kentucky.