



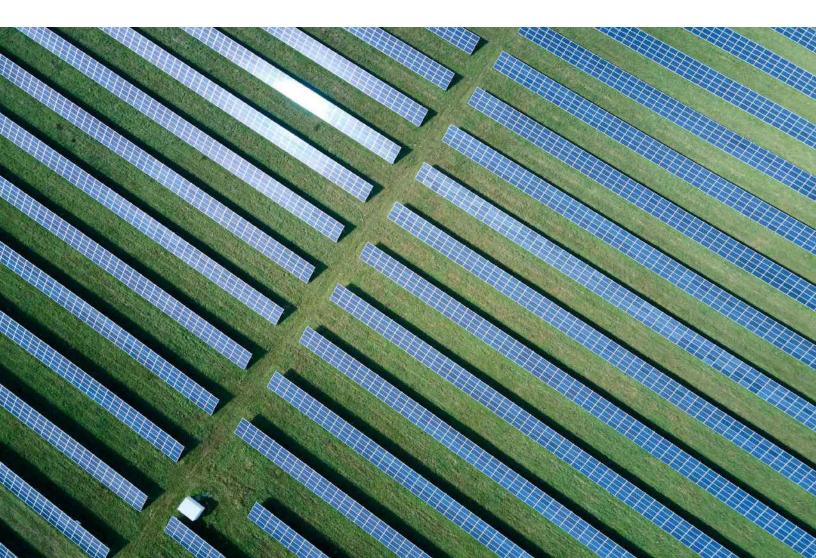
Acoustic Assessment Report

Lynn Bark Energy Center

PREPARED FOR Lynn Bark Energy Center, LLC

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REFERENCE 0718084



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ACRONYMS AND ABBREVIATIONS

AC	Alternating Current
ANSI	American National Standards Institute
dB	decibels
dBA	A-weighted decibels
DC	Direct Current
ERM	Environmental Resources Management, Inc.
Hz	Hertz
IEEE	Institute of Electrical and Electronics Engineers
ISO	Organization for Standardization
kVA	Kilo-volt Ampere
L _{eq}	The equivalent noise level
L _{dn}	The day-night noise level
Lmax	The maximum noise level
MVA	Mega-volt Ampere
MW	Megawatts
NSA	Noise Sensitive Area



1. INTRODUCTION

Lynn Bark Energy Center, LLC (Applicant) proposes to construct and operate the Lynn Bark (Project), a photovoltaic (PV) solar facility in Martin County, Kentucky. The Applicant has engaged Environmental Resources Management, Inc. (ERM) to conduct a noise assessment for the proposed Project.

This report presents the results of construction and operational noise predictions. The noise assessment was carried out to understand the noise levels that would be generated from the construction and operation of the Project. This report also provides general information on noise and comparisons of the expected Project noise levels to estimated existing ambient conditions and guidelines.

1.1 General Information on Noise

Noise is defined as unwanted sound. Excessive noise can cause annoyance and adverse health effects. Annoyance can include sleep disturbance and speech interference. It can also distract attention and make activities more difficult to perform (USEPA 1978).

The range of pressures that cause the vibrations that create noise is large. Noise is therefore measured on a logarithmic scale, expressed in decibels (dB). The frequency of a sound is the "pitch". The unit for frequency is hertz (Hz), or cycles per second. Most sounds are composed of a composite of frequencies. The human ear can usually distinguish frequencies from 20 Hz (low frequency) to about 20,000 Hz (high frequency), although people are most sensitive to frequencies between 500 and 4000 Hz. The individual frequency bands can be combined into one overall dB level.

Noise is typically measured on the A-weighted scale (dBA). The A-weighting scale has been shown to provide a good correlation with the human response to sound and is the most widely used descriptor for community noise assessments (Harris, 1991). The faintest sound that can be heard by a healthy ear is about 0 dBA, while an uncomfortably loud sound is about 120 dBA. In order to provide a frame of reference, ERM has listed some common sound levels below.

•	Chainsaw at 30 feet	90 dBA
•	Truck at 100 feet	85 dBA
•	Noisy Urban Environment	75 dBA
•	Lawn Mower at 100 feet	65 dBA
•	Average Speech	60 dBA
•	Average Office	50 dBA
•	Rural Residential During the Day	40 dBA
•	Quiet Suburban nighttime	35 dBA
•	Soft Whisper at 15 feet	30 dBA

Common terms used in this noise analysis are defined below.



- *L_{eq}* The equivalent noise level over a specified period of time (i.e., 1-hour). It is a single value of sound that includes all the varying sound energy in a given duration.
- L_{dn} the day-night noise level, is the A-weighted L_{eq} sound level over a 24-hour period with an additional 10 dB penalty imposed on sounds that occur between 10 p.m. and 7 a.m. to account for the increased sensitivity to noise during these periods.

1.2 Applicable Noise Standards

1.2.1 Noise Ordinances and Standards

No local noise ordinances or Commonwealth of Kentucky noise standards applicable to the Project were identified.

1.2.2 United States Environmental Protection Agency Guidelines

In 1974, the U.S. Environmental Protection Agency (USEPA) published its document entitled "Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin on Safety" (USEPA 1974). This publication evaluated the effects of environmental noise with respect to health and safety. The USEPA recommended in the document that environmental noise levels should not exceed a day-night sound level (L_{dn}) of 55 dBA. A 55 dBA L_{dn} noise level equates to a continuous sound level of 48.6 dBA (i.e., a facility that does not exceed a continuous noise level of 48.6 dBA for a 24-hour period will not exceed 55 dBA L_{dn}). This level was developed for "outdoor residential areas and farms and other outdoor areas where people spend widely varying amounts of time and other places in which quiet is a basis for use". The USEPA considers this level as protective of the public health and welfare from the effects of environmental noise and notes that this criterion was developed without regard to technical or economic feasibility and contains a margin of safety.

1.3 Project Description and Noise Sensitive Areas

The Project evaluated herein would be capable of generating up to 200 megawatts (MW) of electricity and would consist of an estimated 357,588 photovoltaic modules located on approximately 641 acres (array) within an overall project evaluation area of 1,514 acres (Project Boundary). The main noise generating components during the operational phase of the project include 51 direct current (DC) to alternating current (AC) power inverters, 51 auxiliary transformers, and one 150 megavolt-amperes (MVA) main step-up transformer. Noise sensitive areas (NSAs) consist of light density residential uses around the Project Boundary. A review of aerial photography identified 10 NSAs in proximity to the Project to be evaluated. NSA receptor locations, distances/directions from the property line of participating landowners, and distances to the nearest Project Boundary limits, solar panel, inverter, and substation are provided in Table 1 and depicted on Figure 1.



Receiver	Land Use Type	Approximate Distance (feet) to Nearest Project Structure			
		Project Boundary	Panel	Inverter	Substation
NSA 1	Residential	650	1067	1758	5458
NSA 2	Residential	2302	2536	3378	7366
NSA 3	Residential	2052	2633	3393	6616
NSA 4	Residential	3935	5583	5979	8550
NSA 5	Residential	1121	1931	2445	4995
NSA 6	Residential	2306	2443	2737	5586
NSA 7	Residential	872	2511	2838	5360
NSA 8	Residential	683	2264	2756	6932
NSA 9	Residential	407	1725	2375	7024
NSA 10	Residential	710	1652	2314	6963

Table 1. Noise Sensitive Area Receptors

2. EXISTING CONDITIONS

Existing sources of noise in the area likely include vehicular traffic noise from Kentucky Route 3, vehicular traffic on other roadways in the area, and natural sounds (e.g., birds and insects). Existing ambient noise levels in the area were estimated by evaluating the land uses in the area and the aforementioned noise sources. General ambient noise levels by land use have been estimated by the USEPA (USEPA 1978). However, a more detailed estimate is provided in American National Standards Institute (ANSI) standard 12.9-2013/Part 3 (ANSI 2013). The standard provides estimates of existing noise levels based on detailed descriptions of land use categories. The levels are in general agreement with those published by USEPA. The ANSI standard noise estimation divides land uses into six (6) distinct categories. These categories, their descriptions, and the estimated existing daytime and nighttime L_{eq} sound levels, are provided in Table 2.



Category	Land Use	Description	Estimated Existing Daytime L _{eq}	Estimated Existing Nighttime L _{eq}
1	Noisy Commercial and Industrial Areas	Very heavy traffic conditions, such as in busy downtown commercial areas, at intersections of mass transportation and other vehicles, including trains, heavy motor trucks and other heavy traffic, and street corners where motor buses and heavy trucks accelerate.	66	58
2	Moderate Commercial and Industrial Areas, and Noisy Residential Areas	Heavy traffic areas with conditions similar to Category 1 but with somewhat less traffic, routes of relatively heavy or fast automobile traffic but where heavy truck traffic is not extremely dense, and motor bus routes.	61	54
3	Quiet Commercial, Industrial Areas, and Normal Urban and Noisy Residential Areas	Light traffic conditions where no mass transportation vehicles and relatively few automobiles and trucks pass, and where these vehicles generally travel at low speeds. Residential areas and commercial streets and intersections with little traffic comprise this category.	55	49
4	Quiet Urban and Normal Residential Areas	These areas are similar to Category 3 above but, for this group, the background is either distant traffic or is unidentifiable.	50	44
5	Quiet Suburban Residential Areas	Isolated areas, far from significant sources of sound.	45	39
6	Very Quiet, Sparse Suburban or Rural Areas	These areas are similar to Category 5 above but are usually in unincorporated areas and, for this group, there are few if any near neighbors.	40	34

Table 2. Measured Sound Levels at the Noise Sensitive Area

Source: ANSI 2013

Existing ambient noise levels at the NSAs in the area were estimated utilizing the ANSI standard. Based upon a review of the land uses, the NSAs in the area are conservatively estimated to fall into a Category 6 land use (Very Quiet, Sparse Suburban or Rural Areas), with estimated daytime L_{eq} sound levels of 40 dBA and nighttime L_{eq} sound levels of 34 dBA.



3. NOISE MODELING

3.1 Operational Noise Modeling Methodology

ERM performed computer modeling to calculate noise levels that will be generated during Project operation and used the commercially available CadnaA model developed by DataKustik GmBH for the analyses (DataKustik GmBH 2006). The software has the ability to account for spreading losses, ground and atmospheric effects, shielding from barriers and buildings, and reflections from surfaces. The software is standards-based. ERM used the International Organization for Standardization (ISO) 9613 standard for air absorption and other noise propagation calculations (ISO 1996). ERM assumed a partially acoustically reflective ground surface (0.5 setting in the model). A setting of "0" corresponds to an acoustically reflective surface, such as pavement or water, while a setting of 1.0 corresponds to loose soils and grassy surfaces. ERM also included area topography. ERM did not account for any vegetation or foliage in order to develop a conservative assessment.

Modeling was conducted for daytime and nighttime operation with Project sources in operation at full load conditions. All sources were included for daytime operation. The inverters would not operate at night when no electricity is being produced, and inverter noise was therefore not included in the nighttime model. Discrete model receptors were placed at the location of the NSA locations. Noise contours were also produced such that noise levels at any location, including along the property line of participating landowners, could be visualized.

A summary of the equipment sources included in the noise modeling assessment and their height above grade is provided in Table 3. Table 4 provides the noise emissions data at maximum load and the derivation of each.

Equipment	Number of Each	Height Above Grade (feet)
Inverter	51	7.5
5 kVA Auxiliary Transformer	51	5
150 MVA Main Step-Up Transformer	1	13

Table 3. Equipment Source Listing

kVA = Kilovolt-amperes

Table 4. Noise Emissions Derivation for Project Sources

Equipment	Noise Emissions Data	Data Source/Vendor
Inverter	81 dBA at 3 feet	SMA ^a
5 kVA Auxiliary Transformer	59 dBA at 3 feet	IEEE
150 MVA Main Step-Up Transformer	82 dBA at 3 feet	IEEE ^b

^{a.} SMA Solar Technology AG



^{b.} Emissions data developed utilizing Institute of Electrical and Electronics Engineers (IEEE) Standard C57.12.90-2010 based on transformer MVA rating.

3.2 Operational Noise Model Results

Model results for Project operation with Project sources operating simultaneously at full load conditions are provided in Table 5 for both daytime and nighttime conditions at all NSA locations and at the Project boundary. The modeled levels are also compared to the estimated existing ambient conditions and to the USEPA's impact guideline. While the USEPA guideline is not a regulatory requirement, it is useful as a guide to evaluate potential noise impacts.

Receiver	Modeled Daytime Noise Level (dBA)	Estimated Daytime Ambient Condition (dBA)	Modeled Nighttime Noise Level (dBA)	Estimated Nighttime Ambient (dBA)	USEPA Recommended Protective Guideline (dBA)
NSA 1	14	40	2	34	48.6
NSA 2	8	40	0	34	48.6
NSA 3	8	40	0	34	48.6
NSA 4	18	40	4	34	48.6
NSA 5	20	40	5	34	48.6
NSA 6	14	40	3	34	48.6
NSA 7	10	40	0	34	48.6
NSA 8	11	40	0	34	48.6
NSA 9	18	40	7	34	48.6
NSA 10	13	40	2	34	48.6
Project Boundary ^a	56	40	38	34	48.6

Table 5. Noise Modeling Results

^a Highest modeled noise level for any location along the Project boundary line. No NSAs are present in this area.

As provided in Table 5, daytime operational noise levels at the NSA locations are shown to be very low, ranging from 8 dBA to 20 dBA, well below the estimated existing daytime ambient noise levels (40 dBA). Nighttime Project noise levels, with only the transformers in operation, were also very low, ranging from 0 dBA to 7 dBA. The existing topographical features result in significant shielding effects from the Project sources to the NSAs, resulting in very low modeled noise levels. Project generated noise levels for daytime and nighttime operation are well below the USEPA's recommended protective noise level of 48.6 dBA for 24-hour operation at the NSA locations.

The highest noise level modeled for any location along the Project Boundary is 56 dBA. This point on the Project Boundary is located on the east side of the Project and is approximately 0.4 miles from the nearest NSA (NSA 10). All modeled noise levels assume Project sources operating at full



load conditions. There will often be times when sources are operating at lower loads, with subsequently lower noise levels at the NSAs and the property line.

Noise contour maps depicting the modeled noise levels for daytime and nighttime operating conditions are provided in Figures 2 and 3, respectively.

3.3 Construction Noise

3.3.1 Pile Driving

A total of approximately 75,000 piles will be installed to support the solar panels. The installation of each pile occurs very quickly, typically requiring 90 seconds or less per pile. It is estimated that pile driving will occur over a period from August 1 to January 30, six days per week, during daylight hours.

Maximum sound level (Lmax) pile driving noise levels of 101 dBA at 50 feet were obtained from the Federal Highway Administration's Roadway Construction Noise Model. No usage factors were incorporated into the analysis so that Lmax sound levels would be calculated at the various distances rather than time-averaged sound levels.

Pile driving noise levels were modeled using the same methodology as utilized for the operational noise modeling, including the existing topographic features in the area. The modeled expected pile driving noise level at each NSA is provided in Table 6. The noise levels presented are for the nearest approach any one single pile driver will be to the respective NSA. As provided in Table 6, pile driving noise levels are shown to be below the estimated existing ambient condition at some NSA locations, due to the shielding effect provided by area topography. About half of the NSA locations are shown to have pile driving noise levels above ambient, and only when pile driving is occurring at the nearest approach to the NSA. Pile driving activity will occur over a very large area, and no one NSA will experience the same or a constant noise level. As piles are quickly installed, noise levels will decrease as piles are installed at greater distances away from an NSA. As a noise mitigation measure, no nighttime pile driving will be conducted, with pile driving scheduled to only occur between the hours of 8 a.m. and 8 p.m. Additionally, NSAs within 1,500 feet of where pile driving will occur will be notified prior to commencing construction.

Receiver	Maximum Pile Driving Noise from Nearest Pile Driver
NSA 1	47
NSA 2	38
NSA 3	37
NSA 4	42
NSA 5	44
NSA 6	39
NSA 7	41

Table 6. Maximum Expected Pile Driving Noise from Nearest Pile Driver (dBA)



Receiver	Maximum Pile Driving Noise from Nearest Pile Driver
NSA 8	39
NSA 9	43
NSA 10	41

3.3.2 General Construction

Construction typically includes the following phases:

- Site preparation
- Excavation
- Foundation Construction
- Building Construction
- Restoration/Finishing

The construction equipment utilized will differ from phase to phase but will include dozers, pile drivers, cranes, cement mixers, dump trucks, and loaders. Noise is generated during construction primarily from diesel engines, which power the equipment. Exhaust noise usually is the predominant source of diesel engine noise, which is the reason that maintaining functional mufflers on all equipment will be a requirement.

Table 1 provided the closest distance any NSA would be to a panel. However, the Project Boundary covers a very large area. The actual sound levels that will be experienced by NSAs surrounding the site during construction will be a function of distance and which equipment are in operation. As such, no single existing NSA will be exposed to the same sound levels over an extended period of time, as construction progresses through the site.

Construction noise transmitted from the site will be attenuated by a variety of mechanisms. The most significant of these mechanisms are the divergence of the sound waves with distance (attenuation by divergence), and the significant shielding effect of the existing topographical features. Additional reductions in noise are achieved through absorption by the atmosphere. Noise levels of construction equipment that may be used for the Project are summarized in Table 7 (FHWA 2006). Provided in Table 8 are the modeled noise levels for the range of construction equipment presented at each NSA location. General construction noise levels were modeled using the same methodology as utilized for the operational and pile driving noise modeling, including the existing topographic features in the area.



Table 7. Construction Equipment Noise Levels (dBA)

Facility and Trues	Maximum Sound Lev		
Equipment Type	50 Feet		
Cement Trucks	79		
Front End Loaders	79		
Graders	85		
Dozers	82		
Pickup Trucks	55		
Backhoes	78		
Concrete Mixers	79		
Air Compressor	78		
Dump Trucks	77		
Cranes	81		
Flatbed Trucks	74		
Pile Driver	101		

^a Source: FHWA, 2006

Table 8. General Construction Equipment Noise Assessment (dBA)

Receiver	Range of Construction Equipment Noise Levels Operating at Nearest Panel
NSA 1	1 to 31
NSA 2	0 to 22
NSA 3	0 to 21
NSA 4	0 to 26
NSA 5	0 to 28
NSA 6	0 to 23
NSA 7	0 to 25
NSA 8	0 to 23
NSA 9	0 to 27
NSA 10	0 to 25

General construction related noise levels will be lower than pile driving noise levels. As noted above, the project site covers a very large area, and the noise levels experienced at any NSAs will vary depending on what areas of the site are being constructed at any given time. It is important



to note that all of the equipment listed is not used in all phases of construction. Further, the equipment used generally is not operated continuously, nor is the equipment always operated simultaneously or at full load conditions.

Construction is a temporary activity, and no noise limits applicable to construction were identified. Exhaust noise from diesel engines that power the equipment is usually the predominant source of construction equipment noise. Accordingly, maintaining functional mufflers on all diesel-powered equipment will be a mitigation measure and a requirement of the project. As an additional mitigation measure, construction will only occur during daytime hours.

4. CONCLUSION

This report presents the results of the noise assessment ERM conducted for the Lynn Bark Energy Center in Martin County, Kentucky. The assessment included a noise model of the construction noise and major facility noise generating equipment operating under full load conditions during both daytime and nighttime operating conditions. ERM evaluated the operational noise model results against estimated existing ambient conditions and the USEPA noise guidance.

The construction noise assessment, conducted for both pile driving and general construction activity, revealed that pile driving noise levels would be below the estimated existing ambient condition at about half of the NSA locations, due to the shielding effect provided by area topography. The other half of NSA locations were shown to have pile driving noise levels above ambient, but only when pile driving is occurring at the nearest approach to the NSA. General construction related noise levels would be lower than pile driving noise.

The operational noise assessment revealed that Project-generated noise levels would be well below estimated existing conditions at all identified NSA locations during daytime hours with all equipment in operation at full load. Much lower operational noise levels, well below the estimated ambient condition, would occur during nighttime hours when the Project inverters are not in operation. Modeled levels were also shown to be well below the USEPA recommended protective noise level at all nearby NSAs during both daytime and nighttime operating conditions.



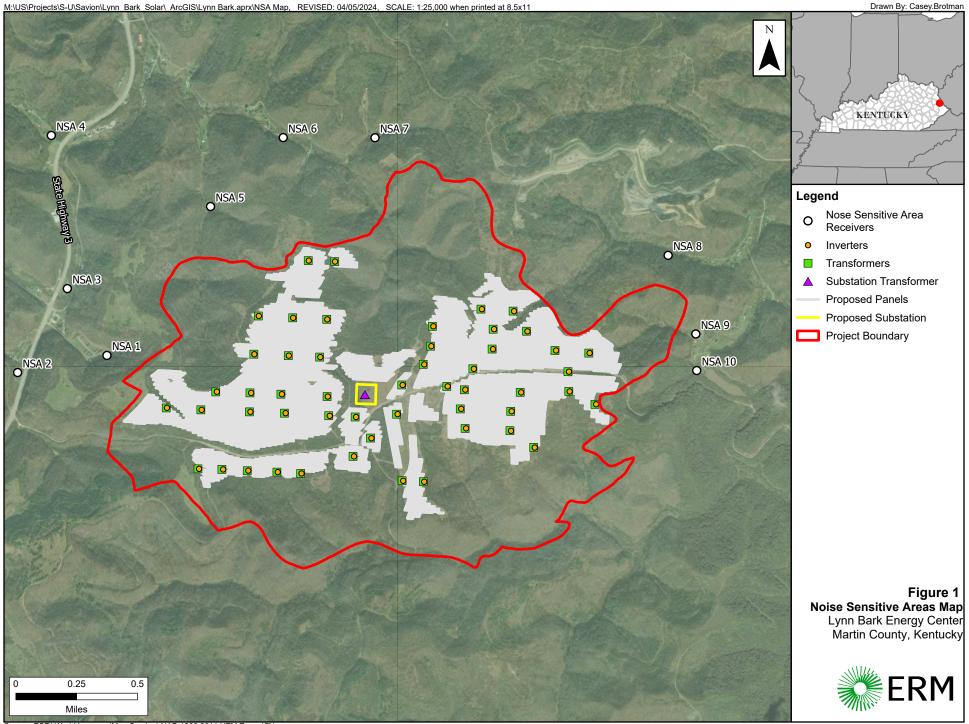
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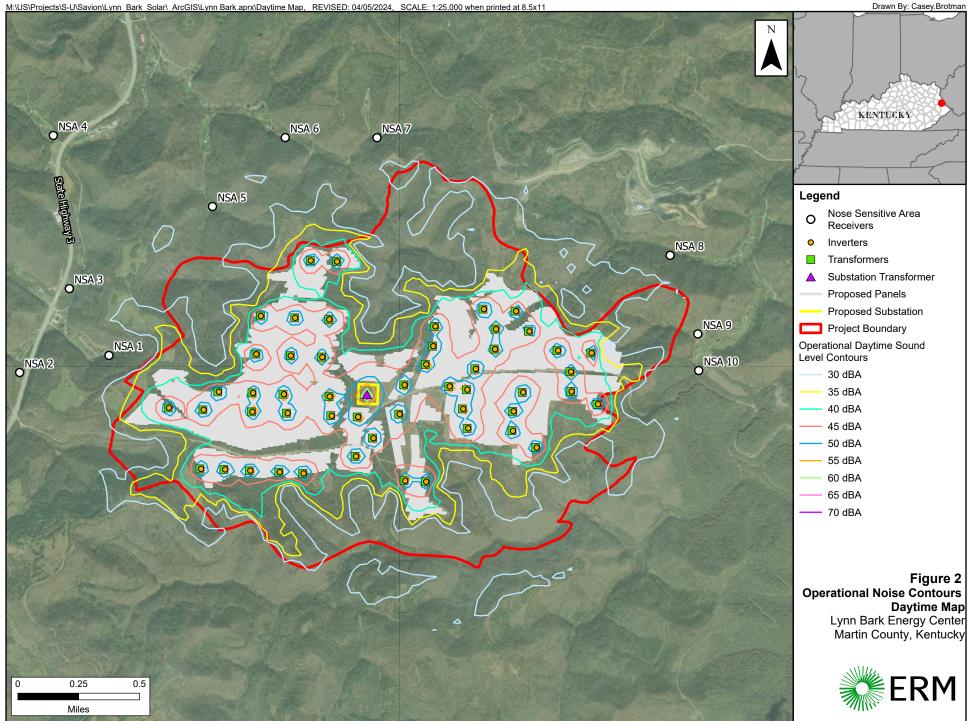


APPENDIX A FIGURES

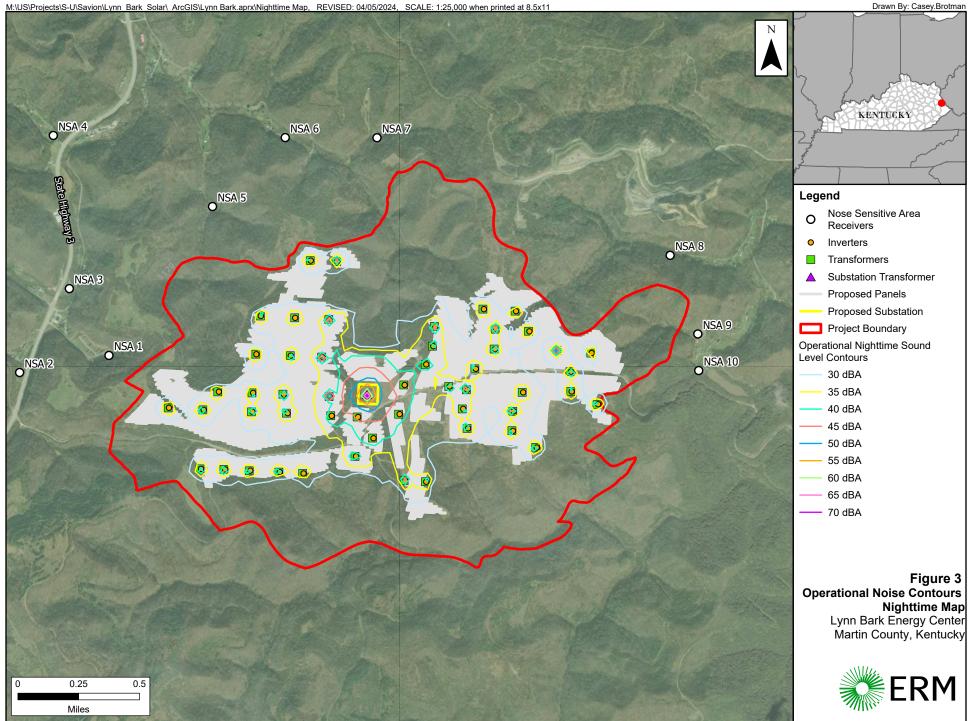




Source: ESRI World Imagery (Map Service) NAD 1983 2011 UTM Zone 17N



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