

**COMMONWEALTH OF KENTUCKY  
BEFORE THE PUBLIC SERVICE COMMISSION**

In the matter of:

THE APPLICATION OF EAST KENTUCKY NETWORK )  
LLC FOR THE ISSUANCE OF A CERTIFICATE OF )  
PUBLIC CONVENIENCE AND NECESSITY TO ) CASE NO. 2021-00008  
CONSTRUCT A TOWER IN WOLFE COUNTY, )  
KENTUCKY. )

East Kentucky Network, LLC d/b/a Appalachian Wireless was granted authorization to provide cellular service in the KY-10 Cellular Market Area (CMA452) by the Federal Communications Commission (FCC). The FCC license is included as Exhibit 1. East Kentucky Network, LLC merger documents were filed with the Commission on February 2, 2001 in Case No. 2001-022. East Kentucky Network, LLC is a Kentucky limited liability company that was organized on June 16, 1998. East Kentucky Network, LLC is in good standing with the Commonwealth of Kentucky.

In an effort to improve service in Wolfe County, pursuant to KRS 278.020 Subsection 1 and 807 KAR 5:001, East Kentucky Network, LLC is seeking the Commission's approval to construct a 190 foot monopole tower on a tract of land located at 1711 KY 746, Campton, Wolfe County, Kentucky (37°45'50.32"N 83°31'34.68"W). A map and detailed directions to the site can be found in Exhibit 7.

Construction of the proposed tower is required by public convenience and necessity. Due to increasing demand for telecommunications service, the proposed tower is necessary to provide adequate coverage. The proposed tower will improve service in Wolfe County by providing an interconnection between East Kentucky Network, LLC other sites thereby forming a cohesive network.

Exhibit 2 is a list of all Property owners according to the Property Valuation Administrator's record who own property within 500 feet of the proposed Tower and all property owners that own

property contiguous to the property upon which construction is proposed in accordance with the Property Valuation Administrator's record.

Pursuant to 807 KAR 5:063 Section 1(1)(l), Section 1(m) and Section 2, all affected property owners according to the Property Valuation Administrator's records who own property within 500 feet of the proposed Tower or contiguous to the property upon which construction is proposed were notified by certified mail return receipt requested of East Kentucky Network, LLC's proposed construction and informed of their right to intervene. They were given the docket number under which this application is filed. Enclosed in Exhibit 2 is a copy of that notification.

Wolfe County has no formal local planning unit. In absence of this unit, the Wolfe County Judge Executive's office was notified by certified mail, return receipt requested, of East Kentucky Network, LLC's proposal and informed of their right to intervene. The Wolfe County Judge Executive's office was also given the docket number under which this application is filed. Enclosed in Exhibit 3 is a copy of that notification.

Notice of the location of the proposed construction was published in The Wolfe County News, January 28, 2021, edition. Enclosed is a copy of that notice in Exhibit 3. The Wolfe County News is the newspaper with the largest circulation in Wolfe County.

A geologist was employed to determine soil and rock types and to ascertain the distance to solid bedrock. The geotechnical report is enclosed as Exhibit 4.

A copy of the tower design information is enclosed as Exhibit 5. The proposed tower has been designed by engineers at Tapp, Inc. and will be constructed under their supervision. Their qualifications are evidenced in Exhibit 5 by the seal and signature of the registered professional engineer responsible for this project.

The tower will be erected by S & S Tower Services of St. Albans, West Virginia. S & S Tower Services has vast experience in the erection of communications towers. Their qualifications are described in Exhibit 13.

FAA and Kentucky Airport Zoning Commission Approvals are included as Exhibit 6.

No Federal Communications Commission approval is required prior to construction of this facility. Once service is established from this tower we must immediately notify the Federal Communications Commission of its operation. Prior approval is needed only if the proposed facility increases the size of the cellular geographic service area. This cell site will not expand the cellular geographic service area.

Two notice signs meeting the requirements prescribed by 807 KAR 5:063, Section 1(2), measuring at least two (2) feet in height and four (4) feet in width and containing all required language in letters of required height, have been posted, one at a visible location on the proposed site and one on the nearest public road. The two signs were posted on January 15, 2021, and will remain posted for at least two weeks after filing of this application as specified.

Enclosed in Exhibit 8 is a copy of East Kentucky Network, LLC's Memorandum of Lease for the site location along with a lot description.

The proposed construction site is located on a tract of land previously developed.

East Kentucky Network, LLC's operation will not affect the use of nearby land nor its value. No more suitable site exists in the area. A copy of the search area map is enclosed in Exhibit 7. One other tower, which is owned by Mountain Telephone Coop Corp., exists within the search area, and East Kentucky Network, LLC currently colocalizes on this tower. However, the tower is reaching capacity and cannot accommodate East Kentucky Network, LLC's needs. To better serve the community, East Kentucky Network, LLC requires its own tower so that it may add more equipment as needed and move the equipment to higher elevations.

Enclosed, and filed as Exhibit 9 is a survey of the proposed tower site signed by a Kentucky registered professional engineer.

Exhibit 10 is a map in one (1) inch equals 200 feet scale identifying every structure and every owner of real estate within 500 feet of the proposed tower and all property owners who own contiguous property to the property upon which construction is proposed.

Exhibit 11 contains a vertical sketch of the tower supplied by James W. Caudill, Kentucky registered professional engineer.

Enclosed as Exhibit 12 is a list of utilities, corporations, or persons with whom the tower is likely to compete.

**[THE REMAINDER OF THIS PAGE INTENTIONALLY LEFT BLANK.]**

**WHEREFORE**, Applicant, having met the requirements of KRS 278.020(1), 278.650, 278.665, and all applicable rules and regulations of the PSC, respectfully requests that the PSC accept the foregoing Application for filing and grant a Certificate of Public Convenience and Necessity to construct and operate the proposed tower.

The foregoing document was prepared by Krystal Branham, Regulatory Compliance Attorney for East Kentucky Network, LLC d/b/a Appalachian Wireless. All related questions or correspondence concerning this filing should be mailed to East Kentucky Network, LLC d/b/a Appalachian Wireless, 101 Technology Trail, Ivel, KY 41642.

SUBMITTED BY: Lynn Haney DATE: 1/22/21  
Lynn Haney, Regulatory Compliance Director

APPROVED BY: W.A. Gillum DATE: 1/22/21  
W.A. Gillum, General Manager

ATTORNEY: Krystal Branham DATE: 1/26/2021  
Hon. Krystal Branham, Attorney

**CONTACT INFORMATION:**

**W.A. Gillum, General Manager**  
Phone: (606) 477-2355, Ext. 111  
Email: wagillum@ekn.com

**Lynn Haney, Regulatory Compliance Director**  
Phone: (606) 477-2355, Ext. 1007  
Email: lhaney@ekn.com

**Krystal Branham, Attorney**  
Phone: (606) 477-2355, Ext. 1009  
Email: kbranham@ekn.com

**Mailing Address:**

**East Kentucky Network, LLC  
d/b/a Appalachian Wireless  
101 Technology Trail  
Ivel, KY 41642**

|    |   |
|----|---|
| 1  | FCC License   |
| 2  | Copies of Cell Site Notice to Land Owners   |
| 3  | Notifications of County Judge Executive and Newspaper                                 |
| 4  | Universal Soil Bearing Analysis   |
| 5  | Tower Design  |
| 6  | FAA and KAZC Determination  |
| 7  | Driving Directions from County Court House and Map to SUItable Scale                  |
| 8  | Memorandum of Lease for Proposed Site with Legal Description                          |
| 9  | Survey of Site Signed/Sealed by Professional Engineer Registered in State of Kentucky |
| 10 | Site Survey Map with Property Owners Identified in Accordance with PVA of County      |
| 11 | Vertical Profile Sketch of Proposed Tower   |
| 12 | List of Competitors   |
| 13 | Qualifications  |
| 14 |   |
| 15 |   |

# Exhibit 1

ULS License

## Cellular License - KNKN809 - East Kentucky Network, LLC d/b/a Appalachian Wireless

|           |         |               |               |
|-----------|---------|---------------|---------------|
| Call Sign | KNKN809 | Radio Service | CL - Cellular |
| Status    | Active  | Auth Type     | Regular       |

**Market**

|           |                               |               |   |
|-----------|-------------------------------|---------------|---|
| Market    | CMA452 - Kentucky 10 - Powell | Channel Block | B |
| Submarket | 0                             | Phase         | 2 |

**Dates**

|           |            |              |            |
|-----------|------------|--------------|------------|
| Grant     | 08/30/2011 | Expiration   | 10/01/2021 |
| Effective | 10/10/2014 | Cancellation |            |

**Five Year Buildout Date**

10/17/1996

**Control Points**

**1** US Route 23, FLOYD, Harold, KY  
P: (606)478-2355

**Licensee**

|     |            |      |                           |
|-----|------------|------|---------------------------|
| FRN | 0001786607 | Type | Limited Liability Company |
|-----|------------|------|---------------------------|

**Licensee**

East Kentucky Network, LLC d/b/a Appalachian Wireless  
101 Technology Trail  
Ivel, KY 41642  
P:(606)477-2355

**Contact**

|                                     |                    |
|-------------------------------------|--------------------|
| Lukas, Nace, Gutierrez & Sachs, LLP | P:(703)584-8665    |
| Pamela L Gist Esq                   | F:(703)584-8695    |
| 8300 Greensboro Drive               | E:pgist@fcclaw.com |
| McLean, VA 22102                    |                    |

**Ownership and Qualifications**

Radio Service Type Mobile  
Regulatory Status Common Carrier Interconnected Yes

**Alien Ownership**

The Applicant answered "No" to each of the Alien Ownership questions.

**Basic Qualifications**

The Applicant answered "No" to each of the Basic Qualification questions.

**Demographics**

Race

Ethnicity

Gender

# Exhibit 2

**EXHIBIT 2 - LIST OF PROPERTY OWNERS**

**Statement Pursuant to Section 1 (1) (I) 807 KAR 5:063**

**Section 1 (1)(I) 1.** The following is a list of every property owner who according to property valuation administrator's records, owns property within 500 feet of the proposed tower and each have been: notified by certified mail, return receipt requested, of the proposed construction,

**Section 1 (1)(I) 2.** Every person listed below who, according to the property valuation administrator's records, owns property within 500 feet of the proposed tower has been: Given the Commission docket number under which the application will be processed: and

**Section 1 (1)(I) 3.** Every person listed below who, according to property valuation administrator's records owns property within 500 feet of the proposed tower has been: Informed of his right to request intervention.

**Section 2.** If the construction is proposed for an area outside the incorporated boundaries of a city, the application shall state that public notices required by Section 1(1)(L) have been sent to every person who, according to the property valuation administrator, owns property contiguous to the property upon which the construction is proposed

LIST OF PROPERTY OWNERS

Todd Haddix  
212 Lowell Leshar Road  
Campton, KY 41301

Todd Haddix and Chastity Haddix  
50 Rose Street  
Campton , KY 41301

John and Betty Mayabb  
1625 KY 746  
Campton, KY 41301

B. Scott Graham  
P.O. Box 637  
Stanton, KY 40380

Pauline Ratliff  
P.O. Box 132  
212 Lowell Leshar Road  
Campton, KY 41301

Mountain Telephone Coop Corp.  
P.O. Box 399  
West Liberty, KY 41472

Kenneth Ray Branham  
P.O. Box 873  
Campton, KY 41301

VIA: U.S. CERTIFIED MAIL

PUBLIC NOTICE

January 22, 2021

Todd Haddix  
212 Lowell Leshar Road  
Campton, KY 41301

RE: Public Notice-Public Service Commission of Kentucky (Case No. 2021-00008)

East Kentucky Network, LLC d/b/a Appalachian Wireless has applied to the Public Service Commission of Kentucky for a Certificate of Public Convenience and Necessity to construct and operate a new facility to provide cellular telecommunications service in Wolfe County. The facility will include a 190-foot self-supporting tower with attached antennas extending upwards, and an equipment shelter located on a tract of land at 1711 KY 746, Campton, Wolfe County. A map showing the location of the proposed new facility is enclosed. This notice is being sent to you because you may own property within a 500' radius of the proposed tower or own property contiguous to the property upon which construction is proposed.

The Commission invites your comments regarding the proposed construction. You also have the right to intervene in this matter. The Commission must receive your initial communication within 20 days of the date of this letter as shown above.

Your comments and request for intervention should be addressed to: Executive Director's Office, Public Service Commission of Kentucky, P.O. Box 615, Frankfort, KY 40602. Please refer to Case No. 2021-00008 in your correspondence.

If you have any questions for East Kentucky Network, LLC, please direct them to my attention at the following address: East Kentucky Network, LLC, 101 Technology Trail, Ivel, KY 41642 or call me at 606-477-2355, Ext. 1007.

Sincerely,



Lynn Haney, CPA  
Regulatory Compliance Director  
Enclosure 1

VIA: U.S. CERTIFIED MAIL

PUBLIC NOTICE

January 22, 2021

Todd Haddix and Chastity Haddix  
50 Rose Street  
Campton, KY 41301

RE: Public Notice-Public Service Commission of Kentucky (Case No. 2021-00008)

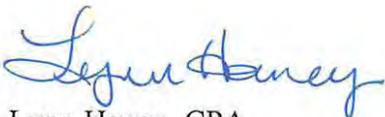
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Sincerely,



Lynn Haney, CPA  
Regulatory Compliance Director  
Enclosure 1

VIA: U.S. CERTIFIED MAIL

PUBLIC NOTICE

January 22, 2021

John and Betty Mayabb  
1625 KY 746  
Campton, KY 41301

RE: Public Notice-Public Service Commission of Kentucky (Case No. 2021-00008)

East Kentucky Network, LLC d/b/a Appalachian Wireless has applied to the Public Service Commission of Kentucky for a Certificate of Public Convenience and Necessity to construct and operate a new facility to provide cellular telecommunications service in Wolfe County. The facility will include a 190-foot self-supporting tower with attached antennas extending upwards, and an equipment shelter located on a tract of land at 1711 KY 746, Campton, Wolfe County. A map showing the location of the proposed new facility is enclosed. This notice is being sent to you because you may own property within a 500' radius of the proposed tower or own property contiguous to the property upon which construction is proposed.

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If you have any questions for East Kentucky Network, LLC, please direct them to my attention at the following address: East Kentucky Network, LLC, 101 Technology Trail, Ivel, KY 41642 or call me at 606-477-2355, Ext. 1007.

Sincerely,



Lynn Haney, CPA  
Regulatory Compliance Director  
Enclosure 1

VIA: U.S. CERTIFIED MAIL

PUBLIC NOTICE

January 22, 2021

B. Scott Graham  
P.O. Box 637  
Stanton, KY 40380

RE: Public Notice-Public Service Commission of Kentucky (Case No. 2021-00008)

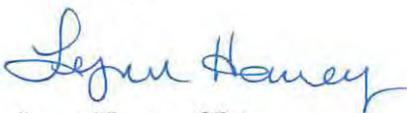
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Sincerely,



Lynn Haney, CPA  
Regulatory Compliance Director  
Enclosure 1

VIA: U.S. CERTIFIED MAIL

PUBLIC NOTICE

January 22, 2021

Pauline Ratliff  
P.O. Box 132  
212 Lowell Leshner Road  
Campton, KY 41301

RE: Public Notice-Public Service Commission of Kentucky (Case No. 2021-00008)

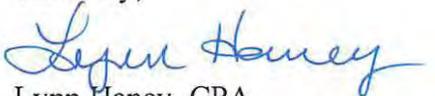
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If you have any questions for East Kentucky Network, LLC, please direct them to my attention at the following address: East Kentucky Network, LLC, 101 Technology Trail, Ivel, KY 41642 or call me at 606-477-2355, Ext. 1007.

Sincerely,



Lynn Haney, CPA  
Regulatory Compliance Director  
Enclosure 1

VIA: U.S. CERTIFIED MAIL

PUBLIC NOTICE

January 22, 2021

Mountain Telephone Coop Corp.  
P.O. Box 399  
West Liberty, KY 41472

RE: Public Notice-Public Service Commission of Kentucky (Case No. 2021-00008)

East Kentucky Network, LLC d/b/a Appalachian Wireless has applied to the Public Service Commission of Kentucky for a Certificate of Public Convenience and Necessity to construct and operate a new facility to provide cellular telecommunications service in Wolfe County. The facility will include a 190-foot self-supporting tower with attached antennas extending upwards, and an equipment shelter located on a tract of land at 1711 KY 746, Campton, Wolfe County. A map showing the location of the proposed new facility is enclosed. This notice is being sent to you because you may own property within a 500' radius of the proposed tower or own property contiguous to the property upon which construction is proposed.

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Your comments and request for intervention should be addressed to: Executive Director's Office, Public Service Commission of Kentucky, P.O. Box 615, Frankfort, KY 40602. Please refer to Case No. 2021-00008 in your correspondence.

If you have any questions for East Kentucky Network, LLC, please direct them to my attention at the following address: East Kentucky Network, LLC, 101 Technology Trail, Ivel, KY 41642 or call me at 606-477-2355, Ext. 1007.

Sincerely,



Lynn Haney, CPA  
Regulatory Compliance Director  
Enclosure 1

VIA: U.S. CERTIFIED MAIL

PUBLIC NOTICE

January 22, 2021

Kenneth Ray Branham  
P.O. Box 873  
Campton, KY 41301

RE: Public Notice-Public Service Commission of Kentucky (Case No. 2021-00008)

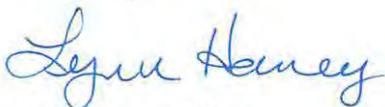
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Sincerely,



Lynn Haney, CPA  
Regulatory Compliance Director  
Enclosure 1

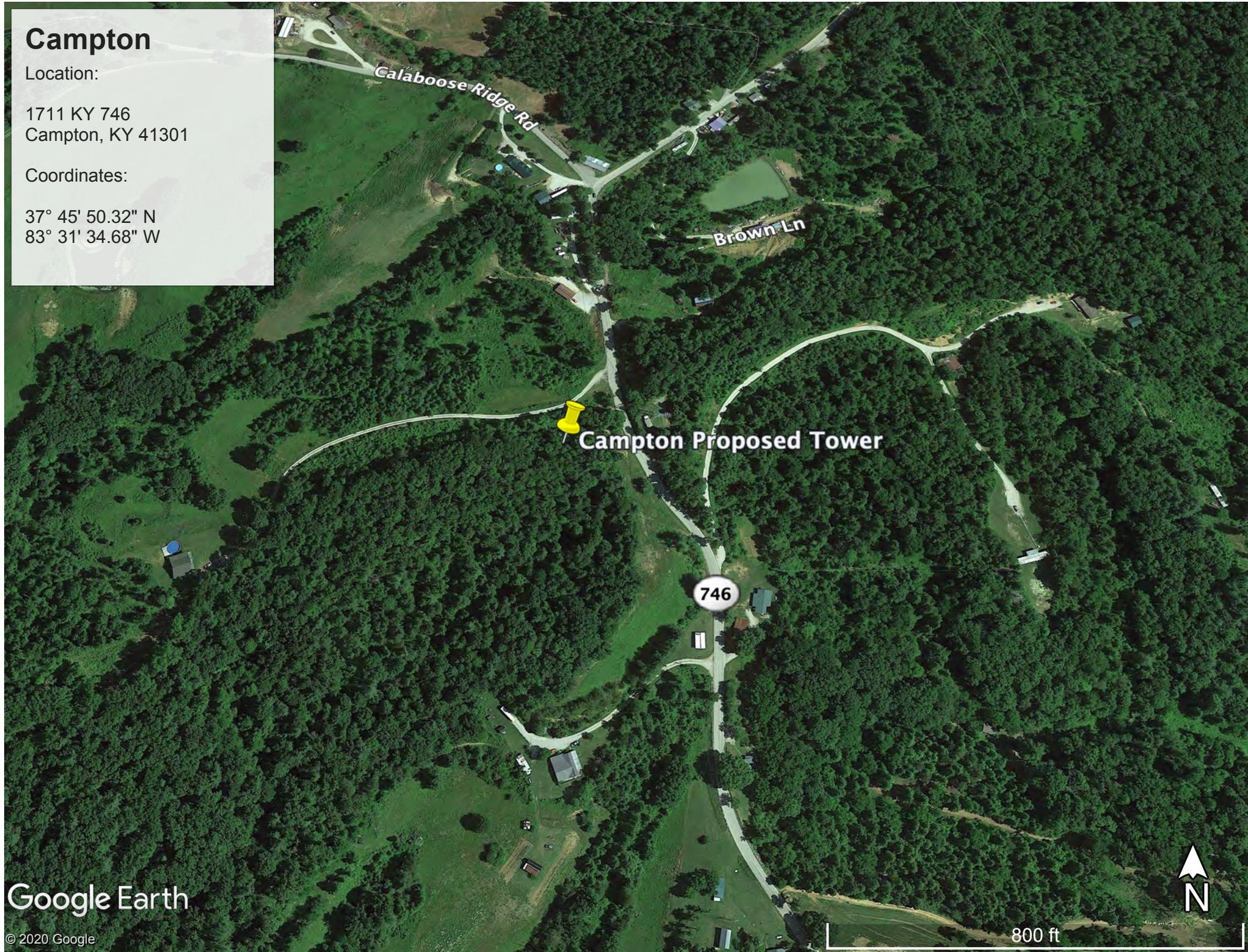
# Campton

Location:

1711 KY 746  
Campton, KY 41301

Coordinates:

37° 45' 50.32" N  
83° 31' 34.68" W



Google Earth

© 2020 Google



800 ft

# Exhibit 3



VIA: U.S. CERTIFIED MAIL

January 22, 2021

Raymond Banks, Judge Executive  
P.O. Box 429  
Campton, KY 41301

RE: Public Notice-Public Service Commission of Kentucky (Case No. 2021-00008)

East Kentucky Network, LLC d/b/a Appalachian Wireless has applied to the Public Service Commission of Kentucky for a Certificate of Public Convenience and Necessity to construct and operate a new facility to provide cellular telecommunications service in Wolfe County. The facility will include a 190-foot self-supporting tower with attached antennas extending upwards, and an equipment shelter located on a tract of land located at 1711 Highway 746, Wolfe County, Kentucky. A map showing the location of the proposed new facility is enclosed. This notice is being sent to you because you are the County Judge Executive of Wolfe County.

The Commission invites your comments regarding the proposed construction. You also have the right to intervene in this matter. The Commission must receive your initial communication within 20 days of the date of this letter as shown above.

Your comments and request for intervention should be addressed to: Executive Director's Office, Public Service Commission of Kentucky, P.O. Box 615, Frankfort, KY 40602. Please refer to Case No. 2021-00008 in your correspondence.

If you have any questions for East Kentucky Network, LLC, please direct them to my attention at the following address: East Kentucky Network, LLC, 101 Technology Trail, Ivel, KY 41642 or call me at 606-477-2355, Ext. 1007.

Sincerely,

A handwritten signature in blue ink that reads "Lynn Haney".

Lynn Haney, CPA  
Regulatory Compliance Director  
Enclosure

dba Appalachian Wireless  
101 Technology Trail  
Ivel, KY 41642  
Phone: 606-477-2355  
Fax: 606-791-2225

EAST KENTUCKY  
NETWORK



**To:** The Wolfe County News  
Attn: Classifieds

**From:** Raina Helton  
Regulatory Compliance Assistant

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**Email:** wolfenew@mrtc.com

**Date:** January 19, 2021

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**Re:** PUBLIC NOTICE ADVERTISEMENT

**Pages:** 1

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Please place the following Public Notice Advertisement in The Wolfe County News to be ran on January 28, 2021.

**PUBLIC NOTICE:**

RE: Public Service Commission of Kentucky (CASE NO. 2021-00008)

Public Notice is hereby given that East Kentucky Network, LLC, dba Appalachian Wireless has applied to the Kentucky Public Service Commission to construct a cellular telecommunications tower on a tract of land located at 1711 Highway 746, Campton, Wolfe County, Kentucky. The proposed tower will be a 190 foot self-supporting tower with attached antennas. If you would like to respond to this notice, please contact the Executive Director, Public Service Commission, 211 Sower Boulevard, PO Box 615, Frankfort, Kentucky 40602. Please refer to Case No. 2021-00008.

If you have any questions about the placement of the above-mentioned notice, please call me at 606-477-2375, ext. 1005.

Thank you,

Raina Helton  
Regulatory Compliance Paralegal

The message above and the information contained in the documents transmitted are confidential and intended only for the person(s) named above. Dissemination, distribution or copying of this communication by anyone other than the person(s) named above is prohibited. If you have received this communication in error, please notify us immediately by telephone and return the original message to us at the address listed above via regular mail. Thank you.

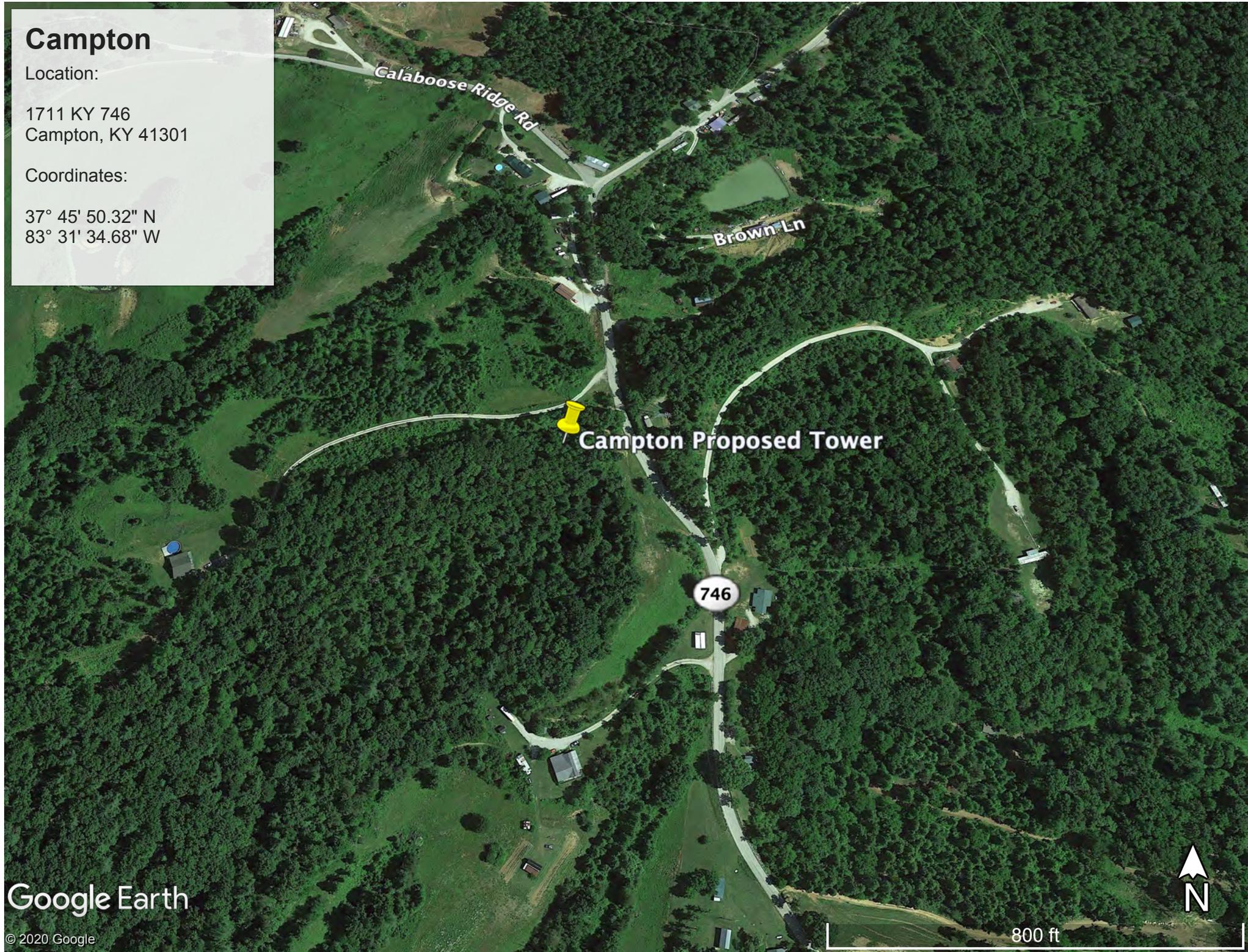
# Campton

Location:

1711 KY 746  
Campton, KY 41301

Coordinates:

37° 45' 50.32" N  
83° 31' 34.68" W



Google Earth

© 2020 Google



800 ft

# Exhibit 4

230 Swartz Drive • Hazard • Kentucky • 41701

Phone (606) 551-1050



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**EAST KENTUCKY ENGINEERING, LLC.**

**APPALACHIAN WIRELESS  
Geotechnical Investigation on the  
Campton North Tower Site  
Wolfe County, Kentucky  
EKYENG Project No. 165-000-0117**

PREPARED FOR:

Appalachian Wireless.  
101 Technology Trail  
Ivel, Kentucky 41642

PREPARED BY:

Richard Dirk Smith PE, PLS  
President  
**East Kentucky Engineering**  
230 Swartz Drive  
Hazard, Kentucky 41701

\_\_\_\_\_, 20215, October 6<sup>th</sup>, 2020



# EAST KENTUCKY ENGINEERING, LLC.

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## **EXECUTIVE SUMMARY**

### **1.0 INTRODUCTION**

### **2.0 PROJECT DESCRIPTION**

### **3.0 SITE DESCRIPTION & HISTORICAL MINING**

3.1 GENERAL INFORMATION

3.2 SURFACE MINING

3.3 UNDERGROUND MINING

3.4 FLOOD HAZARD

### **4.0 FIELD EXPLORATION**

4.1 SITE INFORMATION

4.2 BORING DATA

4.3 GROUNDWATER

4.4 SEISMIC SITE CLASSIFICATION

### **5.0 DISCUSSION AND RECOMMENDATIONS**

5.1 GENERAL

5.2 DRILLED PIERS FOUNDATION RECOMMENDATIONS

5.3 BURIED UTILITIES

### **6.0 WARRANTY**

6.1 SUBSURFACE EXPLORATION

6.2 LABORATORY AND FIELD TEST

6.3 ANALYSIS AND RECOMMENDATIONS

6.4 CONSTRUCTION MONITORING

6.5 GENERAL

## **SPECIFICATIONS**

**I – GENERAL**

**II – ENGINEERED FILL BENEATH STRUCTURES CLEARING AND GRADING SPECIFICATIONS**

**III – GUIDELINES FOR EXCAVATIONS AND TRENCHING**

**IV – DRILLED PIER INSTALLATION**

**V – GENERAL CONCRETE SPECIFICATIONS**

**APPENDIX A – BORING LOGS**

**APPENDIX B – CORE PHOTOGRAPHS**

**APPENDIX C – SEISMIC DATA**

**APPENDIX D – PHOTOGRAPHS**

**APPENDIX E – MAPS**



## EXECUTIVE SUMMARY

A geotechnical investigation has been performed on the Campton North Tower Site, located in Wolfe County, Kentucky. This site is readily accessible. A location map is shown in Figure 1 of this report. One (1) boring was advanced to a maximum depth of 31.4 ft. The following geotechnical considerations were identified:

- Borings utilized for this study encountered sandy silt to 2.5 ft, brown weathered shale to 12.2 ft, sandstone to 21.9 ft, gray shale to 25.4 ft., sandstone to 27.2 ft., and gray shale to 31.4 ft.
- This site is on a forested point.
- **The allowable bearing capacities of the brown weathered shale are estimated at 3 tsf, the sandstone is estimated at 8 tsf and the gray shale is 4 tsf. See section 5.2 for additional details.**
- The 2015 International Building Code seismic site classification for this site is **“A”**.
- If during the foundation design it becomes necessary to lower, raise, or change the footer configuration, alternate design recommendations can be provided by EKYENG.
- Close monitoring of the construction operations discussed herein will be critical in achieving the design subgrade support. We, therefore, recommend that EKYENG is retained to monitor this portion of the work.

This executive summary is included to provide a general overview of the project and should not be relied upon except for the purpose it was prepared. Please rely on the complete report for the information on the findings, recommendations, and all other concerns.



# EAST KENTUCKY ENGINEERING, LLC.

## 1. INTRODUCTION

East Kentucky Engineering (EKYENG) was retained by Mr. Stanton Neece of Appalachian Wireless to prepare a geotechnical engineering report for the proposed tower site located on the Campton North Property, in Wolfe County, Kentucky. A site location map is shown in Figure No. 1.

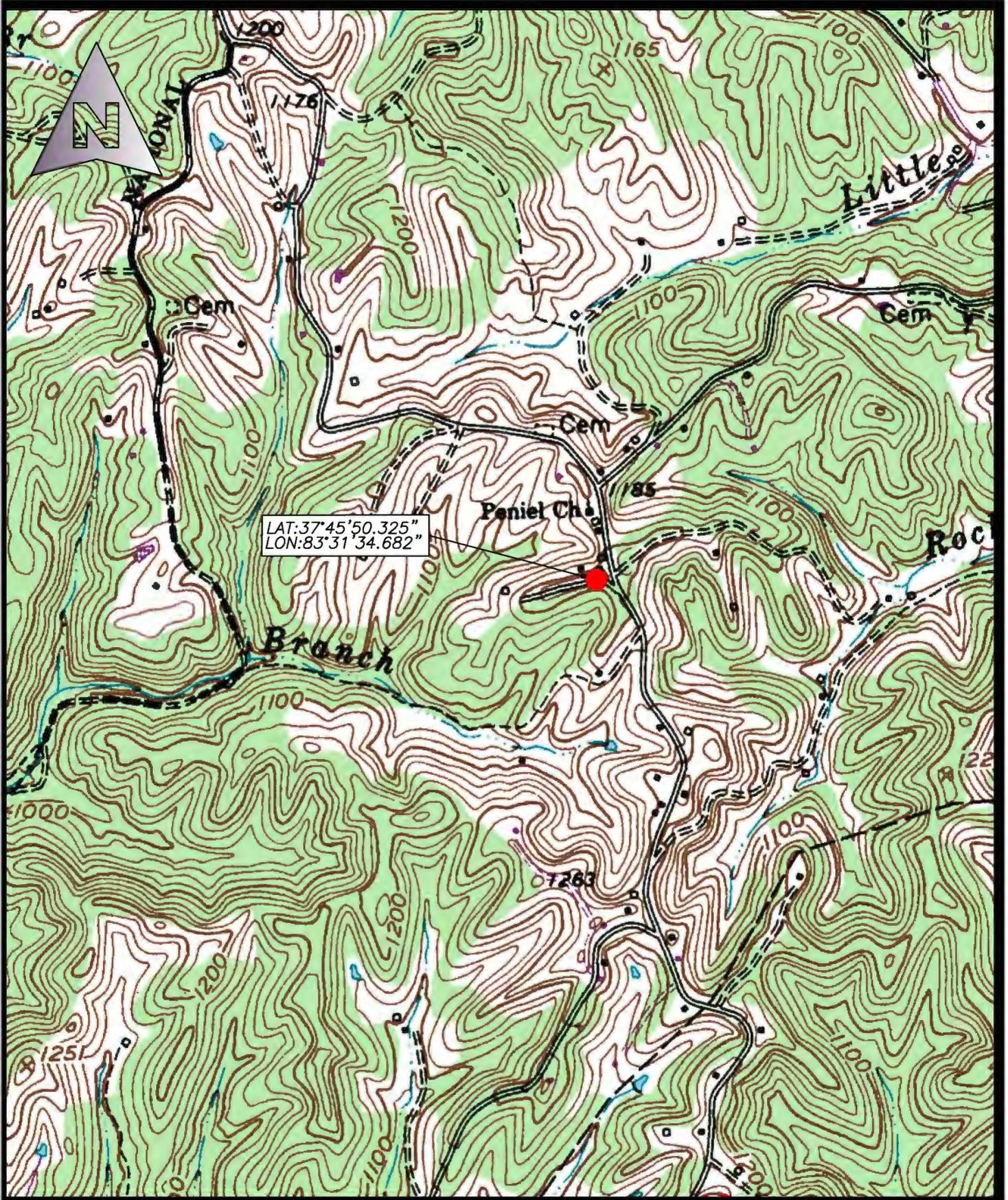
One (1) boring was advanced to a maximum depth of 31.4 ft. Horn and Associates, Inc. provided drilling services to obtain these borings. Logs of the borings along with a boring location plan are included in Appendix A and Appendix D. The purpose of these services is to provide information and geotechnical engineering recommendations about subsurface conditions, earthwork, seismic considerations, groundwater conditions, and foundation design.

## 2.0 PROJECT DESCRIPTION

The proposed communication facility will consist of a self-supporting tower of undetermined height and ancillary support areas. The footing area is estimated to be an 8 ft diameter pier, with a base of the tower elevation at 1216'. Based on the information provided, we estimate the structural loads will be like the following conditions.

| CONDITION   | LOAD    |
|-------------|---------|
| Total Shear | 40 Kips |
| Axial Load  | 50 Kips |

We anticipate that overturning will govern the structural design. If the loading is significantly different than these expected values, EKYENG should be notified to re-evaluate the recommendations provided in this report.



|             |                |
|-------------|----------------|
| Drawn:RDS   | 9/16/2020      |
| Job:165-117 | Scale:1"=1000' |

APPALACHIAN WIRELESS  
 EXCERPT FROM USGS QUAD  
 LOCATION MAP  
 CAMPTON TOWER SITE  
 FIGURE NO 1

East Kentucky Engineering,LLC.  
 230 Swartz Drive  
 Hazard, KY 41701  
 (606) 551-1050



## **3.0 SITE DESCRIPTION & HISTORICAL MINING**

### **3.1 GENERAL INFORMATION**

The site location is on a forested point in Wolfe County, Kentucky. The current surface elevation is approximately 1216.0 ft. Research on the historical mining was conducted by obtaining previous mine license maps from the “Kentucky Mine Mapping Information System” (KMMIS).

### **3.2 SURFACE MINING**

No issues from surface mining activities are expected at this site location.

### **3.3 UNDERGROUND MINING**

No underground mines were found within the vicinity of this site. Therefore, no subsidence issues are anticipated.

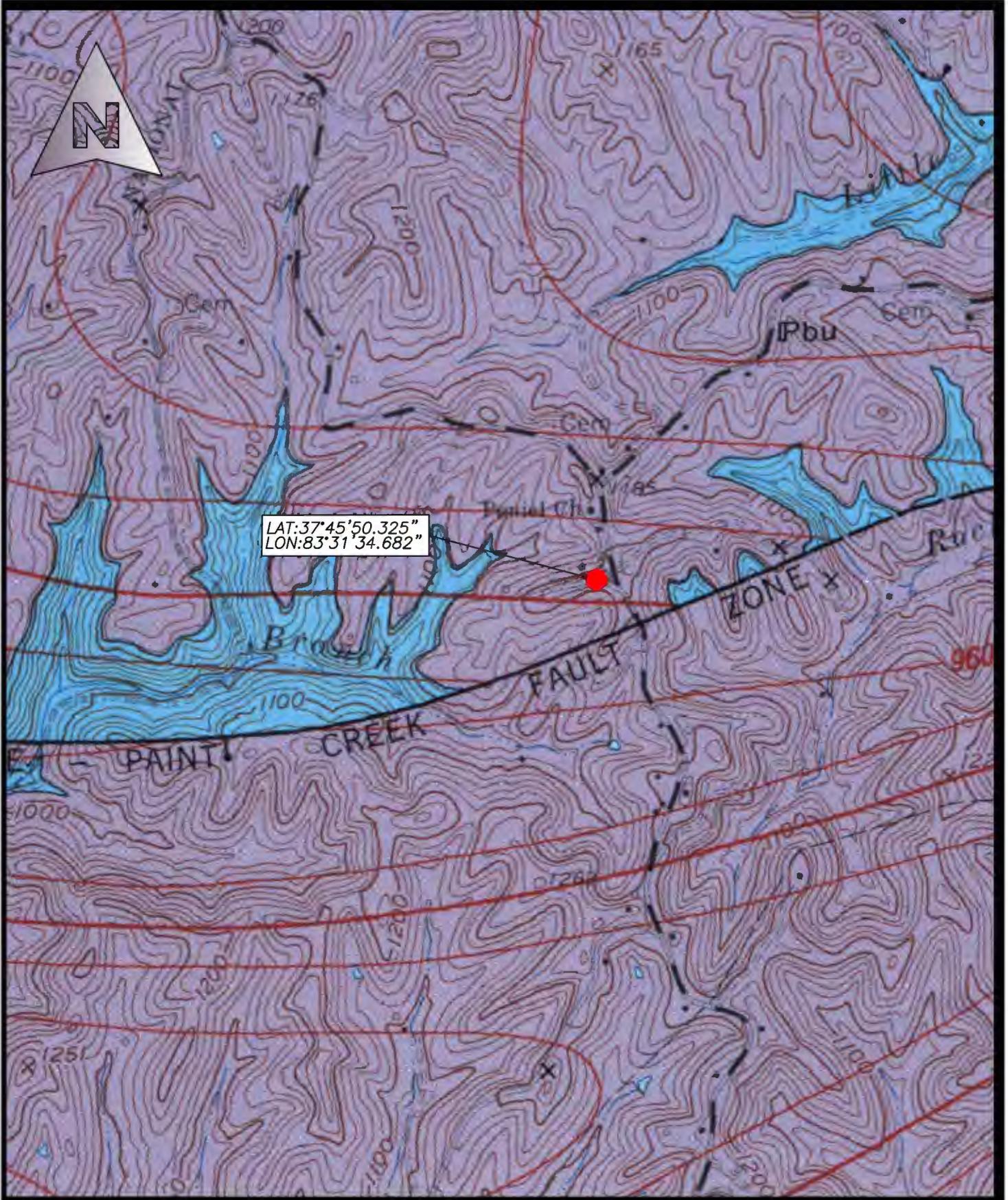
### **3.4 FLOOD HAZARD**

A potential flood determination was conducted by EKYENG. For this determination, the FEMA Flood Map Service was reviewed for this location. The flood map for the selected area is number **21237C0050C-210349**. The flood zone for this area is Zone X and is an area of minimal flood hazard. A FIRMette map is included in Appendix E of this report.

## **4.0 FIELD EXPLORATION**

### **4.1 SITE INFORMATION**

The proposed site is located on a forested point in Wolfe County, Kentucky. The site lies within the Pomeroyton Quadrangle. The site is readily accessible by conventional exploratory equipment. An estimated pad location was determined based on the information provided. Foundation dimensions were estimated to be an 8 ft. diameter circular pier footer for this report.



|             |                |
|-------------|----------------|
| Drawn:RDS   | 9/16/2020      |
| Job:165-117 | Scale:1"=1000' |

APPALACHIAN WIRELESS  
 EXCERPT FROM GEOLOGIC QUAD  
 LOCATION MAP  
 CAMPTON TOWER SITE  
 FIGURE NO 2

East Kentucky Engineering,LLC.  
 230 Swartz Drive  
 Hazard, KY 41701  
 (606) 551-1050



## 4.2 BORING DATA

One (1) boring was made in the relative position shown on the Site Map in Appendix D. The boring logs and resulting data are included in Appendix A. This boring was made with a track-mounted boring rig using hollow-stem augers and employing standard penetration resistance methods (ASTM D-1586, which includes 140-pound hammer, 30-inch drop, and two-inch-O.D. split-spoon sampler) at maximum depth intervals of five feet or at major changes in stratum, whichever occurred first. The disturbed split-spoon samples were visually classified, logged, sealed in moisture-proof jars, and taken to the EKYENG laboratory for study. The depths where these "A"-type split-spoon samples were collected are noted on the boring logs. The results of the natural moisture contents by boring and interval are shown in Table 2.

TABLE 2  
RESULTS OF NATURAL MOISTURE CONTENT TESTS (ASTM D-4643)

| SAMPLE NO. | DEPTH INCREMENT, (FT.) | NATURAL MOISTURE CONTENT, % |
|------------|------------------------|-----------------------------|
| B1 S-1     | 1.5 – 3.0              | 12.7%                       |
| B1 S-2     | 4.0 – 5.5              | 12.7%                       |
| B1 S-3     | 6.5 – 8.0              | 12.3%                       |
| B1 S-4     | 9.0 – 10.5             | 13.8%                       |
| B1 S-5     | 11.5 – 12.2            | 11.3%                       |

The position at which the core was taken is indicated on the boring logs and shown on the sitemap in Appendix D. The corresponding blow counts are shown in Table No. 3.



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TABLE NO. 3  
STANDARD PENETRATIONS

| SAMPLE NO. | DEPTH INCREMENT | BLOW COUNT / RQD * | DESCRIPTION                |
|------------|-----------------|--------------------|----------------------------|
| B-1        | 0.0-2.5         | 8-7-19             | Sandy Silt w/ Veg Organics |
| B-1        | 2.5-12.2        | 12-17-19           | Shale, Brown, Weathered    |
| B-1        | 12.2-21.9       | 95*                | Sandstone                  |
| B-1        | 21.9-25.4       | 92*                | Shale, Gray                |
| B-1        | 25.4-27.2       | 92*                | Sandstone                  |
| B-1        | 27.2-31.4       | 92*                | Shale, Gray                |

The boring encountered weathered shale and sandstone. This boring was extended by "NX" size rock core that was taken to confirm the presence of rock at the site and to determine its physical characteristics. The core was made with "NX" size diamond coring equipment. This boring is between 12.2 ft and 31.4 ft in depth. The position at which the core was taken is indicated on the boring logs and shown on the boring location map in Appendix D.

### 4.3 GROUNDWATER

Groundwater in Eastern Kentucky is characterized by water flowing through a system of internal fractures that lead to an alluvial aquifer near the bottom of valley floors. Large, defined aquifers other than the alluvium is not common, especially in higher elevations such as where this tower site is proposed. Therefore, groundwater should not be a concern in this area. During the site investigation, no groundwater resources were observed.

### 4.4 SEISMIC SITE CLASSIFICATION

Based on the encountered soil conditions at the project site, the site classification was determined to be "Site Class A" per the 2018 Kentucky Building Code. In addition, an  $S_{DS}$  coefficient of 0.105 g was calculated, and an  $S_{D1}$  coefficient of



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0.047 g was also calculated for design based on the aforementioned building code.

## 5.0 DISCUSSION AND RECOMMENDATIONS

### 5.1 GENERAL

The structure will be a self-supporting free-standing monopole tower. Due to wind loading, lattice tower foundations can experience both vertical loads and horizontal loads. The vertical loads act in both an upward and downward direction as the tower attempts to overturn and can act in any directions.

### 5.2 DRILLED PIER FOUNDATION RECOMMENDATIONS

If drilled piers are used for foundation support, we recommend the following design parameters.

TABLE NO. 1

| Approx. Depth (ft.)                | Allowable Skin Friction (psf.) | Allowable End Bearing Pressure (psf.) | Effective Unit Weight (pcf.) | Cohesion (psf.) | Internal Angle of Friction (Degrees) |
|------------------------------------|--------------------------------|---------------------------------------|------------------------------|-----------------|--------------------------------------|
| 0 – 6.8                            | To Be Removed                  |                                       |                              |                 |                                      |
| Brown Weathered Shale<br>6.8– 12.2 | 1200                           | 6000                                  | 150                          | -----           | 24                                   |
| Sandstone<br>12.2 – 21.9           | 2500                           | 16,000                                | 165                          | -----           | 30                                   |
| Gray Shale<br>21.9 – 25.4          | 1500                           | 8,000                                 | 150                          | -----           | 27                                   |



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| Approx. Depth<br>(ft.)    | Allowable<br>Skin<br>Friction<br>(psf.) | Allowable<br>End<br>Bearing<br>Pressure<br>(psf.) | Effective<br>Unit<br>Weight<br>(pcf.) | Cohesion<br>(psf.) | Internal<br>Angle of<br>Friction<br>(Degrees) |
|---------------------------|---|---|---------------------------------------|--------------------|---|
| Sandstone<br>25.4 – 27.2  | 2500                                    | 16,000  | 165                                   | -----              | 30  |
| Gray Shale<br>27.2 – 31.4 | 1500                                    | 8,000   | 150                                   | -----              | 27  |

- *The first 12 feet of material will be removed to construct tower pad.*

The skin friction and passive resistance have a factor of safety of 2. The allowable end bearing pressure has an approximate safety factor of 3. If the drilled piers are designed using the above design parameters and socketed into solid bedrock, settlements are not anticipated to exceed  $\frac{1}{4}$  inch.

It is furthermore recommended that other slabs-on-grade be supported on 4 to 6-inch layer of relatively clean granular material such as sand and gravel or crushed stone. This is to help distribute concentrated loads and equalize moisture conditions beneath the slab. Proper drainage must be incorporated into this granular layer to preclude future wet areas in the finished slab-on-grade. However, all topsoil and/or other deleterious materials encountered during site preparation must be removed and replaced with 4000 psi. concrete below the foundation base. Provided that a minimum of 4 inches of granular material is placed below the new slab-on-grade, a modulus of subgrade reaction (k30) of 100 lbs./cu. in. can be used for design of the slabs.

Support structure for this tower can be placed as needed. It is recommended that test pits are examined to ensure that any of these structures are on the competent materials. If pockets of soft, loose or otherwise unsuitable material are



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encountered in the footing excavations and it is inconvenient to lower the footings, the proposed footing elevations may be re-established by backfilling after the undesirable material has been removed. The undercut excavation beneath each footing should extend to suitable bearing soils and the dimensions of the excavation base should be determined by imaginary planes extending outward and down on a 1 (vertical) to 1 (horizontal) slope from the base perimeter of the footing. The entire excavation should then be refilled with a well-compacted engineered fill, or lean concrete (Please note that the width of the lean concrete zone should be equal or wider than the width of the overlying footing element). Special care should be exercised to remove any sloughed, loose or soft materials near the base of the excavation slopes. In addition, special care should be taken to "tie-in" the compacted fill with the excavation slopes, with benches as necessary, to ensure that no pockets of loose or soft materials will be left in place along the excavation slopes below the foundation bearing level. All Federal, State, and Local regulations should be strictly adhered to relative to excavation side-slope geometry.

### **5.3 BURIED UTILITIES**

Excavations for buried utility pipelines should follow the guidelines set forth in this report. Depending on the pipeline material, a minimum thickness of at least 0.5 feet of select fine-grained granular bedding material should be used beneath all below-grade pipes, with a minimum cover thickness of at least 3 feet to afford an "arching" effect and reduce stresses on the pipe. The cover thickness may be reduced if the external loading condition on the pipe is relatively light or if the pipe is designed to withstand the external loading condition. It is not recommended that "pea-gravel" or other "open-work" aggregates be used for trench backfill since these materials are nearly impossible to compact and tend to pond water within their interstices.



## **6.0 WARRANTY**

Our professional services have been performed, our findings obtained, and our recommendations prepared in accordance with generally accepted geotechnical engineering principles and practices. No other warranty, express or implied, is made.

While the services of EKYENG are a valuable and integral part of the design and construction teams, we do not warrant, guarantee, or insure the quality or completeness of services provided by other members of those teams, the quality, completeness, or satisfactory performance of construction plans and specifications which we have not prepared, nor the ultimate performance of building site materials.

### **6.1 SUBSURFACE EXPLORATION**

Subsurface exploration is normally accomplished by test borings, although test pits are sometimes employed. The method of determining the boring location and the surface elevation at the boring is noted in the report and is presented on the Boring Location Plan or on the boring log. The location and elevation of the boring should be considered accurate only to the degree inherent with the method used.

The boring log includes sampling information, description of the materials recovered, approximate depth of boundaries between soil and rock strata and groundwater data. The boring log represents conditions specifically at the location and time the boring was made. The boundaries between different soil strata are indicated at specific depths; however, these depths are in fact approximate and are somewhat dependent upon the frequency of sampling (The transition between soil strata is often gradual). Free groundwater level readings are made at the times and under conditions stated on the boring logs



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(Groundwater levels change with time and season). The borehole does not always remain open sufficiently long enough for the measured water level to coincide with the groundwater table.

### **6.2 LABORATORY AND FIELD TESTS**

Laboratory and field tests are performed by specific ASTM standards unless otherwise indicated. All determinations included in each ASTM standard are not always required and performed. Each test report indicates the measurements and determinations made.

### **6.3 ANALYSIS AND RECOMMENDATIONS**

The geotechnical report is prepared primarily to aid in the engineering design of site work and structural foundations. Although the information in the report is expected to be sufficient for these purposes, it is not intended to determine the cost of construction or to stand alone as a construction specification.

Our engineering report recommendations are based primarily on data from test borings made at the locations shown in a boring location drawing included. Soil variations may exist between borings, and these variations may not become evident until construction. If significant variations are then noted, the geotechnical engineer should be contacted so that field conditions can be examined and recommendations revised if necessary.

The geotechnical engineering report states our understanding as to the location, dimensions and structural features proposed for the site. Any significant changes in the nature, design, or location of the site improvements **MUST** be communicated to the geotechnical engineer such that the geotechnical analysis, conclusions, and recommendations can be appropriately adjusted. The geotechnical engineer should be given the opportunity to review all drawings that have been prepared based on their recommendations.



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### **6.4 CONSTRUCTION MONITORING**

Construction monitoring is a vital element of complete geotechnical services. The field engineer/inspector is the owner's "representative" observing the work of the contractor, performing tests as required in the specifications, and reporting data developed from such tests and observations. The field engineer or inspector does not direct the contractor's construction means, methods, operations or personnel. The field inspector/engineer does not interfere with the relationship between the owner and the contractor and, except as an observer, does not become a substitute owner on site. The field inspector/engineer is responsible for his own safety but has no responsibility for the safety of other personnel at the site. The field inspector/engineer is an important member of a team whose responsibility is to watch and test the work being done and report to the owner whether that work is being carried out in general conformance with the plans and specifications.

### **6.5 GENERAL**

The scope of our services did not include an environmental assessment for the presence or absence of hazardous or toxic materials in the soil, surface water, groundwater or air, on, within or beyond the site studied. Any statements in the report or on the boring logs regarding odors, staining of soils or other unusual items or conditions observed are strictly for the information of our client.

To evaluate the site for possible environmental liabilities, we recommend an environmental assessment, consisting of a detailed site reconnaissance, a record review, and report of findings. Additional subsurface drilling and samplings, including groundwater sampling, may be required.

This report has been prepared for the exclusive use of Appalachian Wireless, for specific application to the proposed cellular tower located on the Campton North Property located in Wolfe County, Kentucky. Specific design and construction recommendations have been provided in the various sections of the report. The report shall, therefore, be used in its entirety. This report is not a bidding



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document and shall not be used for that purpose. Anyone reviewing this report must interpret and draw their conclusions regarding specific construction techniques and methods that were chosen. EKYENG is not responsible for the independent conclusions, opinions or recommendations made by others based on the field exploratory and laboratory test data presented in this report.



## SPECIFICATIONS

### I – GENERAL

#### 1.0 STANDARDS AND DEFINITIONS

**1.1 STANDARDS** - All standards refer to latest edition unless otherwise noted.

**1.1.1** ASTM D-698-70 (Method C) "Standard Test Methods for Moisture, Density Relations of Soils and Soil Aggregate Mixtures Using 5.5-lb (2.5 kg.) Rammer and 12-inch (305-mm) Drop".

**1.1.2** ASTM D-2922 "Standard Test Method for Density of Soil and Soil Aggregate in Place by Nuclear methods (Shallow Depth)".

**1.1.3** ASTM D-1556 "Standard Test Method for Density of Soil in place by the Sand-Cone Method".

#### 1.2 DEFINITIONS

**1.2.1** Owner - In these specifications the word "Owner" shall mean Appalachian Wireless.

**1.2.2** Engineer - In these specifications the word "Engineer" shall mean the Owner designated engineer.

**1.2.3** Design Engineer - In these specifications the words "Design Engineer" shall mean the Owner designated design engineer.

**1.2.4** Contractor - In these specifications the word "Contractor" shall mean the firm or corporation undertaking the execution of any work under the terms of these specifications.

**1.2.5** Approved - In these specifications the word "approved" shall refer to the approval of the Engineer or his designated representative.

**1.2.6** As Directed - In these specifications the words "as directed" shall refer to the directions to the Contractor from the Owner or his designated representative.



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## **2.0 GENERAL CONDITIONS**

- 2.1** The Contractor shall furnish all labor, material and equipment and perform all work and services except those set out and furnished by the Owner, necessary to complete in a satisfactory manner the site preparation, excavation, filling, compaction, grading as shown on the plans and as described therein.

This work shall consist of all mobilization clearing and grading, grubbing, stripping, removal of existing material unless otherwise stated, preparation of the land to be filled, filling of the land, spreading and compaction of the fill, and all subsidiary work necessary to complete the grading of the cut and fill areas to conform with the lines, grades, slopes, and specifications.

This work is to be accomplished under the observation of the Owner or his designated representative.

- 2.2** Prior to bidding the work, the Contractor shall examine, investigate and inspect the construction site as to the nature and location of the work, and the general and local conditions at the construction site, including, without limitation, the character of surface or subsurface conditions and obstacles to be encountered on and around the construction site; and shall make such additional investigation as he may deem necessary for the planning and proper execution of the work.

If conditions other than those indicated are discovered by the Contractor, the Owner should be notified immediately. The material which the Contractor believes to be a changed condition should not be disturbed so that the owner can investigate the condition.

- 2.3** The construction shall be performed under the direction of an experienced engineer who is familiar with the design plan.



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## II - ENGINEERED FILL BENEATH STRUCTURES CLEARING AND GRADING SPECIFICATIONS

### **1.0 GENERAL CONDITIONS**

The Contractor shall furnish all labor, materials, and equipment, and perform all work and services necessary to complete in a satisfactory manner the site preparation, excavation, filling, compaction and grading as shown on the plans and as described therein.

This work shall consist of all clearing and grading, removal of existing structures unless otherwise stated, preparation of the land to be filled, filling of the land, spreading and compaction of the fill, and all subsidiary work necessary to complete the grading of the cut and fill areas to conform with the lines, grades, slopes, and specifications.

This work is to be accomplished under the constant and continuous supervision of the Owner or his designated representative.

In these specifications, the terms "approved" and "as directed" shall refer to directions to the Contractor from the Owner or his designated representative.

### **2.0 SUBSURFACE CONDITIONS**

Prior to bidding the work, the Contractor shall examine, investigate and inspect the construction site as to the nature and location of the work, and the general and local conditions at the construction site, including without limitation, the character of surface or subsurface conditions and obstacles to be encountered on and around the construction site; and shall make such additional investigation as he may deem necessary for the planning and proper execution of the work. Borings and/or soil investigations shall have been made. Results of these borings and studies will be made available by the Owner to the Contractor upon his request, but the Owner is not responsible for any interpretations or conclusions with respect thereto made by the Contractor based on such information, and the Owner further has no responsibility for the accuracy of the borings and the soil investigations.

If conditions other than those indicated are discovered by the Contractor, the Owner should be notified immediately. The material which the Contractor believes to be a changed condition should not be disturbed so that the Owner can investigate the condition.

### **3.0 SITE PREPARATION**

Within the specified areas, all trees, brush, stumps, logs, tree roots, and structures scheduled for demolition shall be removed and disposed of.

All cut and fill areas shall be properly stripped. Topsoil will be removed to its full depth and stockpiled for use in finish grading. Any rubbish, organic and other objectionable soils, and other deleterious material shall be disposed of off the site, or as directed by the Owner or his designated representative if on site disposal is



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provided. In no case shall such objectionable material be allowed in or under the fill unless specifically authorized in writing.

Prior to the addition of fill, the original ground shall be compacted to job specifications as outlined below. Special notice shall be given to the proposed fill area now. If wet spots, spongy conditions, or groundwater seepage is found, corrective measures must be taken before the placement of fill.

### **4.0 FORMATION OF FILL AREAS**

Fills shall be formed of satisfactory materials placed in successive horizontal layers of not more than eight (8) inches in loose depth for the full width of the cross-section. The depth of lift may be increased if the Contractor can demonstrate the ability to compact a larger lift. If compaction is accomplished using hand-tamping equipment, lifts will be limited to 4-inch loose lifts. Engineered fill placed below the structure bearing elevation shall be compacted to at least 95% of the maximum dry unit weight with a moisture content within 2% of the optimum moisture content as determined by the modified Proctor test. The top size of the material placed shall not exceed 4 inches.

All material entering the fill shall be free of organic matter such as leaves, grass, roots, and other objectionable material.

The operations on earth work shall be suspended at any time when satisfactory results cannot be obtained because of rain, freezing weather, or other unsatisfactory conditions. The Contractor shall keep the work areas graded to provide the drainage always.

The fill material shall be of the proper moisture content before compaction efforts are started. Wetting or drying of the material and manipulation to secure a uniform moisture content throughout the layer shall be required. Should the material be too wet to permit proper compaction or rolling, all work thus affected shall be delayed until the material has dried to the required moisture content. The moisture content of the fill material should be no more than two (2) percentage points higher or lower than optimum unless otherwise authorized. Sprinkling shall be done with equipment that will satisfactorily distribute the water over the disced area. Any areas inaccessible to a roller shall be consolidated and compacted by mechanical tampers. The equipment shall be operated in such a manner that hardpan, cemented gravel, clay or other chunky soil material will be broken up into small particles and become incorporated with the other material in the layer.

In the construction of filled areas, starting layers shall be placed in the deepest portion of the fill, and as placement progresses, additional layers shall be constructed in horizontal planes. Original slopes shall be continuously, vertically benched to provide horizontal fill planes. The size of the benches shall be formed so that the base of the bench is horizontal, and the back of the bench is vertical. As many benches as are necessary to bring the site to final grade shall be constructed. Filling operations shall begin on the lowest bench, with the fill being



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placed in horizontal eight (8) inch thick loose lifts unless otherwise authorized. The filling shall progress in this manner until the entire first bench has been filled, before any fill is placed on the succeeding benches. Proper drainage shall be maintained always during benching and filling of the benches, to ensure that all water is drained away from the fill area.

Frozen material shall not be placed in the fill nor shall the fill be placed upon frozen material.

The Contractor shall be responsible for the stability of all fills made under the contract, and shall replace any portion, which in the opinion of the Owner or his designated representative, has become displaced due to carelessness or negligence on the part of the Contractor. Fill damaged by inclement weather shall be repaired at the Contractor's expense.

### **5.0 SLOPE RATIO AND STORM WATER RUN-OFF**

Slopes shall not be greater than 2 (horizontal) to 1 (vertical) in both cut and fill, or as illustrated on the construction drawings. Excavations shall be constructed in accordance with all Federal, State and local codes relative to slope geometry.

### **6.0 GRADING**

The Contractor shall furnish, operate, and maintain such equipment as is necessary to construct uniform layers, and control smoothness of grade for maximum compaction and drainage.

### **7.0 COMPACTING**

The compaction equipment shall be approved equipment of such design, weight, and quantity to obtain the required density in accordance with these specifications.

### **8.0 TESTING AND INSPECTION SERVICES**

Testing and inspection services will be provided by the Owner.



## GUIDELINES FOR EXCAVATIONS AND TRENCHES

The following represents some general guidelines relative to the design and construction of excavations and trenches. It must be emphasized that these guidelines are not intended to represent a "safety plan," but rather are presented herein to provide general guidance regarding the design characteristics and safety measures for excavations and trenches.

1. Check with the following utilities prior to breaking ground:

- Sewer
- Telephone
- Fuel
- Electric
- Water
- Gas
- Cable

When utility companies or owners do not respond to your request within 48 hours, the contractor may only then proceed provided the contractor does so with caution by using detection equipment or other acceptable means to locate utility installations.

Once the excavation is open, the contractor should protect and support the exposed underground utilities or remove installations to safeguard workers and prevent damage to exposed utilities.

2. Access and egress ramps must be designed by a "competent person" and structural ramps used for equipment must be designed by a "competent person" with qualified knowledge in structural design. In addition:

- Ramps must be secured to prevent displacement;
- Ramps used in lieu of steps must have cleats to prevent slipping; and
- Trenching excavations four feet or greater in depth must have a stairway, ladder, ramps or other safe means to egress with lateral travel no more than 25 feet.

3. Workers must be provided with reflector garments, such as warning orange or red vests, when exposed to vehicular traffic.

4. Contractors must not allow workers to work under or near equipment when there is danger of falling debris, spillage or equipment-related injuries.



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5. Mobile equipment, operating adjacent to an open excavation or approaching the edge of an excavation, must have one of the following when the operator's view is obstructed:
  - Warning System
  - Mechanical Signals
  - Barricades
  - Stop Logs
  - Hand Signals
6. The contractor must check the atmosphere for hazardous gases and oxygen deficiencies when excavating four feet or greater around landfills, or when hazardous substances are stored nearby, and when the contractor expects there could be any exposure to the workers.
7. When hazardous atmospheric conditions exist, or when conditions could change, the contractor must make emergency rescue equipment readily available including breathing apparatus, safety harnesses with life lines and a basket stretcher.
8. When workers enter bell-bottom pier holes or other deep and confined excavations, the worker must wear (always while performing work in the confined space) a separate life line attached to a harness. The line must be attended by someone above while work is being performed. The worker must check for hazardous atmospheric conditions prior to entry.
9. The contractor must ensure that water does not accumulate in open excavations and must inspect the excavation prior to allowing workers to re-enter after heavy rains.
10. Adjacent structures (buildings, walls, etc.) must be supported or secured to prevent worker exposure to unsafe conditions and damage to existing structures.
11. A registered professional engineer must approve operations when a contractor underpins existing structures to ensure worker safety and prevent damage to existing structures.
12. Workers must not be exposed to loose soil and rock or materials in and around excavations. Materials, such as removed soil and rock, must not be stored closer than two feet from the edge of the excavation.
13. Daily inspections of the excavation, the adjacent areas and protective systems must be made by a "competent person" for evidence of possible cave-ins, indications of failure of protective systems, hazardous atmospheres or other hazardous conditions. The "competent person" must



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stop work immediately and remove workers from the excavation when conditions change and pose a threat to their safety.

- 14.** Workers must not be exposed to fall hazards associated with excavations. Protective walkways or bridges with standard guard rails must be provided.
- 15.** All wells, pits, shafts etc. must be barricaded or covered. After completion of work, all wells, pits, shafts etc. must be backfilled.



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## IV - DRILLED PIER INSTALLATION

### 1.0 DRILLING PROCEDURE

- 1.1 Drilled piers will be installed with large caisson drill rigs capable of torque and crowd forces sufficient to install drilled piers at the project site given the in-situ soil conditions.
  
- 1.2 The drill rig kelly bar and auger will be carefully and accurately placed over the centerline of the drilled pier. The Contractor is responsible for providing necessary surveying to verify drilled pier location before, during, and after the drilled pier installation.
  
- 1.3 The augers are advanced downwards as they are rotated such that drilling of the soil mass is efficiently accomplished. Depending on the subsurface conditions, and the requirements for the given project, a temporary steel casing should be installed at this time to preclude caving of the soil and/or broken rock mass being penetrated.

### 2.0 CASING INSTALLATION

- 2.1 The casing will be checked for centerline accuracy and plumbness by the Contractor's survey crew. During casing installation, the Contractor's survey crew will verify alignment with instruments. If plumbness and alignment are not within tolerance as determined by the Contractor's survey crew, the casing will be extracted and re-aligned as necessary.
  
- 2.2 The drill rig will remove soil and bedrock material from within the casing to the drilled pier design tip elevation. A steel casing or "Sonotube" shall be inserted into the borehole to preclude cave-ins and/or instability in the borehole.



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- 2.3** The bearing surface within the drilled pier will be inspected by a registered Professional Engineer before being approved for structural concreting.

### **3.0 INSTALLATION OF THE REBAR CAGE**

- 3.1** An epoxy coated spiral reinforcing steel cage will be installed while in the drilled pier borehole.
- 3.2** To assist in assuring that the reinforcing steel cage does not settle during concrete pumping, a mat of reinforcing steel bars will be installed across the bottom of the reinforcing steel cage perpendicular to the vertical axis of the cage. The exact number of bars will be determined and installed by the Structural Engineer. The number of rebar boots used on the bottom of the cage will also be determined by the Structural Engineer.
- 3.3** The reinforcing steel cage will be lowered into the drilled pier borehole, while drilled pier spacers are placed at intervals as required by the Structural Engineer. The reinforcing steel cage will be checked for alignment by the Contractors survey crew.
- 3.4** The crane will remain attached to the reinforcing steel cage while the concrete pump outlet pipe is lowered to just above the bottom of the drilled pier. The concrete pump pipe sections will be welded together to assure that do not separate during pumping.

### **4.0 CONCRETING OF THE DRILLED PIER**

- 4.1** Concrete pumping may commence once the bearing surface has been approved in accordance with Clause 2.3



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- 4.2** A three-inch trash pump will be used to pump slurry and/or water from within the casing and from above the newly pumped concrete.
- 4.3** The concrete pump outlet pipe will maintain at least ten (10) feet of embedment into the fresh concrete. The concrete level in the casing will be monitored.
- 4.4** The casing will be completely extracted with the crane and/or vibratory hammer. Caisson clamps on the vibratory hammer (if applicable) will be adjusted to the proper dimension to withdraw the casing.
- 4.5** The concrete will be terminated at the top of drilled pier elevation and screeded flat.
- 4.6** The upper reinforcing steel dowel cage will be lowered into the concrete to the embedment elevation. If necessary, the concrete will be vibrated to assist in placement. Alignment will be verified by the Contractors survey crew and the cage will be sufficiently braced.



## V - GENERAL CONCRETE SPECIFICATIONS

### 1.0 GENERAL

It is the intent of this specification to secure, for every part of the work, concrete of homogenous structure which, when hardened, will have the required strength and resistance to weathering. To this end, the limiting values of concrete and the requirements hereinafter specified must be met. Standard tests of the cement, aggregates, concrete and reinforcement will be made by the Owner as it sees fit. The Contractor shall furnish the material for all required samples plus such labor as required to obtain samples. The Contractor shall provide to authorized representatives of the Owner, convenient access to all parts of the work of all concreting operations for the purpose of sampling and inspection.

### 2.0 SCOPE

Contractor shall furnish all materials, labor, services, transportation, tools, equipment, and related items required to complete work indicated on the drawings and/or specified.

Unless otherwise noted or as modified by more stringent requirements specified herein, all plain and reinforced concrete work shall be performed in full compliance with applicable requirements of the Building Code Requirements for Reinforced Concrete ACI 318.

Contractor shall obtain Owner's approval of all subgrades, footing bottoms, forms, and reinforcement just prior to placing concrete.

Contractor shall coordinate the work specified in this section with that specified in other sections so that all anchors, pipes and other embedded items are properly installed before concrete is placed.

Contractor shall clean all exposed concrete surfaces and obtain approval of Owner for method of cleaning

### 3.0 MATERIALS

All materials shall be of the respective quality specified herein, delivered, stored, and handled as to prevent inclusion of foreign matter and damage by dampness or breakage. Packaged material shall be stored in original container until ready for use. Materials showing evidence of dampness or other damage may be rejected.

A. Fine and Coarse Aggregates: Coarse and fine aggregates shall conform to ASTM Specification C33. The maximum size of aggregate shall not be larger than one-fifth (1/5) of the narrowest dimensions between forms, or larger than three fourths (3/4) of the minimum clear spacing between reinforcement.

1. Fine Aggregate: Sand shall be composed essentially of clean, hard, strong, durable grains free of structurally weak



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- grains, organic matter, loam, clay, silt, salt, mica or other fine materials that may affect bonding of the cement paste.
2. Coarse Aggregate: Cement concrete shall consist of crushed rock or screened gravel and shall be composed essentially of clean, hard, strong and impermeable particles, resistant to wear and frost and free from deleterious amounts of organic matter, loam, clay, salts, mica, and soft, thin, elongated, laminated or disintegrated stone, and shall be inert to water and cement.
- B. Portland Cement: Portland cement shall conform to ASTM Specification C150. Type I or Type II Portland Cement shall be used provided that they are not intermixed during any one batch. Type II Portland Cement shall not be used unless indicated on the plans.
- C. Water: Water for mixing and curing shall be clean, fresh, and free from deleterious materials.
- D. Metal Reinforcement: Rebar shall be Grade 60 and with deformations conforming to ASTH Specification A305. Welded wire mesh shall conform to W4 x W4 size and be of Grade 60 steel.
- E. Admixtures: Except as herein noted, admixtures shall not be used.
1. Under adverse weather conditions only retarding or accelerating agents containing no chloride may be used.
  2. Air-Entraining Agent shall be used for all concrete will give an entrained air range of not less than 4 percent but no greater than 8 percent in the finished product. Under no circumstances shall the air-entraining be interground with cement.
  3. Approval in writing shall be required from Owner prior to the use of any admixture.

### 4.0 FORM

Forms shall be constructed with proper shoring and cross-bracing, safeguarding the total structure and specifically lateral stability and sufficiently strong to stand vibrations of concrete and to carry, without appreciable deflection or displacement, all dead and live loads to which they may be subjected.

### 5.0 INSERTS, ETC.

Anchors, bolts, dowels, conduit, water stops, vent pipes and other similar built-in or concreted-in items shall be properly located, accurately positioned and secured. The Contractor shall cooperate in placing of such items with other contractors who require a fastening device for their work and he shall maintain them in proper location during the progress of his work.



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## 6.0 REINFORCEMENT

Reinforcement at the time concrete is placed shall be free from rust, scale or other coatings that will destroy or reduce the bond.

Reinforcement shall be accurately placed and securely tied at intersections and shall be securely held in position during the placing of concrete by pacers, chairs, or other approved supports.

The reinforcement of foundations, footings and other principal structural members in which the concrete is deposited against the ground shall not have less than three (3) inches of concrete between it and the ground contact surface. If concrete surfaces after removal of the forms are to be exposed to the weather or to be in contact with the ground or rock, reinforcement shall be protected with not less than two (2) inches of concrete,

## 7.0 CONCRETE

Concrete for the various parts of the work shall be of 4000 pounds per square inch compressive strength with a minimum 28-day cure. Contractor is responsible to provide a mix of not less than 6 bags of cement per yard of concrete and not more than 7 gallons of water per bag of cement, producing a minimum slump of 2-1/2 inches and a maximum slump of 4-1/2 inches. Concrete that exceeds the above range of maximum or minimum slump requirements may be rejected by the Owner. All concrete shall be air-entrained. Contractors are required to furnish the name or names of the company(s) that will be providing the mix. The Owner reserves the right to disapprove any concrete supplier that has been known to supply an undesirable material to the Owner on previous occasions.

## 8.0 DEPOSITING CONCRETE

4.1. Preparation for Placing Concrete: Before depositing concrete, the Contractor shall:

1. Remove from space to be occupied by concrete all debris, including snow, ice, and water unless otherwise permitted by Owner.
  2. Provide diversion, satisfactory to Owner, of any flow of water to an excavation to avoid washing the freshly deposited concrete.
  3. Coat the forms prior to placing of reinforcing steel as required in form work.
  4. Secure firmly in correct position, all reinforcement and other items to be encased and remove therefrom all coating including ice and frost.
- B. Transportation of Concrete from Batch Plant: The concrete shall be delivered to the site of the work and discharge shall be completed within 90 minutes after addition of the cement and water to the aggregates. Each batch of concrete delivered at the job site shall be



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accompanied by a time slip issued at the batching plant, bearing the time of charging of the mixer drum with the cement and aggregates.

- C. Transporting of Concrete from Mixer to Place of Final Deposit: Transportation shall be done as rapidly as practical by means which shall prevent the separation or loss of the ingredients. If chutes are used, they shall be at a slope not flatter than one vertical to two horizontal. Buggies or carts shall be equipped with pneumatic rubber tires or surfaces of runways shall be sufficiently smooth or both so as not to cause separation or segregation of concrete ingredients. Concrete shall not be allowed to drop freely more than 4 feet. Where greater drops are required, canvas "elephant trunks" or galvanized iron chutes equipped with suitable hopper heads shall be employed and a sufficient number placed to ensure that the concrete may be effectively compacted into horizontal layers not exceeding 12 inches in thickness with minimum lateral movements.
- D. Depositing of Concrete: Depositing of concrete shall:
1. Proceed continuously after once starting until reaching the end of a section of construction joint location shown on the drawings, or as approved by the Owner. The operations shall be conducted so that no concrete is deposited on concrete sufficiently hardened to cause formation of seams, and planes of weakness.
  2. Be as near as practical to its final position in the forms.
  3. Proceed to maintain constantly a top surface which is approximately level.
  4. Be placed before initial set has occurred, and in no event after it has contained its water content for more than 90 minutes.
  5. Be thoroughly worked and compacted by means of suitable tools to provide impermeability, durability and strength and shall be thoroughly worked around reinforcements and embedded items and into corners of forms and to be free from voids, pockets or honeycombing. Care shall be taken to provide impermeability.
- E. Vibration Equipment: Vibration equipment shall be of the appropriate type and shall, always, be adequate in number of units and power of each unit to properly consolidate all concrete.



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- F. Monolithic Pours: Proper delivery of concrete shall be the Contractor's responsibility to make a mono-lithic pour without delays and changes of cold joints.

### 9.0 CURING

All concrete work shall be protected from injurious action by the sun, rain, flowing water, frost and other injury and shall be covered with plastic after application of curing compound for three (3) days on pours located above ground.

Contractor shall not remove any formwork for a minimum period of 24 hours after a concrete pour without written approval of the Owner.

### 10.0 CONCRETE FINISHES

Finishes of all exposed concrete shall be free of defects which impair its durability or adversely affect its appearance. All such surfaces when stripped, shall be uniform in appearance and any surfaces displaying any deviations from adjacent uniform surfaces shall be rejected and subject to removal.

Finished work shall be level and plumb, true to lines, and dimensions. Finished plane surfaces shall be smooth, and as nearly perfect as practical; however, deviations from a true plane shall not exceed 1/8 inch when measured from a 6-foot straight edge placed against the surface to any point on the surface and under the straight edge.

All exposed surfaces shall have defects corrected, protrusions removed, and holes filled.



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|                               |
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| <b>APPENDIX A BORING LOGS</b> |
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# EAST KENTUCKY ENGINEERING, LLC.

## APPENDIX B CORE PHOTOGRAPHS





# EAST KENTUCKY ENGINEERING, LLC.





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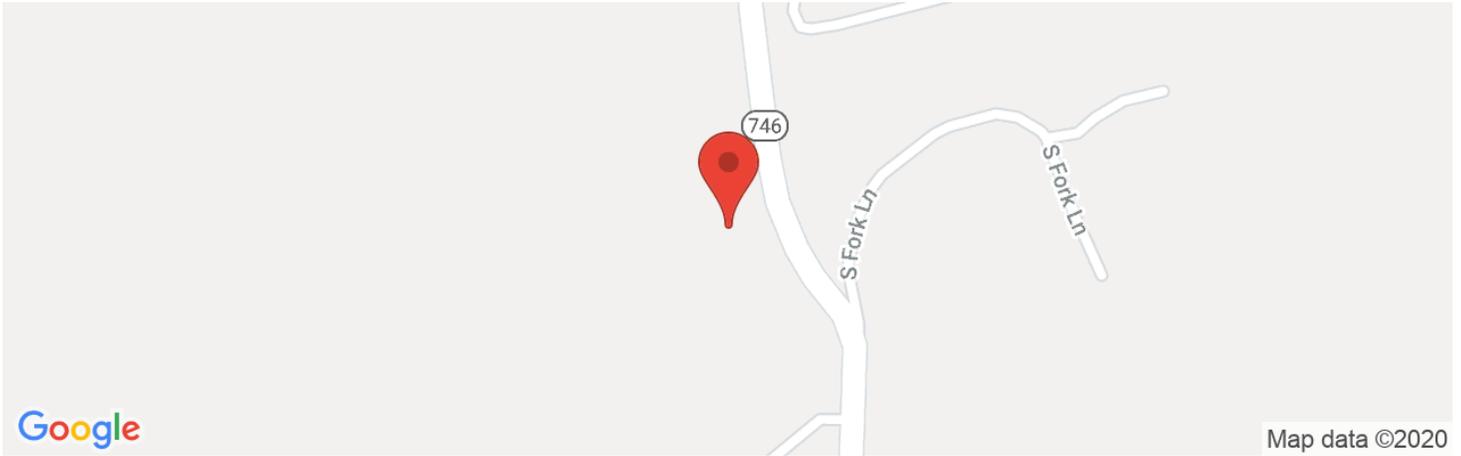
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**APPENDIX C SEISMIC DATA**



# Campton North

Latitude, Longitude: 37.7640, -83.5263



|                                       |                       |
|---------------------------------------|-----------------------|
| <b>Date</b>                           | 10/6/2020, 4:23:56 PM |
| <b>Design Code Reference Document</b> | IBC-2015              |
| <b>Risk Category</b>                  | IV                    |
| <b>Site Class</b>                     | A - Hard Rock         |

| Type            | Value | Description   |
|-----------------|-------|---|
| S <sub>S</sub>  | 0.196 | MCE <sub>R</sub> ground motion. (for 0.2 second period) |
| S <sub>1</sub>  | 0.087 | MCE <sub>R</sub> ground motion. (for 1.0s period)       |
| S <sub>MS</sub> | 0.157 | Site-modified spectral acceleration value               |
| S <sub>M1</sub> | 0.07  | Site-modified spectral acceleration value               |
| S <sub>DS</sub> | 0.105 | Numeric seismic design value at 0.2 second SA           |
| S <sub>D1</sub> | 0.047 | Numeric seismic design value at 1.0 second SA           |

| Type             | Value | Description   |
|------------------|-------|---|
| SDC              | A     | Seismic design category   |
| F <sub>a</sub>   | 0.8   | Site amplification factor at 0.2 second   |
| F <sub>v</sub>   | 0.8   | Site amplification factor at 1.0 second   |
| PGA              | 0.096 | MCE <sub>G</sub> peak ground acceleration   |
| F <sub>PGA</sub> | 0.8   | Site amplification factor at PGA  |
| PGA <sub>M</sub> | 0.077 | Site modified peak ground acceleration  |
| T <sub>L</sub>   | 12    | Long-period transition period in seconds  |
| SsRT             | 0.196 | Probabilistic risk-targeted ground motion. (0.2 second)                                   |
| SsUH             | 0.212 | Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration  |
| SsD              | 1.5   | Factored deterministic acceleration value. (0.2 second)                                   |
| S1RT             | 0.087 | Probabilistic risk-targeted ground motion. (1.0 second)                                   |
| S1UH             | 0.097 | Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration. |
| S1D              | 0.6   | Factored deterministic acceleration value. (1.0 second)                                   |
| PGAd             | 0.6   | Factored deterministic acceleration value. (Peak Ground Acceleration)                     |
| C <sub>RS</sub>  | 0.926 | Mapped value of the risk coefficient at short periods                                     |
| C <sub>R1</sub>  | 0.903 | Mapped value of the risk coefficient at a period of 1 s                                   |

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# EAST KENTUCKY ENGINEERING, LLC.

## APPENDIX D PHOTOGRAPHS

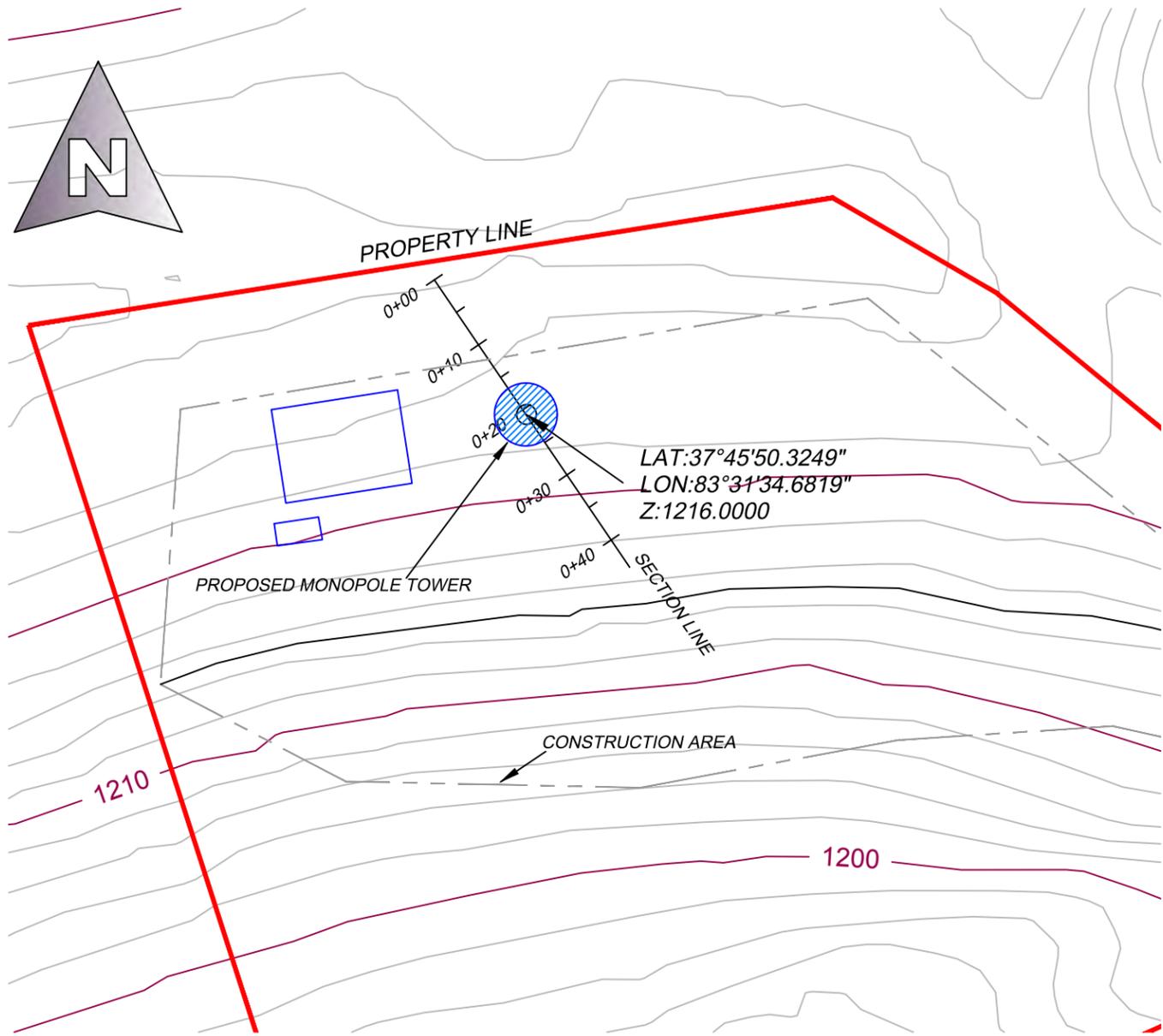




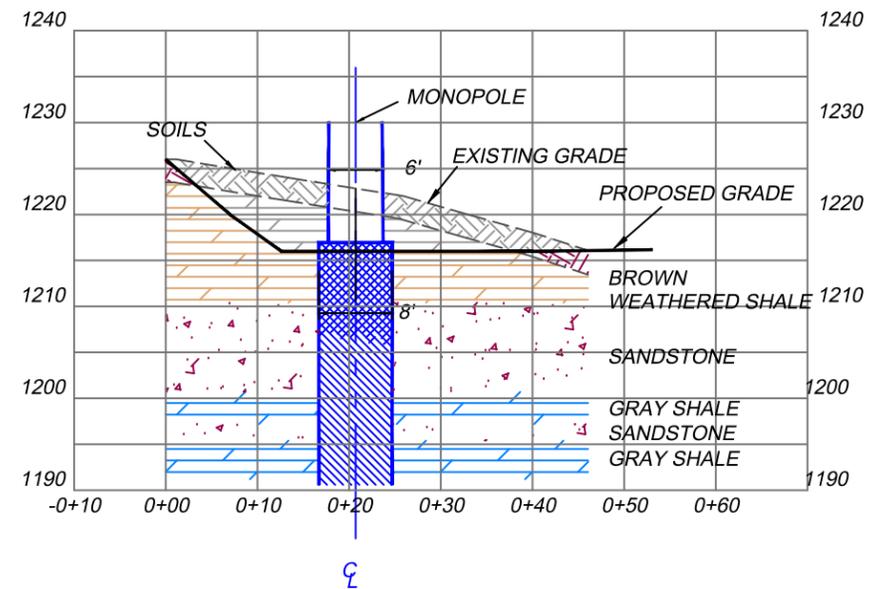
**EAST KENTUCKY ENGINEERING, LLC.**

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**APPENDIX E  
MAPS**



PLAN VIEW  
1" = 20'



SECTION LINE  
1" = 20'

East Kentucky Engineering, LLC

230 Swartz  
Hazard, KY 41701  
(606) 551-1050  
Email: ekyeng@ekyeng.net



0' 20' 40'



Drawn by: RDS

10/5/2020

Job #: 165-000-0117

Scale: 1" = AS NOTED

File Location:

APPALACHIAN WIRELESS  
PROPOSED CAMPTON NORTH TOWER  
WOLFE COUNTY  
KENTUCKY

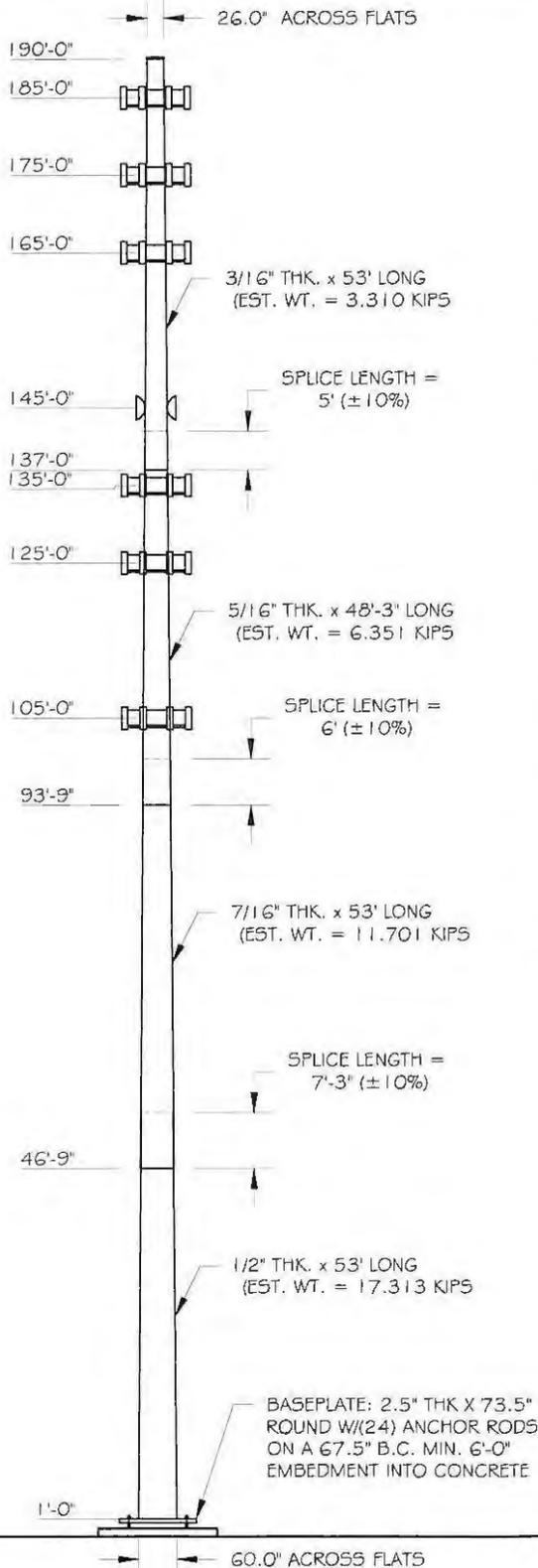
**Exhibit 5**



# TAPP

2427 Kelly Lane  
Houston, Texas 77066  
281-444-8277

QUALITY STEEL POLES. DELIVERED.



|   |                        |
|---|------------------------|
| Page 1 of 2                                     | Job Number: 23520-441  |
| Eng: MFP  | Customer Ref: TP-19363 |
|   | Date: 10/30/2020       |
| Structure: 190-FT MONOPOLE                      |                        |
| Site: CAMPTON NORTH                             |                        |
| Location: WOLFE CO., KY / 37°45'50", -83°31'35" |                        |
| Owner: APPALACHIAN WIRELESS                     |                        |
| Revision No.:      Revision Date:               |                        |

### DESIGN

|   |                  |                    |               |
|---|------------------|--------------------|---------------|
| Building Code: 2018 KENTUCKY BUILDING CODE                                |                  |                    |               |
| Design Standard: ANSI/TIA-222-G   |                  |                    |               |
| Wind Speed Load Cases: ASCE-7-05 CONVERTED TO ASCE-7-10                   |                  |                    |               |
| Load Case #1: 90 MPH Design Wind Speed - $V_{AS3}$ ( $V_{dir} = 116$ MPH) |                  |                    |               |
| Load Case #2: 30 MPH Wind with 0.75" Ice Accumulation                     |                  |                    |               |
| Load Case #3: 60 MPH Service Wind Speed                                   |                  |                    |               |
| Structure Class Risk Category: II   | Exposure Cat.: C | Topography Cat.: I | Crest Height: |

STRUCTURE MEETS THE MINIMUM REQUIREMENTS OF TIA-222-H

### EQUIPMENT LIST

| Elev. | Description                  |
|-------|------------------------------|
| 185   | (12) NN-G5A-M + (12) RRU     |
| 185   | 12-FT PLATFORM WITH HANDRAIL |
| 175   | (12) NN-G5A-M + (12) RRU     |
| 175   | 12-FT PLATFORM WITH HANDRAIL |
| 165   | (12) NN-G5A-M + (12) RRU     |
| 165   | 12-FT PLATFORM WITH HANDRAIL |
| 145   | (2) 4-FT DISH                |
| 145   | DUAL MICROWAVE MOUNT         |
| 135   | (12) NN-G5A-M + (12) RRU     |
| 135   | 12-FT PLATFORM WITH HANDRAIL |
| 125   | (12) NN-G5A-M + (12) RRU     |
| 125   | 12-FT PLATFORM WITH HANDRAIL |
| 105   | (12) NN-G5A-M + (12) RRU     |
| 105   | 12-FT PLATFORM WITH HANDRAIL |

ANTENNA FEED LINES ROUTED ON THE INSIDE OF THE POLE

### STRUCTURE PROPERTIES

| Cross-Section: 18-Sided                    | Taper: 0.18981 in/ft             |                |             |               |               |
|--|----------------------------------|----------------|-------------|---------------|---------------|
| Shaft Steel: ASTM A572 GR 65               | Baseplate Steel: ASTM A572 GR 50 |                |             |               |               |
| Anchor Rods: 2.25 in. AG 15 GR. 75 X 7'-0" |                                  |                |             |               |               |
| Sect.                                      | Length (ft)                      | Thickness (in) | Splice (ft) | Top Dia. (in) | Bot Dia. (in) |
| 1  | 53.00                            | 0.1875         | 5.00        | 26.00         | 36.06         |
| 2  | 48.25                            | 0.3125         | 6.00        | 34.74         | 43.89         |
| 3  | 53.00                            | 0.4375         | 7.25        | 42.13         | 52.19         |
| 4  | 53.00                            | 0.5000         | 0.00        | 49.94         | 60.00         |



MICHAEL F. PLAHOVINSAK, P.E. #25466  
Soil Inspector - Independent Engineer  
18301 S.R. 161, Plain City, OH 43064  
614-398-6250 / mike@mfpeng.com

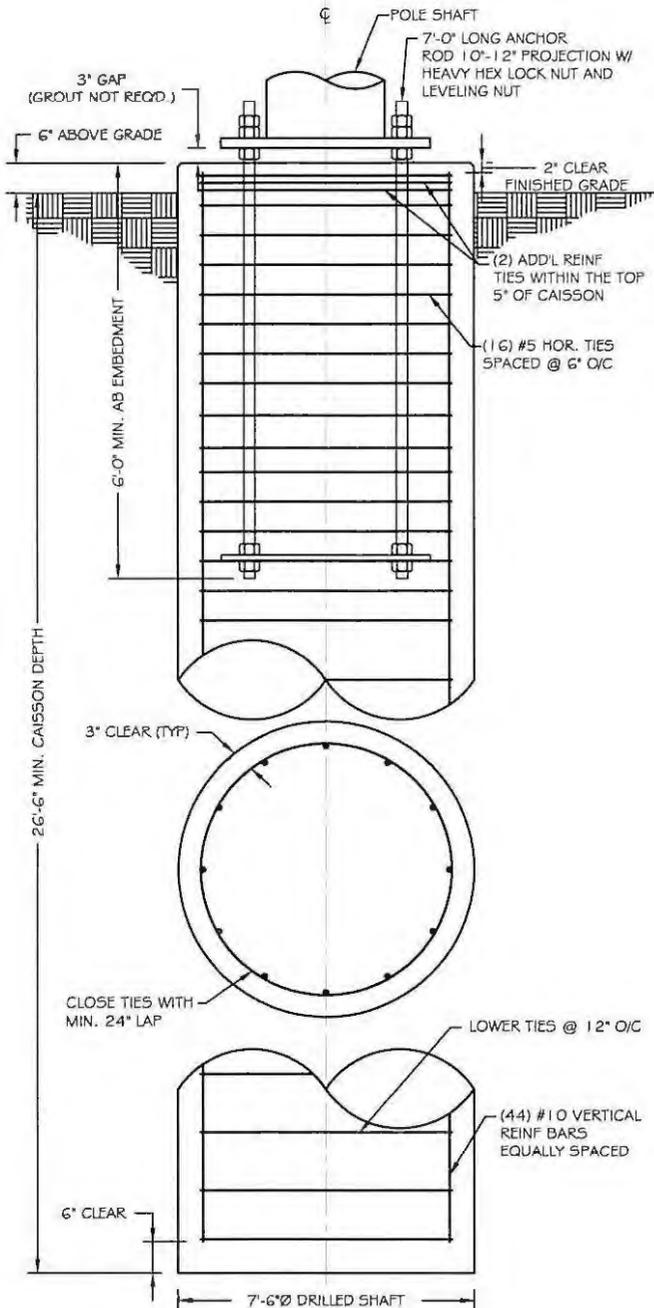
### BASE REACTIONS FOR FOUNDATION DESIGN

Moment: 7782 ft-kip  
Shear: 57 kip  
Axial: 89 kip

|               |                                       |
|---------------|---------------------------------------|
| Page 2 of 2   | Job Number: 23520-441                 |
| Eng: MFP      | Customer Ref: TP-19363                |
|               | Date: 10/30/2020                      |
| Structure:    | 190-FT MONOPOLE                       |
| Site:         | CAMPTON NORTH                         |
| Location:     | WOLFE CO., KY / 37°45'50", -83°31'35" |
| Owner:        | APPALACHIAN WIRELESS                  |
| Revision No.: | Revision Date:                        |

FOUNDATION NOTES:

1. ALL FOUNDATION CONCRETE SHALL USE TYPE II CEMENT AND ATTAIN A MINIMUM COMPRESSIVE STRENGTH OF 4000 PSI AT 28 DAYS. CONCRETE SHALL HAVE A MAXIMUM WATER/CEMENT RATIO OF 0.46. IN AREAS OF POTENTIAL FREEZING, CONCRETE SHALL BE AIR ENTRAINED 6% ( $\pm 1.5\%$ ). ALL CONCRETE CONSTRUCTION SHALL BE IN ACCORDANCE WITH ACI 318, 'THE BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE', LATEST EDITION.
2. ALL REINFORCING STEEL SHALL CONFORM TO ASTM A615 VERTICAL BARS SHALL BE GRADE 60, AND TIES OR STIRRUPS SHALL BE A MINIMUM OF GRADE 40. THE PLACEMENT OF ALL REINFORCEMENT SHALL CONFORM TO ACI 315, 'MANUAL OF STANDARD PRACTICE FOR DETAILING REINFORCED CONCRETE STRUCTURES', LATEST EDITION.
3. CAISSON FOUNDATION INSTALLATION SHALL BE IN ACCORDANCE WITH ACI 336, 'STANDARD SPECIFICATIONS FOR THE CONSTRUCTION OF DRILLED PIERS', LATEST EDITION.
4. THE CONTRACTOR SHALL DETERMINE THE MEANS AND METHODS TO SUPPORT THE EXCAVATION DURING CONSTRUCTION. THE CONTRACTOR SHALL READ THE GEOTECHNICAL REPORT AND SHALL CONSULT THE GEOTECHNICAL ENGINEER AS NECESSARY PRIOR TO CONSTRUCTION.
5. FOUNDATION DESIGN IS BASED ON GEOTECHNICAL REPORT BY:  
ENGINEER: EAST KENTUCKY ENGINEERING  
REPORT NO.: 165-000-0117 (DATED 10/6/20)
6. ESTIMATED CONCRETE VOLUME = 44 CUBIC YARDS.
7. THE FOUNDATION HAS BEEN DESIGNED TO RESIST THE FOLLOWING FACTORED LOADS:  
MOMENT: 7782 FT\*KIPS  
SHEAR: 57 KIPS  
AXIAL: 89 KIPS



**CAISSON FOUNDATION**

NOT TO SCALE



|   |  |                                  |
|---|--|----------------------------------|
| <b>tnxTower</b><br><br><b>Michael Plahovinsak, P.E.</b><br>18301 State Route 161<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>FAX: mike@mfpeng.com | <b>Job</b><br>190-ft Monopole - MFP #23520-441 | <b>Page</b><br>1 of 8            |
|   | <b>Project</b><br>Campton North                | <b>Date</b><br>17:36:30 10/30/20 |
|   | <b>Client</b><br>TP-19363                      | <b>Designed by</b><br>JC         |

### Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in Wolfe County, Kentucky.

Basic wind speed of 90 mph.

Structure Class II.

Exposure Category C.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 0.7500 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 30 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

### Tapered Pole Section Geometry

| Section | Elevation<br>ft | Section Length<br>ft | Splice Length<br>ft | Number of Sides | Top Diameter<br>in | Bottom Diameter<br>in | Wall Thickness<br>in | Bend Radius<br>in | Pole Grade          |
|---------|-----------------|----------------------|---------------------|-----------------|--------------------|-----------------------|----------------------|-------------------|---------------------|
| L1      | 190.00-137.00   | 53.00                | 5.00                | 18              | 26.0000            | 36.0602               | 0.1875               | 0.7500            | A572-65<br>(65 ksi) |
| L2      | 137.00-93.75    | 48.25                | 6.00                | 18              | 34.7361            | 43.8947               | 0.3125               | 1.2500            | A572-65<br>(65 ksi) |
| L3      | 93.75-46.75     | 53.00                | 7.25                | 18              | 42.1308            | 52.1910               | 0.4375               | 1.7500            | A572-65<br>(65 ksi) |
| L4      | 46.75-1.00      | 53.00                |                     | 18              | 49.9398            | 60.0000               | 0.5000               | 2.0000            | A572-65<br>(65 ksi) |

### Tapered Pole Properties

| Section | Tip Dia.<br>in | Area<br>in <sup>2</sup> | I<br>in <sup>4</sup> | r<br>in | C<br>in | I/C<br>in <sup>3</sup> | J<br>in <sup>4</sup> | I/Q<br>in <sup>2</sup> | w<br>in | w/t    |
|---------|----------------|-------------------------|----------------------|---------|---------|------------------------|----------------------|------------------------|---------|--------|
| L1      | 26.3722        | 15.3617                 | 1293.1111            | 9.1634  | 13.2080 | 97.9036                | 2587.9238            | 7.6823                 | 4.2460  | 22.645 |
|         | 36.5875        | 21.3487                 | 3470.8616            | 12.7348 | 18.3186 | 189.4723               | 6946.2902            | 10.6764                | 6.0166  | 32.088 |
| L2      | 36.1875        | 34.1439                 | 5111.6801            | 12.2204 | 17.6459 | 289.6802               | 10230.0864           | 17.0752                | 5.5636  | 17.803 |
|         | 44.5236        | 43.2281                 | 10373.4000           | 15.4717 | 22.2985 | 465.2063               | 20760.4496           | 21.6181                | 7.1755  | 22.961 |
| L3      | 43.8697        | 57.8963                 | 12715.1309           | 14.8011 | 21.4024 | 594.0973               | 25446.9927           | 28.9537                | 6.6450  | 15.189 |
|         | 52.9286        | 71.8662                 | 24318.7306           | 18.3725 | 26.5130 | 917.2375               | 48669.4605           | 35.9399                | 8.4156  | 19.236 |
| L4      | 52.0305        | 78.4610                 | 24229.5243           | 17.5511 | 25.3694 | 955.0679               | 48490.9305           | 39.2379                | 7.9094  | 15.819 |
|         | 60.8485        | 94.4265                 | 42234.2974           | 21.1225 | 30.4800 | 1385.6397              | 84524.1679           | 47.2222                | 9.6800  | 19.36  |

| Tower Elevation<br>ft | Gusset Area<br>(per face)<br>ft <sup>2</sup> | Gusset Thickness<br>in | Gusset Grade | Adjust. Factor<br>A <sub>f</sub> | Adjust. Factor<br>A <sub>r</sub> | Weight Multi. | Double Angle<br>Stitch Bolt<br>Spacing<br>Diagonals<br>in | Double Angle<br>Stitch Bolt<br>Spacing<br>Horizontals<br>in | Double Angle<br>Stitch Bolt<br>Spacing<br>Redundants<br>in |
|-----------------------|--|------------------------|--------------|----------------------------------|----------------------------------|---------------|---|---|--|
| L1                    |  |                        |              | 1                                | 1                                | 1             |   |   |  |

|   |  |                                  |
|---|--|----------------------------------|
| <b>tnxTower</b><br><br><b>Michael Plahovinsak, P.E.</b><br>18301 State Route 161<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>FAX: mike@mfpeng.com | <b>Job</b><br>190-ft Monopole - MFP #23520-441 | <b>Page</b><br>2 of 8            |
|   | <b>Project</b><br>Campton North                | <b>Date</b><br>17:36:30 10/30/20 |
|   | <b>Client</b><br>TP-19363                      | <b>Designed by</b><br>JC         |

| Tower Elevation     | Gusset Area (per face) | Gusset Thickness | Gusset Grade | Adjust. Factor $A_j$ | Adjust. Factor $A_r$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals | Double Angle Stitch Bolt Spacing Horizontals | Double Angle Stitch Bolt Spacing Redundant |
|---------------------|------------------------|------------------|--------------|----------------------|----------------------|--------------|--|--|--|
| ft                  | ft <sup>2</sup>        | in               |              |                      |                      |              | in   | in   | in   |
| 190.00-137.00<br>L2 |                        |                  |              | 1                    | 1                    | 1            |  |  |  |
| 137.00-93.75<br>L3  |                        |                  |              | 1                    | 1                    | 1            |  |  |  |
| 93.75-46.75<br>L4   |                        |                  |              | 1                    | 1                    | 1            |  |  |  |

### Feed Line/Linear Appurtenances - Entered As Area

| Description | Face or Leg | Allow Shield | Exclude From Torque Calculation | Component Type | Placement     | Total Number | $C_A A_A$           | Weight |
|-------------|-------------|--------------|---------------------------------|----------------|---------------|--------------|---------------------|--------|
|             |             |              |                                 |                | ft            |              | ft <sup>2</sup> /ft | plf    |
| 1 5/8"      | C           | No           | Yes                             | Inside Pole    | 185.00 - 1.00 | 18           | No Ice              | 0.00   |
|             |             |              |                                 |                |               |              | 1/2" Ice            | 0.00   |
|             |             |              |                                 |                |               |              | 1" Ice              | 0.00   |
| 1 5/8"      | C           | No           | Yes                             | Inside Pole    | 175.00 - 1.00 | 18           | No Ice              | 0.00   |
|             |             |              |                                 |                |               |              | 1/2" Ice            | 0.00   |
|             |             |              |                                 |                |               |              | 1" Ice              | 0.00   |
| 1 5/8"      | C           | No           | Yes                             | Inside Pole    | 165.00 - 1.00 | 18           | No Ice              | 0.00   |
|             |             |              |                                 |                |               |              | 1/2" Ice            | 0.00   |
|             |             |              |                                 |                |               |              | 1" Ice              | 0.00   |
| 1 5/8"      | C           | No           | Yes                             | Inside Pole    | 145.00 - 1.00 | 2            | No Ice              | 0.00   |
|             |             |              |                                 |                |               |              | 1/2" Ice            | 0.00   |
|             |             |              |                                 |                |               |              | 1" Ice              | 0.00   |
| 1 5/8"      | C           | No           | Yes                             | Inside Pole    | 135.00 - 1.00 | 18           | No Ice              | 0.00   |
|             |             |              |                                 |                |               |              | 1/2" Ice            | 0.00   |
|             |             |              |                                 |                |               |              | 1" Ice              | 0.00   |
| 1 5/8"      | C           | No           | Yes                             | Inside Pole    | 125.00 - 1.00 | 18           | No Ice              | 0.00   |
|             |             |              |                                 |                |               |              | 1/2" Ice            | 0.00   |
|             |             |              |                                 |                |               |              | 1" Ice              | 0.00   |
| 1 5/8"      | C           | No           | Yes                             | Inside Pole    | 105.00 - 1.00 | 18           | No Ice              | 0.00   |
|             |             |              |                                 |                |               |              | 1/2" Ice            | 0.00   |
|             |             |              |                                 |                |               |              | 1" Ice              | 0.00   |

### Feed Line/Linear Appurtenances Section Areas

| Tower Section | Tower Elevation | Face | $A_R$           | $A_F$           | $C_A A_A$ In Face | $C_A A_A$ Out Face | Weight |
|---------------|-----------------|------|-----------------|-----------------|-------------------|--------------------|--------|
|               | ft              |      | ft <sup>2</sup> | ft <sup>2</sup> | ft <sup>2</sup>   | ft <sup>2</sup>    | K      |
| L1            | 190.00-137.00   | A    | 0.000           | 0.000           | 0.000             | 0.000              | 0.00   |
|               |                 | B    | 0.000           | 0.000           | 0.000             | 0.000              | 0.00   |
|               |                 | C    | 0.000           | 0.000           | 0.000             | 0.000              | 1.90   |
| L2            | 137.00-93.75    | A    | 0.000           | 0.000           | 0.000             | 0.000              | 0.00   |
|               |                 | B    | 0.000           | 0.000           | 0.000             | 0.000              | 0.00   |
|               |                 | C    | 0.000           | 0.000           | 0.000             | 0.000              | 3.60   |
| L3            | 93.75-46.75     | A    | 0.000           | 0.000           | 0.000             | 0.000              | 0.00   |
|               |                 | B    | 0.000           | 0.000           | 0.000             | 0.000              | 0.00   |
|               |                 | C    | 0.000           | 0.000           | 0.000             | 0.000              | 4.74   |
| L4            | 46.75-1.00      | A    | 0.000           | 0.000           | 0.000             | 0.000              | 0.00   |
|               |                 | B    | 0.000           | 0.000           | 0.000             | 0.000              | 0.00   |
|               |                 | C    | 0.000           | 0.000           | 0.000             | 0.000              | 4.61   |

|   |  |                                  |
|---|--|----------------------------------|
| <b>tnxTower</b><br><br><b>Michael Plahovinsak, P.E.</b><br>18301 State Route 161<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>FAX: mike@mfpeng.com | <b>Job</b><br>190-ft Monopole - MFP #23520-441 | <b>Page</b><br>3 of 8            |
|   | <b>Project</b><br>Campton North                | <b>Date</b><br>17:36:30 10/30/20 |
|   | <b>Client</b><br>TP-19363                      | <b>Designed by</b><br>JC         |

### Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower Section | Tower Elevation<br>ft | Face or Leg | Ice Thickness<br>in | $A_R$<br>ft <sup>2</sup> | $A_F$<br>ft <sup>2</sup> | $C_d A_d$<br>In Face<br>ft <sup>2</sup> | $C_d A_d$<br>Out Face<br>ft <sup>2</sup> | Weight<br>K |
|---------------|-----------------------|-------------|---------------------|--------------------------|--------------------------|---|--|-------------|
| L1            | 190.00-137.00         | A           | 1.759               | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 0.00        |
|               |                       | B           |                     | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 0.00        |
|               |                       | C           |                     | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 1.90        |
| L2            | 137.00-93.75          | A           | 1.699               | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 0.00        |
|               |                       | B           |                     | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 0.00        |
|               |                       | C           |                     | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 3.60        |
| L3            | 93.75-46.75           | A           | 1.617               | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 0.00        |
|               |                       | B           |                     | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 0.00        |
|               |                       | C           |                     | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 4.74        |
| L4            | 46.75-1.00            | A           | 1.455               | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 0.00        |
|               |                       | B           |                     | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 0.00        |
|               |                       | C           |                     | 0.000                    | 0.000                    | 0.000                                   | 0.000                                    | 4.61        |

### Discrete Tower Loads

| Description                          | Face or Leg | Offset Type | Offsets:<br>Horz<br>Lateral<br>Vert<br>ft<br>ft<br>ft | Azimuth Adjustment<br>° | Placement<br>ft | $C_d A_d$<br>Front<br>ft <sup>2</sup> | $C_d A_d$<br>Side<br>ft <sup>2</sup> | Weight<br>K |      |
|--------------------------------------|-------------|-------------|---|-------------------------|-----------------|---------------------------------------|--------------------------------------|-------------|------|
| (4) Andrew NN-65A-M w/<br>mount pipe | A           | From Face   | 3.00  | 0.0000                  | 185.00          | No Ice                                | 12.41                                | 5.04        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 12.89                                | 5.71        | 0.17 |
|                                      |             |             | 0.00  |                         |                 | 1" Ice                                | 13.38                                | 6.37        | 0.26 |
| (4) Andrew NN-65A-M w/<br>mount pipe | B           | From Face   | 3.00  | 0.0000                  | 185.00          | No Ice                                | 12.41                                | 5.04        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 12.89                                | 5.71        | 0.17 |
|                                      |             |             | 0.00  |                         |                 | 1" Ice                                | 13.38                                | 6.37        | 0.26 |
| (4) Andrew NN-65A-M w/<br>mount pipe | C           | From Face   | 3.00  | 0.0000                  | 185.00          | No Ice                                | 12.41                                | 5.04        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 12.89                                | 5.71        | 0.17 |
|                                      |             |             | 0.00  |                         |                 | 1" Ice                                | 13.38                                | 6.37        | 0.26 |
| (12) Ericsson<br>RRUS22212-B13       | A           | From Face   | 2.00  | 0.0000                  | 185.00          | No Ice                                | 1.86                                 | 1.62        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 2.03                                 | 1.78        | 0.10 |
|                                      |             |             | 0.00  |                         |                 | 1" Ice                                | 2.20                                 | 1.95        | 0.12 |
| 12' Platform w/ Handrail             | C           | None        |   | 0.0000                  | 185.00          | No Ice                                | 30.00                                | 30.00       | 1.80 |
|                                      |             |             |   |                         |                 | 1/2" Ice                              | 35.00                                | 35.00       | 2.60 |
|                                      |             |             |   |                         |                 | 1" Ice                                | 40.00                                | 40.00       | 3.40 |
| **                                   |             |             |   |                         |                 |                                       |                                      |             |      |
| (4) Andrew NN-65A-M w/<br>mount pipe | A           | From Face   | 3.00  | 0.0000                  | 175.00          | No Ice                                | 12.41                                | 5.04        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 12.89                                | 5.71        | 0.17 |
|                                      |             |             | 0.00  |                         |                 | 1" Ice                                | 13.38                                | 6.37        | 0.26 |
| (4) Andrew NN-65A-M w/<br>mount pipe | B           | From Face   | 3.00  | 0.0000                  | 175.00          | No Ice                                | 12.41                                | 5.04        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 12.89                                | 5.71        | 0.17 |
|                                      |             |             | 0.00  |                         |                 | 1" Ice                                | 13.38                                | 6.37        | 0.26 |
| (4) Andrew NN-65A-M w/<br>mount pipe | C           | From Face   | 3.00  | 0.0000                  | 175.00          | No Ice                                | 12.41                                | 5.04        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 12.89                                | 5.71        | 0.17 |
|                                      |             |             | 0.00  |                         |                 | 1" Ice                                | 13.38                                | 6.37        | 0.26 |
| (12) Ericsson<br>RRUS22212-B13       | A           | From Face   | 2.00  | 0.0000                  | 175.00          | No Ice                                | 1.86                                 | 1.62        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 2.03                                 | 1.78        | 0.10 |
|                                      |             |             | 0.00  |                         |                 | 1" Ice                                | 2.20                                 | 1.95        | 0.12 |
| 12' Platform w/ Handrail             | C           | None        |   | 0.0000                  | 175.00          | No Ice                                | 30.00                                | 30.00       | 1.80 |
|                                      |             |             |   |                         |                 | 1/2" Ice                              | 35.00                                | 35.00       | 2.60 |
|                                      |             |             |   |                         |                 | 1" Ice                                | 40.00                                | 40.00       | 3.40 |
| **                                   |             |             |   |                         |                 |                                       |                                      |             |      |
| (4) Andrew NN-65A-M w/<br>mount pipe | A           | From Face   | 3.00  | 0.0000                  | 165.00          | No Ice                                | 12.41                                | 5.04        | 0.08 |
|                                      |             |             | 0.00  |                         |                 | 1/2" Ice                              | 12.89                                | 5.71        | 0.17 |

|   |  |                                  |
|---|--|----------------------------------|
| <b>tnxTower</b><br><br><b>Michael Plahovinsak, P.E.</b><br>18301 State Route 161<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>FAX: mike@mfpeng.com | <b>Job</b><br>190-ft Monopole - MFP #23520-441 | <b>Page</b><br>4 of 8            |
|   | <b>Project</b><br>Campton North                | <b>Date</b><br>17:36:30 10/30/20 |
|   | <b>Client</b><br>TP-19363                      | <b>Designed by</b><br>JC         |

| Description                       | Face or Leg | Offset Type | Offsets: Horz Lateral Vert<br>ft ft ft | Azimuth Adjustment<br>° | Placement<br>ft | C <sub>AA</sub> Frant<br>ft <sup>2</sup> | C <sub>AA</sub> Side<br>ft <sup>2</sup> | Weight<br>K |
|-----------------------------------|-------------|-------------|--|-------------------------|-----------------|--|---|-------------|
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (4) Andrew NN-65A-M w/ mount pipe | B           | From Face   | 3.00                                   | 0.0000                  | 165.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (4) Andrew NN-65A-M w/ mount pipe | C           | From Face   | 3.00                                   | 0.0000                  | 165.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (12) Ericsson RRUS22212-B13       | A           | From Face   | 2.00                                   | 0.0000                  | 165.00          | No Ice 1.86                              | 1.62                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 2.03                            | 1.78                                    | 0.10        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 2.20                              | 1.95                                    | 0.12        |
| 12' Platform w/ Handrail          | C           | None        |  | 0.0000                  | 165.00          | No Ice 30.00                             | 30.00                                   | 1.80        |
|                                   |             |             |  |                         |                 | 1/2" Ice 35.00                           | 35.00                                   | 2.60        |
|                                   |             |             |  |                         |                 | 1" Ice 40.00                             | 40.00                                   | 3.40        |
| **                                |             |             |  |                         |                 |  |   |             |
| (4) Andrew NN-65A-M w/ mount pipe | A           | From Face   | 3.00                                   | 0.0000                  | 135.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (4) Andrew NN-65A-M w/ mount pipe | B           | From Face   | 3.00                                   | 0.0000                  | 135.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (4) Andrew NN-65A-M w/ mount pipe | C           | From Face   | 3.00                                   | 0.0000                  | 135.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (12) Ericsson RRUS22212-B13       | A           | From Face   | 2.00                                   | 0.0000                  | 135.00          | No Ice 1.86                              | 1.62                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 2.03                            | 1.78                                    | 0.10        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 2.20                              | 1.95                                    | 0.12        |
| 12' Platform w/ Handrail          | C           | None        |  | 0.0000                  | 135.00          | No Ice 30.00                             | 30.00                                   | 1.80        |
|                                   |             |             |  |                         |                 | 1/2" Ice 35.00                           | 35.00                                   | 2.60        |
|                                   |             |             |  |                         |                 | 1" Ice 40.00                             | 40.00                                   | 3.40        |
| **                                |             |             |  |                         |                 |  |   |             |
| (4) Andrew NN-65A-M w/ mount pipe | A           | From Face   | 3.00                                   | 0.0000                  | 125.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (4) Andrew NN-65A-M w/ mount pipe | B           | From Face   | 3.00                                   | 0.0000                  | 125.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (4) Andrew NN-65A-M w/ mount pipe | C           | From Face   | 3.00                                   | 0.0000                  | 125.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (12) Ericsson RRUS22212-B13       | A           | From Face   | 2.00                                   | 0.0000                  | 125.00          | No Ice 1.86                              | 1.62                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 2.03                            | 1.78                                    | 0.10        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 2.20                              | 1.95                                    | 0.12        |
| 12' Platform w/ Handrail          | C           | None        |  | 0.0000                  | 125.00          | No Ice 30.00                             | 30.00                                   | 1.80        |
|                                   |             |             |  |                         |                 | 1/2" Ice 35.00                           | 35.00                                   | 2.60        |
|                                   |             |             |  |                         |                 | 1" Ice 40.00                             | 40.00                                   | 3.40        |
| **                                |             |             |  |                         |                 |  |   |             |
| (4) Andrew NN-65A-M w/ mount pipe | A           | From Face   | 3.00                                   | 0.0000                  | 105.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (4) Andrew NN-65A-M w/ mount pipe | B           | From Face   | 3.00                                   | 0.0000                  | 105.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (4) Andrew NN-65A-M w/ mount pipe | C           | From Face   | 3.00                                   | 0.0000                  | 105.00          | No Ice 12.41                             | 5.04                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 12.89                           | 5.71                                    | 0.17        |
|                                   |             |             | 0.00                                   |                         |                 | 1" Ice 13.38                             | 6.37                                    | 0.26        |
| (12) Ericsson RRUS22212-B13       | A           | From Face   | 2.00                                   | 0.0000                  | 105.00          | No Ice 1.86                              | 1.62                                    | 0.08        |
|                                   |             |             | 0.00                                   |                         |                 | 1/2" Ice 2.03                            | 1.78                                    | 0.10        |

|   |         |                                  |             |                   |
|---|---------|----------------------------------|-------------|-------------------|
| <b>tnxTower</b><br><br><b>Michael Plahovinsak, P.E.</b><br>18301 State Route 161<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>FAX: mike@mfpeng.com | Job     | 190-ft Monopole - MFP #23520-441 | Page        | 5 of 8            |
|   | Project | Campton North                    | Date        | 17:36:30 10/30/20 |
|   | Client  | TP-19363                         | Designed by | JC                |

| Description              | Face or Leg | Offset Type | Offsets: |         | Azimuth Adjustment | Placement | C <sub>A</sub> A <sub>A</sub> |                 | Weight |      |
|--------------------------|-------------|-------------|----------|---------|--------------------|-----------|-------------------------------|-----------------|--------|------|
|                          |             |             | Horz     | Lateral |                    |           | Front                         | Side            |        |      |
|                          |             |             | ft       | ft      | °                  | ft        | ft <sup>2</sup>               | ft <sup>2</sup> | K      |      |
| 12' Platform w/ Handrail | C           | None        | 0.00     |         | 0.0000             | 105.00    | 1" Ice                        | 2.20            | 1.95   | 0.12 |
|                          |             |             | No Ice   | 30.00   |                    |           | 30.00                         | 1.80            |        |      |
|                          |             |             | 1/2" Ice | 35.00   |                    |           | 35.00                         | 2.60            |        |      |
|                          |             |             | 1" Ice   | 40.00   |                    |           | 40.00                         | 3.40            |        |      |

### Dishes

| Description   | Face or Leg | Dish Type             | Offset Type | Offsets: |         | Azimuth Adjustment | 3 dB Beam Width | Elevation | Outside Diameter | Aperture Area   | Weight |      |
|---------------|-------------|-----------------------|-------------|----------|---------|--------------------|-----------------|-----------|------------------|-----------------|--------|------|
|               |             |                       |             | Horz     | Lateral |                    |                 |           |                  |                 |        |      |
|               |             |                       |             | ft       | ft      | °                  | °               | ft        | ft               | ft <sup>2</sup> | K      |      |
| 4 ft standard | A           | Paraboloid w/o Radome | From Face   | 1.00     | 0.0000  | 0.0000             |                 | 145.00    | 4.00             | No Ice          | 12.57  | 0.10 |
|               |             |                       |             | 0.00     | 0.00    |                    |                 |           |                  | 1/2" Ice        | 13.10  | 0.18 |
|               |             |                       |             | 0.00     | 0.00    |                    |                 |           |                  | 1" Ice          | 13.62  | 0.25 |
| 4 ft standard | B           | Paraboloid w/o Radome | From Face   | 1.00     | 0.0000  | 0.0000             |                 | 145.00    | 4.00             | No Ice          | 12.57  | 0.10 |
|               |             |                       |             | 0.00     | 0.00    |                    |                 |           |                  | 1/2" Ice        | 13.10  | 0.18 |
|               |             |                       |             | 0.00     | 0.00    |                    |                 |           |                  | 1" Ice          | 13.62  | 0.25 |

### Load Combinations

| Comb. No. | Description                                |
|-----------|--|
| 1         | Dead Only                                  |
| 2         | 1.2 Dead+1.6 Wind 0 deg - No Ice           |
| 3         | 0.9 Dead+1.6 Wind 0 deg - No Ice           |
| 4         | 1.2 Dead+1.6 Wind 90 deg - No Ice          |
| 5         | 0.9 Dead+1.6 Wind 90 deg - No Ice          |
| 6         | 1.2 Dead+1.6 Wind 180 deg - No Ice         |
| 7         | 0.9 Dead+1.6 Wind 180 deg - No Ice         |
| 8         | 1.2 Dead+1.0 Ice+1.0 Temp                  |
| 9         | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp   |
| 10        | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp  |
| 11        | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 12        | Dead+Wind 0 deg - Service                  |
| 13        | Dead+Wind 90 deg - Service                 |
| 14        | Dead+Wind 180 deg - Service                |

### Maximum Member Forces

| Section Na. | Elevation ft | Component Type | Condition        | Gov. Load Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
|-------------|--------------|----------------|------------------|-----------------|---------|--------------------------|--------------------------|
| L1          | 190 - 137    | Pole           | Max Tension      | 4               | 0.00    | 0.00                     | -0.01                    |
|             |              |                | Max. Compression | 8               | -46.79  | 21.83                    | 13.60                    |
|             |              |                | Max. Mx          | 4               | -15.76  | -792.23                  | -1.43                    |
|             |              |                | Max. My          | 2               | -15.89  | 15.11                    | 800.13                   |
|             |              |                | Max. Vy          | 4               | 26.71   | -792.23                  | -1.43                    |
|             |              |                | Max. Vx          | 6               | 26.46   | 4.43                     | -789.92                  |
|             |              |                | Max. Torque      | 6               |         |                          | -7.28                    |
|             |              |                | Max Tension      | 1               | 0.00    | 0.00                     | 0.00                     |
| L2          | 137 - 93.75  | Pole           | Max Tension      | 1               | 0.00    | 0.00                     | 0.00                     |
|             |              |                | Max. Compression | 8               | -97.88  | 46.27                    | 27.82                    |

|   |  |                                  |
|---|--|----------------------------------|
| <b>tnxTower</b><br><br><b>Michael Plahovinsak, P.E.</b><br>18301 State Route 161<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>FAX: mike@mfpeng.com | <b>Job</b><br>190-ft Monopole - MFP #23520-441 | <b>Page</b><br>6 of 8            |
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|   | <b>Client</b><br>TP-19363                      | <b>Designed by</b><br>JC         |

| Section No. | Elevation ft  | Component Type | Condition        | Gov. Load Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
|-------------|---------------|----------------|------------------|-----------------|---------|--------------------------|--------------------------|
| L3          | 93.75 - 46.75 | Pole           | Max. Mx          | 4               | -39.05  | -2433.53                 | -25.16                   |
|             |               |                | Max. My          | 2               | -39.18  | 36.66                    | 2423.05                  |
|             |               |                | Max. Vy          | 4               | 50.26   | -2433.53                 | -25.16                   |
|             |               |                | Max. Vx          | 6               | 49.84   | 5.83                     | -2421.31                 |
|             |               |                | Max. Torque      | 6               |         |                          | -13.98                   |
|             |               |                | Max Tension      | 1               | 0.00    | 0.00                     | 0.00                     |
|             |               |                | Max. Compression | 8               | -121.30 | 49.58                    | 29.81                    |
|             |               |                | Max. Mx          | 4               | -59.41  | -4829.15                 | -60.56                   |
|             |               |                | Max. My          | 6               | -59.45  | -7.05                    | -4797.69                 |
|             |               |                | Max. Vy          | 4               | 54.17   | -4829.15                 | -60.56                   |
| L4          | 46.75 - 1     | Pole           | Max. Vx          | 6               | 53.75   | -7.05                    | -4797.69                 |
|             |               |                | Max. Torque      | 6               |         |                          | -13.96                   |
|             |               |                | Max Tension      | 1               | 0.00    | 0.00                     | 0.00                     |
|             |               |                | Max. Compression | 8               | -154.67 | 50.77                    | 30.53                    |
|             |               |                | Max. Mx          | 4               | -89.13  | -7781.69                 | -100.65                  |
|             |               |                | Max. My          | 6               | -89.13  | -22.28                   | -7728.46                 |
|             |               |                | Max. Vy          | 4               | 56.62   | -7781.69                 | -100.65                  |
|             |               |                | Max. Vx          | 6               | 56.22   | -22.28                   | -7728.46                 |
|             |               |                | Max. Torque      | 6               |         |                          | -13.88                   |

### Maximum Tower Deflections - Service Wind

| Section No. | Elevation ft  | Horz. Deflection in | Gov. Load Comb. | Tilt ° | Twist ° |
|-------------|---------------|---------------------|-----------------|--------|---------|
| L1          | 190 - 137     | 49.800              | 12              | 2.2953 | 0.0190  |
| L2          | 142 - 93.75   | 27.906              | 12              | 1.8991 | 0.0104  |
| L3          | 99.75 - 46.75 | 13.463              | 12              | 1.2969 | 0.0051  |
| L4          | 54 - 1        | 3.866               | 12              | 0.6646 | 0.0019  |

### Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance                      | Gov. Load Comb. | Deflection in | Tilt ° | Twist ° | Radius of Curvature ft |
|--------------|-----------------------------------|-----------------|---------------|--------|---------|------------------------|
| 185.00       | (4) Andrew NN-65A-M w/ mount pipe | 12              | 47.395        | 2.2625 | 0.0180  | 36846                  |
| 175.00       | (4) Andrew NN-65A-M w/ mount pipe | 12              | 42.619        | 2.1946 | 0.0162  | 12281                  |
| 165.00       | (4) Andrew NN-65A-M w/ mount pipe | 12              | 37.940        | 2.1201 | 0.0143  | 7368                   |
| 145.00       | 4 ft standard                     | 12              | 29.137        | 1.9332 | 0.0109  | 4097                   |
| 135.00       | (4) Andrew NN-65A-M w/ mount pipe | 12              | 25.140        | 1.8126 | 0.0094  | 3895                   |
| 125.00       | (4) Andrew NN-65A-M w/ mount pipe | 12              | 21.451        | 1.6753 | 0.0080  | 3984                   |
| 105.00       | (4) Andrew NN-65A-M w/ mount pipe | 12              | 14.971        | 1.3759 | 0.0056  | 4174                   |

|   |  |                                  |
|---|--|----------------------------------|
| <b>tnxTower</b><br><br><b>Michael Plahovinsak, P.E.</b><br>18301 State Route 161<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>FAX: mike@mfpeng.com | <b>Job</b><br>190-ft Monopole - MFP #23520-441 | <b>Page</b><br>7 of 8            |
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|   | <b>Client</b><br>TP-19363                      | <b>Designed by</b><br>JC         |

### Maximum Tower Deflections - Design Wind

| Section No. | Elevation<br>ft | Horz.<br>Deflection<br>in | Gov.<br>Load<br>Comb. | Tilt<br>° | Twist<br>° |
|-------------|-----------------|---------------------------|-----------------------|-----------|------------|
| L1          | 190 - 137       | 201.351                   | 4                     | 9.1963    | 0.0759     |
| L2          | 142 - 93.75     | 113.548                   | 4                     | 7.6971    | 0.0416     |
| L3          | 99.75 - 46.75   | 54.979                    | 4                     | 5.2886    | 0.0203     |
| L4          | 54 - 1          | 15.819                    | 4                     | 2.7187    | 0.0078     |

### Critical Deflections and Radius of Curvature - Design Wind

| Elevation<br>ft | Appurtenance                      | Gov.<br>Load<br>Comb. | Deflection<br>in | Tilt<br>° | Twist<br>° | Radius of<br>Curvature<br>ft |
|-----------------|-----------------------------------|-----------------------|------------------|-----------|------------|------------------------------|
| 185.00          | (4) Andrew NN-65A-M w/ mount pipe | 4                     | 191.728          | 9.0761    | 0.0721     | 9748                         |
| 175.00          | (4) Andrew NN-65A-M w/ mount pipe | 4                     | 172.609          | 8.8262    | 0.0645     | 3246                         |
| 165.00          | (4) Andrew NN-65A-M w/ mount pipe | 4                     | 153.866          | 8.5479    | 0.0572     | 1944                         |
| 145.00          | 4 ft standard                     | 4                     | 118.511          | 7.8304    | 0.0435     | 1074                         |
| 135.00          | (4) Andrew NN-65A-M w/ mount pipe | 4                     | 102.386          | 7.3560    | 0.0373     | 1014                         |
| 125.00          | (4) Andrew NN-65A-M w/ mount pipe | 4                     | 87.454           | 6.8096    | 0.0318     | 1028                         |
| 105.00          | (4) Andrew NN-65A-M w/ mount pipe | 4                     | 61.121           | 5.6075    | 0.0224     | 1055                         |

### Pole Design Data

| Section No. | Elevation<br>ft      | Size                     | L<br>ft | L <sub>u</sub><br>ft | KI/r | A<br>in <sup>2</sup> | P <sub>u</sub><br>K | φP <sub>n</sub><br>K | Ratio<br>$\frac{P_u}{\phi P_n}$ |
|-------------|----------------------|--------------------------|---------|----------------------|------|----------------------|---------------------|----------------------|---------------------------------|
| L1          | 190 - 137 (1)        | TP36.0602x26x0.1875      | 53.00   | 0.00                 | 0.0  | 20.7839              | -15.89              | 1210.38              | 0.013                           |
| L2          | 137 - 93.75 (2)      | TP43.8947x34.7361x0.3125 | 48.25   | 0.00                 | 0.0  | 42.0984              | -39.05              | 2847.26              | 0.014                           |
| L3          | 93.75 - 46.75<br>(3) | TP52.191x42.1308x0.4375  | 53.00   | 0.00                 | 0.0  | 69.9552              | -59.41              | 5000.71              | 0.012                           |
| L4          | 46.75 - 1 (4)        | TP60x49.9398x0.5         | 53.00   | 0.00                 | 0.0  | 94.4265              | -89.13              | 6682.26              | 0.013                           |

### Pole Bending Design Data

| Section No. | Elevation<br>ft      | Size                     | M <sub>ux</sub><br>kip-ft | φM <sub>ux</sub><br>kip-ft | Ratio<br>$\frac{M_{ux}}{\phi M_{ux}}$ | M <sub>uy</sub><br>kip-ft | φM <sub>uy</sub><br>kip-ft | Ratio<br>$\frac{M_{uy}}{\phi M_{uy}}$ |
|-------------|----------------------|--------------------------|---------------------------|----------------------------|---------------------------------------|---------------------------|----------------------------|---------------------------------------|
| L1          | 190 - 137 (1)        | TP36.0602x26x0.1875      | 800.27                    | 871.38                     | 0.918                                 | 0.00                      | 871.38                     | 0.000                                 |
| L2          | 137 - 93.75 (2)      | TP43.8947x34.7361x0.3125 | 2433.67                   | 2486.24                    | 0.979                                 | 0.00                      | 2486.24                    | 0.000                                 |
| L3          | 93.75 - 46.75<br>(3) | TP52.191x42.1308x0.4375  | 4829.53                   | 5176.11                    | 0.933                                 | 0.00                      | 5176.11                    | 0.000                                 |
| L4          | 46.75 - 1 (4)        | TP60x49.9398x0.5         | 7782.34                   | 8171.44                    | 0.952                                 | 0.00                      | 8171.44                    | 0.000                                 |

|   |  |                                  |
|---|--|----------------------------------|
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|   | <b>Client</b><br>TP-19363                      | <b>Designed by</b><br>JC         |

### Pole Shear Design Data

| Section No. | Elevation ft      | Size                     | Actual $V_u$ K | $\phi V_n$ K | Ratio $V_u / \phi V_n$ | Actual $T_u$ kip-ft | $\phi T_n$ kip-ft | Ratio $T_u / \phi T_n$ |
|-------------|-------------------|--------------------------|----------------|--------------|------------------------|---------------------|-------------------|------------------------|
| L1          | 190 - 137 (1)     | TP36.0602x26x0.1875      | 25.97          | 605.19       | 0.043                  | 7.24                | 1746.31           | 0.004                  |
| L2          | 137 - 93.75 (2)   | TP43.8947x34.7361x0.3125 | 50.27          | 1423.63      | 0.035                  | 8.72                | 4984.10           | 0.002                  |
| L3          | 93.75 - 46.75 (3) | TP52.191x42.1308x0.4375  | 54.18          | 2500.35      | 0.022                  | 8.67                | 10378.42          | 0.001                  |
| L4          | 46.75 - 1 (4)     | TP60x49.9398x0.5         | 56.63          | 3341.13      | 0.017                  | 8.64                | 16383.58          | 0.001                  |

### Pole Interaction Design Data

| Section No. | Elevation ft      | Ratio $P_u$ | Ratio $M_{ux}$ | Ratio $M_{uy}$ | Ratio $V_u$ | Ratio $T_u$ | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
|-------------|-------------------|-------------|----------------|----------------|-------------|-------------|--------------------|---------------------|----------|
| L1          | 190 - 137 (1)     | 0.013       | 0.918          | 0.000          | 0.043       | 0.004       | 0.934              | 1.000               | 4.8.2 ✓  |
| L2          | 137 - 93.75 (2)   | 0.014       | 0.979          | 0.000          | 0.035       | 0.002       | 0.994              | 1.000               | 4.8.2 ✓  |
| L3          | 93.75 - 46.75 (3) | 0.012       | 0.933          | 0.000          | 0.022       | 0.001       | 0.945              | 1.000               | 4.8.2 ✓  |
| L4          | 46.75 - 1 (4)     | 0.013       | 0.952          | 0.000          | 0.017       | 0.001       | 0.966              | 1.000               | 4.8.2 ✓  |

### Section Capacity Table

| Section No. | Elevation ft  | Component Type | Size                     | Critical Element | P K    | $\phi P_{allow}$ K | % Capacity | Pass Fail |
|-------------|---------------|----------------|--------------------------|------------------|--------|--------------------|------------|-----------|
| L1          | 190 - 137     | Pole           | TP36.0602x26x0.1875      | 1                | -15.89 | 1210.38            | 93.4       | Pass      |
| L2          | 137 - 93.75   | Pole           | TP43.8947x34.7361x0.3125 | 2                | -39.05 | 2847.26            | 99.4       | Pass      |
| L3          | 93.75 - 46.75 | Pole           | TP52.191x42.1308x0.4375  | 3                | -59.41 | 5000.71            | 94.5       | Pass      |
| L4          | 46.75 - 1     | Pole           | TP60x49.9398x0.5         | 4                | -89.13 | 6682.26            | 96.6       | Pass      |
| Summary     |               |                |                          |                  |        |                    |            |           |
| Pole (L2)   |               |                |                          |                  |        |                    | 99.4       | Pass      |
| RATING =    |               |                |                          |                  |        |                    | 99.4       | Pass      |

|   |  |                             |
|---|--|-----------------------------|
| <b>Michael F. Plahovinsak, P.E.</b><br>18301 State Route 161 W<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>email: mike@mfpeng.com | <b>Job</b><br>190-ft monopole - MFP #23520-441 | <b>Page</b><br>BP & AB Calc |
|   | <b>Project</b><br>Campton North                | <b>Date</b><br>10/30/2020   |
|   | <b>Client</b><br>TAPP TP-19363                 | <b>Designed by</b><br>Mike  |

## Anchor Rod and Base Plate Calculation

**ANSI/TIA-222-G**

| <i>Factored Base Reactions:</i> | <i>Pole Shape:</i>                | <i>Anchor Rods:</i>       | <i>Base Plate:</i>       |
|---------------------------------|-----------------------------------|---------------------------|--------------------------|
| Moment: 7782 ft-kips            | 18-Sided                          | (24) 2.25 in. A615 GR. 75 | 2.5 in. x 73.5 in. Round |
| Shear: 57 kips                  | <i>Pole Dia. (D<sub>p</sub>):</i> | Anchor Rods Evenly Spaced | f <sub>y</sub> = 50 ksi  |
| Axial: 89 kips                  | 60.00 in                          | On a 67.5 in Bolt Circle  |                          |

**Anchor Rod Calculation According to TIA-222-G section 4.9.9**

$\phi_t, \phi_v = 0.80$  TIA 4.9.9  
 $I_{bolts} = 13668.75 \text{ in}^2$  Moment of Inertia  
 $P_u = 234 \text{ kips}$  Compr Force  
 $V_u = 2.4 \text{ kips}$  Shear Force  
 $R_{nt} = 325.00 \text{ kips}$  Nominal Tensile Strength  
 $n = 0.50$  for detail type (d)  
**Stress Rating = 91.9%** Satisfies TIA-G 4.9.9

**Base Plate Calculation According to TIA-222-G**

$\phi = 0.90$  TIA 4.7  
 $M_{PL} = 538.5 \text{ in-kip}$  Plate Moment  
 $L = 7.9 \text{ in}$  Section Length  
 $Z = 12.3$  Plastic Section Modulus  
 $M_p = 613.6 \text{ in-kip}$  Plastic Moment  
 $\phi M_n = 552.2 \text{ in-kip}$  Factored Resistance

*Calculated Moment vs Factored Resistance*

$538.47 \text{ in-kip} \leq 552 \text{ in-kip}$

**Stress Rating = 97.5%**

|                                 |  |
|---------------------------------|--|
| <b>Anchor Rods Are Adequate</b> | <b>91.9%</b> <input checked="" type="checkbox"/> |
| <b>Base Plate is Adequate</b>   | <b>97.5%</b> <input checked="" type="checkbox"/> |

|   |         |                                  |             |            |
|---|---------|----------------------------------|-------------|------------|
| <b>Michael F. Plahovinsak, P.E.</b><br>18301 State Route 161 W<br>Plain City, OH 43064<br>Phone: 614-398-6250<br>email: mike@mfpeng.com | Job     | 190-ft monopole - MFP #23520-441 | Page        | FND        |
|   | Project | Campton North                    | Date        | 10/30/2020 |
|   | Client  | TAPP TP-19363                    | Designed by | Mike       |
|   |         |                                  |             |            |

## Caisson Calculation

According to ANSITIA-222-G

1. Foundation overturning resistance calculated with PLS Caisson, for Brom's method for rigid piles. Soil layers modeled after recommendations from the geotechnical report.
2. Cohesion strength for the upper 22.5 ft has been reduced by 50%
3. In lieu of a soil resistance factor  $f_s = 0.75$  (TIA-9.4.1) an additional safety factor against soil failure of 1.33 has been applied.
4. Foundation has been designed with factored loads per TIA-222-G.
5. No groundwater within the depth of the foundation.

| *** PIER PROPERTIES  | CONCRETE STRENGTH (ksi) = 4.00   | STEEL STRENGTH (ksi) = 60.00                          |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
|--|--|---|----------------------------------|---------------|----------------|----------------------------|---------------------------------|-----------------------------------|-------------------------------------|----------------------------------|---------------|-----------|---------------|-----------|---------------|------|-------|---------|-------|--------|-------|-------|---------|------|--------|-------|-------|---------|-------|--------|-------|------|---------|-------|--------|-------|--------|---------|--------|--------|-------|--------|---------|--------|--------|---------|--------|--------|--------|--------|-------|---------|--------|---------|--------|-------|---------|--------|--------|--------|-------|---------|-------|--------|-------|-------|-----|------|-----|------|
|  | DIAMETER (ft) = 7.500  | DISTANCE FROM TOP OF PIER TO GROUND LEVEL (ft) = 0.50 |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| *** SOIL PROPERTIES  | <table border="0" style="width: 100%;"> <thead> <tr> <th>LAYER</th> <th>TYPE</th> <th>THICKNESS (ft)</th> <th>DEPTH AT TOP OF LAYER (ft)</th> <th>DENSITY (pcf)</th> <th>CU (pcf)</th> <th>KP (psf)</th> <th>PHI (degrees)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>S</td> <td>7.00</td> <td>0.00</td> <td>100.0</td> <td></td> <td>1.000</td> <td>-0.00</td> </tr> <tr> <td>2</td> <td>S</td> <td>5.00</td> <td>7.00</td> <td>150.0</td> <td></td> <td>2.371</td> <td>24.00</td> </tr> <tr> <td>3</td> <td>S</td> <td>10.00</td> <td>12.00</td> <td>165.0</td> <td></td> <td>3.000</td> <td>30.00</td> </tr> <tr> <td>4</td> <td>S</td> <td>3.50</td> <td>22.00</td> <td>150.0</td> <td></td> <td>2.663</td> <td>27.00</td> </tr> <tr> <td>5</td> <td>S</td> <td>1.50</td> <td>25.50</td> <td>165.0</td> <td></td> <td>3.000</td> <td>30.00</td> </tr> </tbody> </table>   |   | LAYER                            | TYPE          | THICKNESS (ft) | DEPTH AT TOP OF LAYER (ft) | DENSITY (pcf)                   | CU (pcf)                          | KP (psf)                            | PHI (degrees)                    | 1             | S         | 7.00          | 0.00      | 100.0         |      | 1.000 | -0.00   | 2     | S      | 5.00  | 7.00  | 150.0   |      | 2.371  | 24.00 | 3     | S       | 10.00 | 12.00  | 165.0 |      | 3.000   | 30.00 | 4      | S     | 3.50   | 22.00   | 150.0  |        | 2.663 | 27.00  | 5       | S      | 1.50   | 25.50   | 165.0  |        | 3.000  | 30.00  |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| LAYER  | TYPE   | THICKNESS (ft)  | DEPTH AT TOP OF LAYER (ft)       | DENSITY (pcf) | CU (pcf)       | KP (psf)                   | PHI (degrees)                   |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 1  | S  | 7.00  | 0.00                             | 100.0         |                | 1.000                      | -0.00                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 2  | S  | 5.00  | 7.00                             | 150.0         |                | 2.371                      | 24.00                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 3  | S  | 10.00   | 12.00                            | 165.0         |                | 3.000                      | 30.00                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 4  | S  | 3.50  | 22.00                            | 150.0         |                | 2.663                      | 27.00                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 5  | S  | 1.50  | 25.50                            | 165.0         |                | 3.000                      | 30.00                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| *** DESIGN (FACTORED) LOADS AT TOP OF PIER                             | MOMENT (ft-k) = 7782.0   | VERTICAL (k) = 89.0                                   |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
|  | ADDITIONAL SAFETY FACTOR AGAINST SOIL FAILURE = 1.33   |   |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| *** CALCULATED PIER LENGTH (ft) = 27.000                               |  |   |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| *** CHECK OF SOILS PROPERTIES AND ULTIMATE RESISTING FORCES ALONG PIER |  |   |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
|  | <table border="0" style="width: 100%;"> <thead> <tr> <th>TYPE</th> <th>TOP OF LAYER BELOW TOP OF PIER (ft)</th> <th>THICKNESS (ft)</th> <th>DENSITY (pcf)</th> <th>CU (pcf)</th> <th>KP (psf)</th> <th>FORCE (k)</th> <th>ARM (ft)</th> </tr> </thead> <tbody> <tr> <td>S</td> <td>0.50</td> <td>7.00</td> <td>100.0</td> <td></td> <td>1.000</td> <td>55.13</td> <td>5.17</td> </tr> <tr> <td>S</td> <td>7.50</td> <td>5.00</td> <td>150.0</td> <td></td> <td>2.371</td> <td>286.74</td> <td>10.29</td> </tr> <tr> <td>S</td> <td>12.50</td> <td>7.86</td> <td>165.0</td> <td></td> <td>3.000</td> <td>1112.98</td> <td>16.83</td> </tr> <tr> <td>S</td> <td>20.36</td> <td>2.14</td> <td>165.0</td> <td></td> <td>3.000</td> <td>-422.64</td> <td>21.45</td> </tr> <tr> <td>S</td> <td>22.50</td> <td>3.50</td> <td>150.0</td> <td></td> <td>2.663</td> <td>-705.15</td> <td>24.30</td> </tr> <tr> <td>S</td> <td>26.00</td> <td>1.00</td> <td>165.0</td> <td></td> <td>3.000</td> <td>-250.26</td> <td>26.50</td> </tr> </tbody> </table>   |   |                                  |               |                |                            |                                 | TYPE                              | TOP OF LAYER BELOW TOP OF PIER (ft) | THICKNESS (ft)                   | DENSITY (pcf) | CU (pcf)  | KP (psf)      | FORCE (k) | ARM (ft)      | S    | 0.50  | 7.00    | 100.0 |        | 1.000 | 55.13 | 5.17    | S    | 7.50   | 5.00  | 150.0 |         | 2.371 | 286.74 | 10.29 | S    | 12.50   | 7.86  | 165.0  |       | 3.000  | 1112.98 | 16.83  | S      | 20.36 | 2.14   | 165.0   |        | 3.000  | -422.64 | 21.45  | S      | 22.50  | 3.50   | 150.0 |         | 2.663  | -705.15 | 24.30  | S     | 26.00   | 1.00   | 165.0  |        | 3.000 | -250.26 | 26.50 |        |       |       |     |      |     |      |
| TYPE   | TOP OF LAYER BELOW TOP OF PIER (ft)  | THICKNESS (ft)  | DENSITY (pcf)                    | CU (pcf)      | KP (psf)       | FORCE (k)                  | ARM (ft)                        |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| S  | 0.50   | 7.00  | 100.0                            |               | 1.000          | 55.13                      | 5.17                            |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| S  | 7.50   | 5.00  | 150.0                            |               | 2.371          | 286.74                     | 10.29                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| S  | 12.50  | 7.86  | 165.0                            |               | 3.000          | 1112.98                    | 16.83                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| S  | 20.36  | 2.14  | 165.0                            |               | 3.000          | -422.64                    | 21.45                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| S  | 22.50  | 3.50  | 150.0                            |               | 2.663          | -705.15                    | 24.30                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| S  | 26.00  | 1.00  | 165.0                            |               | 3.000          | -250.26                    | 26.50                           |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| *** SHEAR AND MOMENTS ALONG PIER                                       |  |   |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
|  | <table border="0" style="width: 100%;"> <thead> <tr> <th rowspan="2">DISTANCE BELOW TOP OF PIER (ft)</th> <th colspan="2">WITH THE ADDITIONAL SAFETY FACTOR</th> <th colspan="2">WITHOUT ADDITIONAL SAFETY FACTOR</th> </tr> <tr> <th>SHEAR (k)</th> <th>MOMENT (ft-k)</th> <th>SHEAR (k)</th> <th>MOMENT (ft-k)</th> </tr> </thead> <tbody> <tr> <td>0.00</td> <td>76.8</td> <td>10859.6</td> <td>57.6</td> <td>8144.9</td> </tr> <tr> <td>2.70</td> <td>71.4</td> <td>11063.0</td> <td>53.5</td> <td>8297.4</td> </tr> <tr> <td>5.40</td> <td>49.8</td> <td>11230.2</td> <td>37.3</td> <td>8422.8</td> </tr> <tr> <td>8.10</td> <td>-2.2</td> <td>11312.9</td> <td>-1.6</td> <td>8484.9</td> </tr> <tr> <td>10.80</td> <td>-145.1</td> <td>11127.2</td> <td>-108.9</td> <td>8345.6</td> </tr> <tr> <td>13.50</td> <td>-368.5</td> <td>10465.9</td> <td>-276.4</td> <td>7849.6</td> </tr> <tr> <td>16.20</td> <td>-703.4</td> <td>9037.0</td> <td>-527.6</td> <td>6778.0</td> </tr> <tr> <td>18.90</td> <td>-1119.6</td> <td>6594.2</td> <td>-839.7</td> <td>4945.8</td> </tr> <tr> <td>21.60</td> <td>-1139.2</td> <td>3211.3</td> <td>-854.4</td> <td>2408.6</td> </tr> <tr> <td>24.30</td> <td>-606.5</td> <td>858.0</td> <td>-454.9</td> <td>643.5</td> </tr> <tr> <td>27.00</td> <td>0.0</td> <td>-0.0</td> <td>0.0</td> <td>-0.0</td> </tr> </tbody> </table> |   |                                  |               |                |                            | DISTANCE BELOW TOP OF PIER (ft) | WITH THE ADDITIONAL SAFETY FACTOR |                                     | WITHOUT ADDITIONAL SAFETY FACTOR |               | SHEAR (k) | MOMENT (ft-k) | SHEAR (k) | MOMENT (ft-k) | 0.00 | 76.8  | 10859.6 | 57.6  | 8144.9 | 2.70  | 71.4  | 11063.0 | 53.5 | 8297.4 | 5.40  | 49.8  | 11230.2 | 37.3  | 8422.8 | 8.10  | -2.2 | 11312.9 | -1.6  | 8484.9 | 10.80 | -145.1 | 11127.2 | -108.9 | 8345.6 | 13.50 | -368.5 | 10465.9 | -276.4 | 7849.6 | 16.20   | -703.4 | 9037.0 | -527.6 | 6778.0 | 18.90 | -1119.6 | 6594.2 | -839.7  | 4945.8 | 21.60 | -1139.2 | 3211.3 | -854.4 | 2408.6 | 24.30 | -606.5  | 858.0 | -454.9 | 643.5 | 27.00 | 0.0 | -0.0 | 0.0 | -0.0 |
| DISTANCE BELOW TOP OF PIER (ft)  | WITH THE ADDITIONAL SAFETY FACTOR  |   | WITHOUT ADDITIONAL SAFETY FACTOR |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
|  | SHEAR (k)  | MOMENT (ft-k)   | SHEAR (k)                        | MOMENT (ft-k) |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 0.00   | 76.8   | 10859.6   | 57.6                             | 8144.9        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 2.70   | 71.4   | 11063.0   | 53.5                             | 8297.4        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 5.40   | 49.8   | 11230.2   | 37.3                             | 8422.8        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 8.10   | -2.2   | 11312.9   | -1.6                             | 8484.9        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 10.80  | -145.1   | 11127.2   | -108.9                           | 8345.6        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 13.50  | -368.5   | 10465.9   | -276.4                           | 7849.6        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 16.20  | -703.4   | 9037.0  | -527.6                           | 6778.0        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 18.90  | -1119.6  | 6594.2  | -839.7                           | 4945.8        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 21.60  | -1139.2  | 3211.3  | -854.4                           | 2408.6        |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 24.30  | -606.5   | 858.0   | -454.9                           | 643.5         |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| 27.00  | 0.0  | -0.0  | 0.0                              | -0.0          |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| *** TOTAL REINFORCEMENT PCT = 0.84                                     | REINFORCEMENT AREA (in <sup>2</sup> ) = 53.44  |   |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |
| *** USABLE AXIAL CAP. (k) = 89.0                                       | USABLE MOMENT CAP. (ft-k) = 8579.8   |   |                                  |               |                |                            |                                 |                                   |                                     |                                  |               |           |               |           |               |      |       |         |       |        |       |       |         |      |        |       |       |         |       |        |       |      |         |       |        |       |        |         |        |        |       |        |         |        |        |         |        |        |        |        |       |         |        |         |        |       |         |        |        |        |       |         |       |        |       |       |     |      |     |      |

**For Design:**

7.5-ft Diameter caisson x 27-ft long (26.5-ft Embedded with 0.5-ft above grade)  
 Concrete strength = 4000 PSI @ 28 days. Estimated Concrete Volume = 44 CY3.  
 (44) #10 Vertical Rebar. Steel Cross-Section = 55.88 in<sup>2</sup>

# Exhibit 6



Mail Processing Center  
 Federal Aviation Administration  
 Southwest Regional Office  
 Obstruction Evaluation Group  
 10101 Hillwood Parkway  
 Fort Worth, TX 76177

Aeronautical Study No.  
 2020-ASO-25415-OE

Issued Date: 09/17/2020

Cindy D. McCarty  
 East Kentucky Network, LLC  
 101 Technology Trail  
 Ivel, KY 41642

**\*\* DETERMINATION OF NO HAZARD TO AIR NAVIGATION \*\***

The Federal Aviation Administration has conducted an aeronautical study under the provisions of 49 U.S.C., Section 44718 and if applicable Title 14 of the Code of Federal Regulations, part 77, concerning:

Structure: Antenna Tower Campton  
 Location: Campton, KY  
 Latitude: 37-45-50.32N NAD 83  
 Longitude: 83-31-34.68W  
 Heights: 1216 feet site elevation (SE)  
 199 feet above ground level (AGL)  
 1415 feet above mean sea level (AMSL)

This aeronautical study revealed that the structure does not exceed obstruction standards and would not be a hazard to air navigation provided the following condition(s), if any, is(are) met:

It is required that FAA Form 7460-2, Notice of Actual Construction or Alteration, be e-filed any time the project is abandoned or:

- At least 10 days prior to start of construction (7460-2, Part 1)
- Within 5 days after the construction reaches its greatest height (7460-2, Part 2)

Based on this evaluation, marking and lighting are not necessary for aviation safety. However, if marking/lighting are accomplished on a voluntary basis, we recommend it be installed in accordance with FAA Advisory circular 70/7460-1 L Change 2.

This determination expires on 03/17/2022 unless:

- (a) the construction is started (not necessarily completed) and FAA Form 7460-2, Notice of Actual Construction or Alteration, is received by this office.
- (b) extended, revised, or terminated by the issuing office.
- (c) the construction is subject to the licensing authority of the Federal Communications Commission (FCC) and an application for a construction permit has been filed, as required by the FCC, within 6 months of the date of this determination. In such case, the determination expires on the date prescribed by the FCC for completion of construction, or the date the FCC denies the application.

NOTE: REQUEST FOR EXTENSION OF THE EFFECTIVE PERIOD OF THIS DETERMINATION MUST BE E-FILED AT LEAST 15 DAYS PRIOR TO THE EXPIRATION DATE. AFTER RE-EVALUATION OF CURRENT OPERATIONS IN THE AREA OF THE STRUCTURE TO DETERMINE THAT NO SIGNIFICANT AERONAUTICAL CHANGES HAVE OCCURRED, YOUR DETERMINATION MAY BE ELIGIBLE FOR ONE EXTENSION OF THE EFFECTIVE PERIOD.

This determination is based, in part, on the foregoing description which includes specific coordinates, heights, frequency(ies) and power. Any changes in coordinates, heights, and frequencies or use of greater power, except those frequencies specified in the Colo Void Clause Coalition; Antenna System Co-Location; Voluntary Best Practices, effective 21 Nov 2007, will void this determination. Any future construction or alteration, including increase to heights, power, or the addition of other transmitters, requires separate notice to the FAA. This determination includes all previously filed frequencies and power for this structure.

If construction or alteration is dismantled or destroyed, you must submit notice to the FAA within 5 days after the construction or alteration is dismantled or destroyed.

This determination does include temporary construction equipment such as cranes, derricks, etc., which may be used during actual construction of the structure. However, this equipment shall not exceed the overall heights as indicated above. Equipment which has a height greater than the studied structure requires separate notice to the FAA.

This determination concerns the effect of this structure on the safe and efficient use of navigable airspace by aircraft and does not relieve the sponsor of compliance responsibilities relating to any law, ordinance, or regulation of any Federal, State, or local government body.

A copy of this determination will be forwarded to the Federal Communications Commission (FCC) because the structure is subject to their licensing authority.

If we can be of further assistance, please contact our office at (718) 553-2611, or [angelique.eersteling@faa.gov](mailto:angelique.eersteling@faa.gov). On any future correspondence concerning this matter, please refer to Aeronautical Study Number 2020-ASO-25415-OE.

**Signature Control No: 449110220-451188875**  
Angelique Eersteling  
Technician

( DNE )

Attachment(s)  
Case Description  
Frequency Data  
Map(s)

cc: FCC

**Case Description for ASN 2020-ASO-25415-OE**

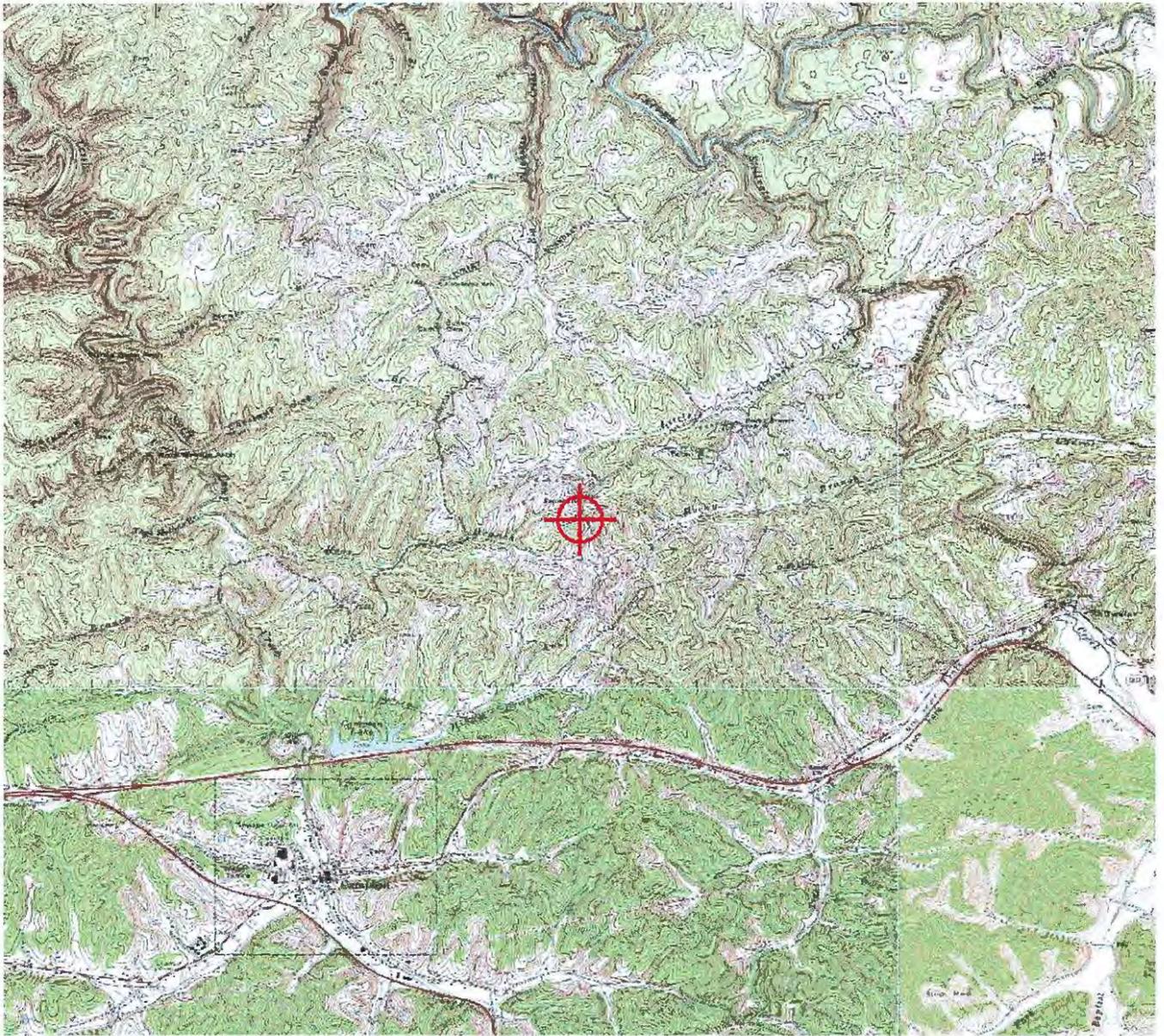
A new 190' structure with top-mounted antennas or other appurtenances (overall height of 199' AGL).

Frequency Data for ASN 2020-ASO-25415-OE

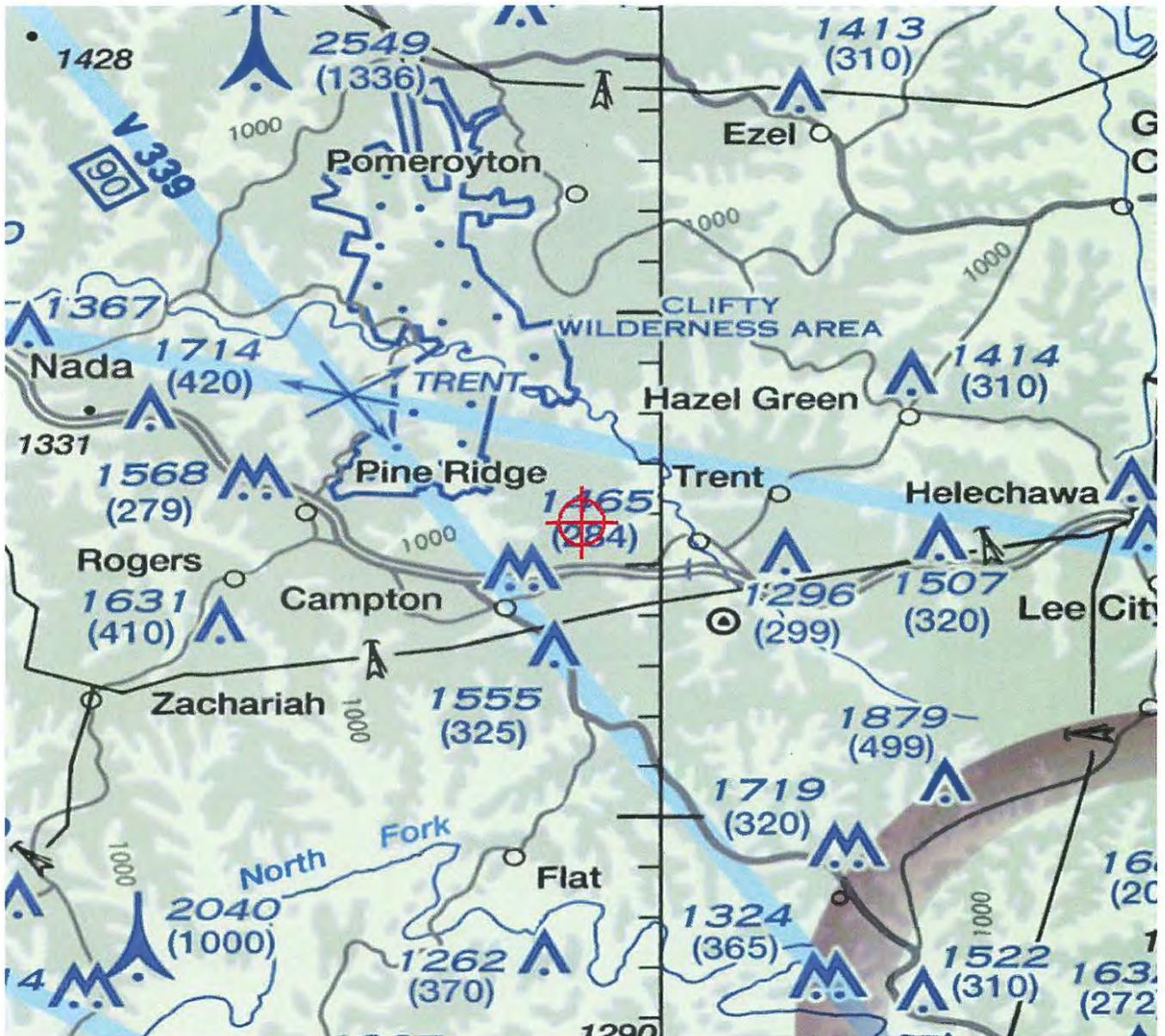
| LOW<br>FREQUENCY | HIGH<br>FREQUENCY | FREQUENCY<br>UNIT | ERP  | ERP<br>UNIT |
|------------------|-------------------|-------------------|------|-------------|
| 6                | 7                 | GHz               | 55   | dBW         |
| 6                | 7                 | GHz               | 42   | dBW         |
| 10               | 11.7              | GHz               | 55   | dBW         |
| 10               | 11.7              | GHz               | 42   | dBW         |
| 17.7             | 19.7              | GHz               | 55   | dBW         |
| 17.7             | 19.7              | GHz               | 42   | dBW         |
| 21.2             | 23.6              | GHz               | 55   | dBW         |
| 21.2             | 23.6              | GHz               | 42   | dBW         |
| 614              | 698               | MHz               | 1000 | W           |
| 614              | 698               | MHz               | 2000 | W           |
| 698              | 806               | MHz               | 1000 | W           |
| 806              | 901               | MHz               | 500  | W           |
| 806              | 824               | MHz               | 500  | W           |
| 824              | 849               | MHz               | 500  | W           |
| 851              | 866               | MHz               | 500  | W           |
| 869              | 894               | MHz               | 500  | W           |
| 896              | 901               | MHz               | 500  | W           |
| 901              | 902               | MHz               | 7    | W           |
| 929              | 932               | MHz               | 3500 | W           |
| 930              | 931               | MHz               | 3500 | W           |
| 931              | 932               | MHz               | 3500 | W           |
| 932              | 932.5             | MHz               | 17   | dBW         |
| 935              | 940               | MHz               | 1000 | W           |
| 940              | 941               | MHz               | 3500 | W           |
| 1670             | 1675              | MHz               | 500  | W           |
| 1710             | 1755              | MHz               | 500  | W           |
| 1850             | 1910              | MHz               | 1640 | W           |
| 1850             | 1990              | MHz               | 1640 | W           |
| 1930             | 1990              | MHz               | 1640 | W           |
| 1990             | 2025              | MHz               | 500  | W           |
| 2110             | 2200              | MHz               | 500  | W           |
| 2305             | 2360              | MHz               | 2000 | W           |
| 2305             | 2310              | MHz               | 2000 | W           |
| 2345             | 2360              | MHz               | 2000 | W           |
| 2496             | 2690              | MHz               | 500  | W           |



TOPO Map for ASN 2020-ASO-25415-OE



Sectional Map for ASN 2020-ASO-25415-OE





**KENTUCKY AIRPORT ZONING COMMISSION**

ANDY BESHEAR  
Governor

Office of Audits, 200 Mero Street, 4th floor  
Frankfort, KY 40622  
[www.transportation.ky.gov](http://www.transportation.ky.gov)  
502-782-4043

JIM GRAY  
Secretary

**APPROVAL OF APPLICATION**

October 15, 2020

**APPLICANT**

East Kentucky Network, LLC  
Cindy McCarty  
101 Technology Trail  
Ivel, KY 41642

**SUBJECT:** AS-WOLFE-JKL-2020-116

**STRUCTURE:** Antenna Tower  
**LOCATION:** Campton, KY  
**COORDINATES:** 37° 45' 50.32" N / 83° 31' 34.68" W  
**HEIGHT:** 199' AGL/1415' AMSL

The Kentucky Airport Zoning Commission has approved your application for a permit to construct 199' AGL/1415' AMSL Antenna Tower near Campton, KY 37° 45' 50.32" N / 83° 31' 34.68" W.

This permit is valid for a period of 18 Month(s) from its date of issuance. If construction is not completed within said 18-Month period, this permit shall lapse and be void, and no work shall be performed without the issuance of a new permit.

No Marking/Lighting Required.

***Randall S. Royer***

Randall S. Royer, Executive Director  
Office of Audits  
Acting Administrator  
[Randall.Royer@ky.gov](mailto:Randall.Royer@ky.gov)  
[Jason.Salazar-Munoz@ky.gov](mailto:Jason.Salazar-Munoz@ky.gov)



An Equal Opportunity Employer M/F/D

# Exhibit 7

## Driving Directions for Campton

1. Beginning at North Washington Street at the Wolfe County Courthouse in Campton, Kentucky travel to the traffic light at the intersection of Washington Street and KY Route 191.
2. Travel one mile and two tenths. Turn left at the intersection of KY Route 191 and KY 746.
3. Drive one mile and six tenths. Turn left onto gravel road (sign posted).
4. Drive approximately two hundred feet to the site (sign posted).

Prepared By:  
Daryl Bartley  
Cell Site Compliance Agent  
East Kentucky Network  
d/b/a Appalachian Wireless  
606-791-0310 (cell)  
606-339-1363 (fax)  
[dbartley@ekn.com](mailto:dbartley@ekn.com)

# Campton

Location:

1711 KY 746  
Campton, KY 41301

Coordinates:

37° 45' 50.32" N  
83° 31' 34.68" W

## Legend

 1/2 Mile Search Area



Google Earth

© 2020 Google



2000 ft

# Exhibit 8

RECEIVED

AUG 24 2020

WOLFE COUNTY CLERK  
STEPHEN OLIVER

MEMORANDUM OF LEASE

THIS MEMORANDUM OF LEASE is made and entered into on this 17<sup>th</sup> day of August, 2020, with a commencement date of August 1, 2020 (the "Commencement Date"), by and between JOHN MAYABB and GERALDINE MAYABB, a married couple, with an address of 1625 KY 746, Campton, Kentucky 41301, hereinafter referred to as "Lessors", and EAST KENTUCKY NETWORK, LLC D/B/A APPALACHIAN WIRELESS, a Kentucky limited liability company, with a mailing address of 101 Technology Trail, Ivel, Kentucky, 41642, hereinafter referred to as "Lessee."

WITNESSETH

1. **Demised Premises.** For good and valuable consideration, Lessors leased to Lessee, and Lessee has leased from Lessors that certain tract of real estate located in Wolfe County, Kentucky, and being a portion of the same land conveyed to John Mayabb and Betty Mayabb by Deed dated October 17, 1991, and recorded on October 17, 1991, in Deed Book 87, Page 684, and by Deed dated October 16, 1991, and recorded on October 17, 1991, in Deed Book 87, Page 682, both of record in the Wolfe County Clerk's Office. Said property is more particularly described in the description attached hereto and made a part hereof as **Exhibit A** and the plat attached hereto and made a part hereof as **Exhibit B**, prepared by James W. Caudill, Licensed Professional Land Surveyor (hereinafter referred to as the "Premises"). The Lessors have also granted unto Lessee full and complete rights of ingress, egress and regress to and from the Premises over any property owned by Lessors and other associated rights for installation of utilities, maintenance, and other purposes. Lessee has the absolute right to assign, sublease, sublicense or otherwise transfer, in whole or in part, the Leased Premises and the easements and rights-of-way.

2. **Term.** The initial term of the Lease is for a period of five (5) years from the Commencement Date set forth above.

3. **Renewals.** The Lease shall automatically renew for an additional seven (7) terms of five (5) years each, unless Lessee provides sixty (60) days written notice prior to the end of the current term that it does not wish to renew.

4. **Binding Effect.** All of the terms, conditions, and covenants hereof shall be binding and inure to the benefit of the parties and their respective heirs, representatives, successors, and assigns.

5. **Purpose.** This Memorandum of Lease is prepared solely for the purpose of recordation, and is not intended to, nor shall it be deemed to, modify any of the terms and conditions set forth in the Lease, nor to construe any of the rights, duties or responsibilities of Lessors and Lessee. In the event of any conflict between the terms and conditions of this Memorandum and the terms and conditions of the Lease, the terms and conditions of the Lease shall supersede and control.

**[THE REMAINDER OF THIS PAGE INTENTIONALLY LEFT BLANK.]**

IN WITNESS WHEREOF, Lessors and Lessee have caused their names to be signed

hereto, as of the date(s) indicated below.

LESSORS:

John Mayabb  
JOHN MAYABB

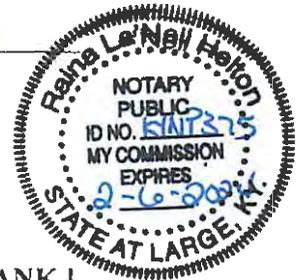
Geraldine Mayabb  
GERALDINE MAYABB

COMMONWEALTH OF KENTUCKY  
COUNTY OF Wolfe

The foregoing instrument was acknowledged before me on this 14<sup>th</sup> day of August, 2020, by John Mayabb and Geraldine Mayabb, Lessors.

Raina L. Helton  
Notary Public  
Commission No.: KYNP375

My Commission Expires 2-6-2024



[THE REMAINDER OF THIS PAGE INTENTIONALLY LEFT BLANK.]

LESSEE:

EAST KENTUCKY NETWORK, LLC D/B/A  
APPALACHIAN WIRELESS

WA Gillum

By: W.A. Gillum  
Its: CEO/ General Manager

COMMONWEALTH OF KENTUCKY

COUNTY OF Floyd

The foregoing instrument was acknowledged before me on this 18<sup>th</sup> day of August, 2020, by W.A. Gillum, CEO/General Manager of East Kentucky Network, LLC d/b/a Appalachian Wireless, Lessee.

Raina D. Helton

Notary Public

Commission No.: KYNP375

My Commission Expires 2-6-2024



This instrument was prepared by:

Krystal Branham

Krystal Branham, Attorney  
101 Technology Trail  
Ivel, Kentucky 41642  
(606) 477-2355



**LOT DESCRIPTION**

Property of  
John Mayabb and  
Betty Mayabb  
1625 Ky. 746  
Campton, KY 41301  
Off of Highway 746  
Near Campton  
in Wolfe County, Kentucky  
July 29, 2020

A certain tract or parcel of land lying in Wolfe County, Kentucky, and being a portion of the same tract of land conveyed to John Mayabb and Betty Mayabb, husband and wife, by General Warranty Deed, dated October 16, 1991, from Ruby Campbell, and of record in Deed Book 87 Page 682-684 of the records of the Wolfe County Court Clerk's Office. The tract is more particularly bounded and described as follows:

Lot 1A

Beginning at set iron pin marked LS#2259 at a 16" maple at a fence on the ridge; thence along the edge of the old road (now gone) South 59 deg 49 min 12 sec East, a distance of 24.16 feet to a set iron pin with cap marked LS#2259; thence continuing with old road South 50 deg 18 min 18 sec East, a distance of 48.62 feet to a set iron pin with cap marked LS#2259; thence still continuing with the old road South 42 deg 07 min 51 sec East, a distance of 52.47 feet to a set iron pin marked LS#2259; thence leaving the old road and down a trail no longer in use South 65 deg 56 min 00 sec West, a distance of 167.21 feet to a set iron pin marked LS#2259 at the edge of the old trail; thence up the hill North 17 deg 29 min 47 sec West, a distance of 138.67 feet to a set iron pin marked LS#2259 on the ridge; thence with the ridge North 79 deg 08 min 34 sec East, a distance 60.69 feet to a set iron pin with cap marked LS#2259 on ridge at fence; thence with fence and ridge North 80 deg 54 min 06 sec East, a distance of 41.80 feet to a set iron pin with cap marked LS#2259 to the point of the beginning. Containing a calculated area of 17,012.0 Sq. Feet, or 0.39 Acres.

Also to be included is an access road from the public highway # 746 to Lot 1A. This access road a being a portion of John Mayabb and Betty Mayabb property in deed book 87 pages 682-684 and deed book 67 page 390. Also to be included is a right to install fiber and utility lines in or along said access road and/or such other location to be agreed upon by the parties.

Unless stated otherwise, any monument referred to herein as "set iron pin with cap" is a set 1/2" diameter rebar, at least eighteen (18") in length, with a plastic cap stamped "LS-2259". All bearings stated herein are referred to NAD83, KY single zone of the Kentucky state plane system.

This survey was performed on July 28, 2020 by James W. Caudill, a Kentucky Licensed Professional Land Surveyor No. 2259

*James W. Caudill*  
James W. Caudill, PLS #2259

STATE OF KENTUCKY  
COUNTY OF WOLFE  
I, STEVE OLIVER, County Clerk for the County  
and State aforesaid, certify that the foregoing  
LEASE was on August 24, 2020 0:00 AM

lodged for record, whereupon the same with the foregoing  
and this certificate have been duly recorded in my office.

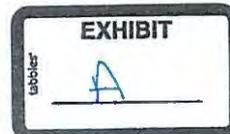
WITNESS my hand this August 24, 2020  
STEVE OLIVER, CLERK

BY: D.C.

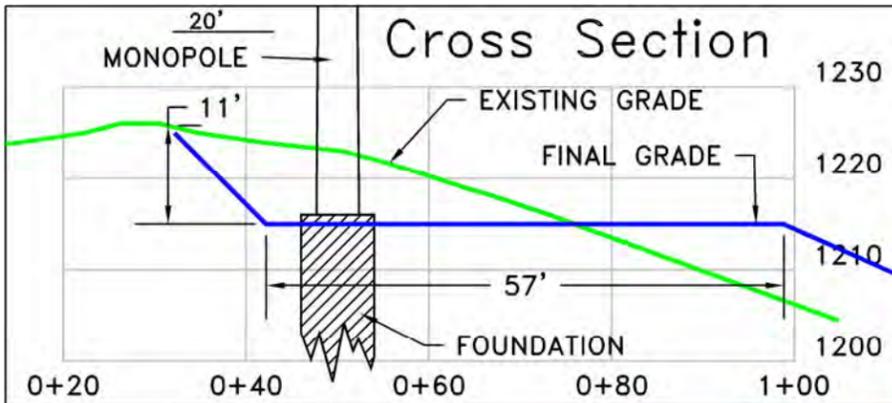


Book: 41  
Name: LEASE  
STEVE OLIVER  
WOLFE COUNTY  
8/24/2020 0:00 AM  
D.C: corinna

Pages: 396-401 (6)  
Deed Tax: \$0.00



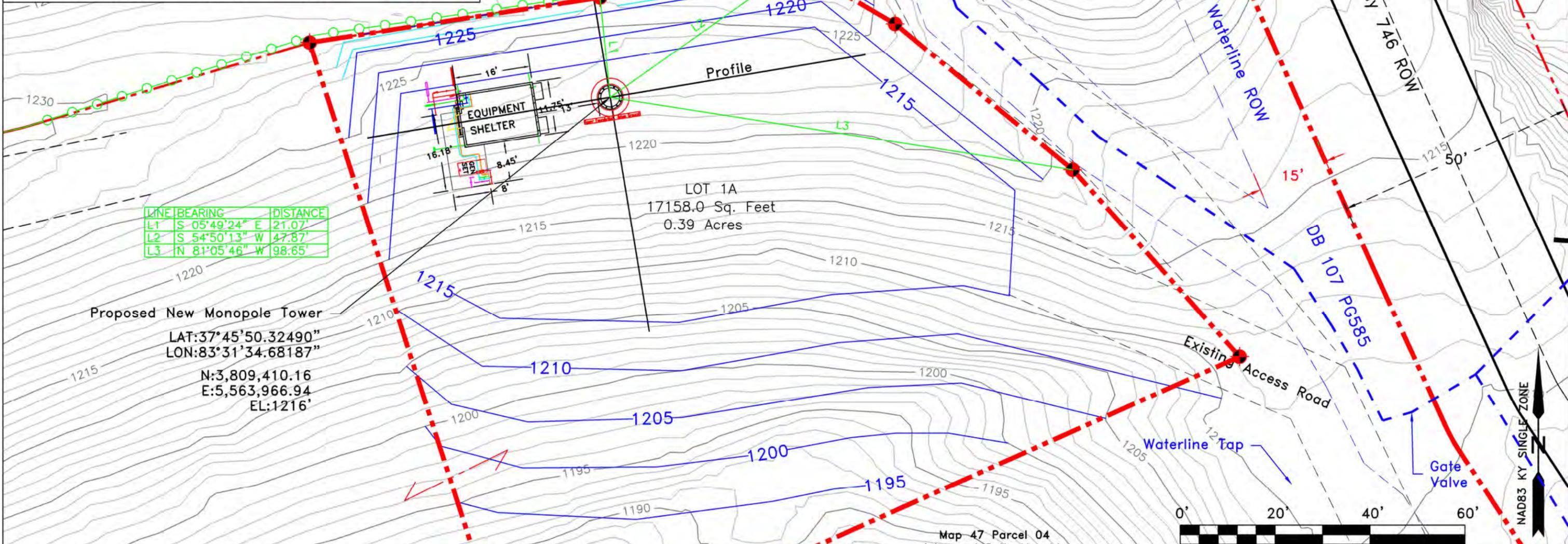
# Exhibit 9



Map 46 Parcel 41  
 Todd Haddix  
 212 Lowell Leshar Road  
 Campton, KY 41301  
 Deed Book 131  
 Page 161

APPALACHIAN WIRELESS  
 101 TECHNOLOGY TRAIL  
 IVEL, KY. 41642  
 PROPOSED NEW TOWER  
 OFF HWY 746 NEAR CAMPTON  
 IN WOLFE COUNTY, KY.

Existing Tower  
 East Kentucky Network, LLC  
 d/b/a Appalachian Wireless  
 101 Technology Trail  
 Ivel, Ky 41642



| LINE | BEARING       | DISTANCE |
|------|---------------|----------|
| L1   | S 05°49'24" E | 21.07'   |
| L2   | S 54°50'13" W | 47.87'   |
| L3   | N 81°05'46" W | 98.65'   |

Proposed New Monopole Tower  
 LAT: 37°45'50.32490"  
 LON: 83°31'34.68187"  
 N: 3,809,410.16  
 E: 5,563,966.94  
 EL: 1216'

Map 47 Parcel 04  
 John and Betty Mayabb  
 1625 Ky. 746  
 Campton, KY 41301  
 DB 87 PG 682-684

"I certify that the latitude 37°45'50.32490"N and longitude 83°31'34.68187"W are within +/- 50 feet horizontally; and the site elevation 1216 ft. MSL, is within +/- 20 feet vertically. With a structure height of 190 ft AGL, the overall height is 1406 ft, AMSL. The horizontal datum (coordinates) is in terms of the North American Datum Of 1983 (NAD 83). The vertical datum heights are in terms of the North American Vertical Datum of 1988, and are determined to the nearest foot."

SIGNED: *James W. Caudill* PE 12305 LS 2259 01/07/21  
 PRINTED: JAMES W. CAUDILL PE #12305 LS #2259 DATE

-THE PROPOSED TOWER HAS BEEN LOCATED USING DUAL FREQUENCY GPS UNIT PROCESSED BY "OPUS"  
 -STATE PLANE COORDINATES NAD 83 KY SINGLE ZONE N:3809410.16, E:5563966.94, EL 1215' FINAL GRADE TOP OF FOUNDATION EL 1216'-TOP TOWER EL 1406'  
 -PRECISION: HORIZONTAL=50' VERTICAL=20'  
 -THIS SURVEY MEETS OBSTACLE ACCURACY CODE 2C.  
 -PROPERTY LINE INFORMATION TAKEN FROM DEEDS

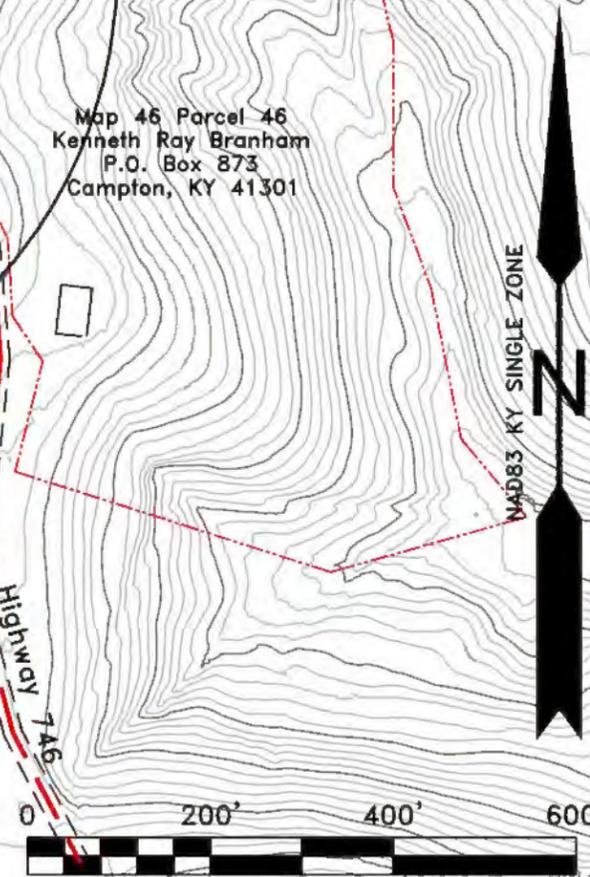
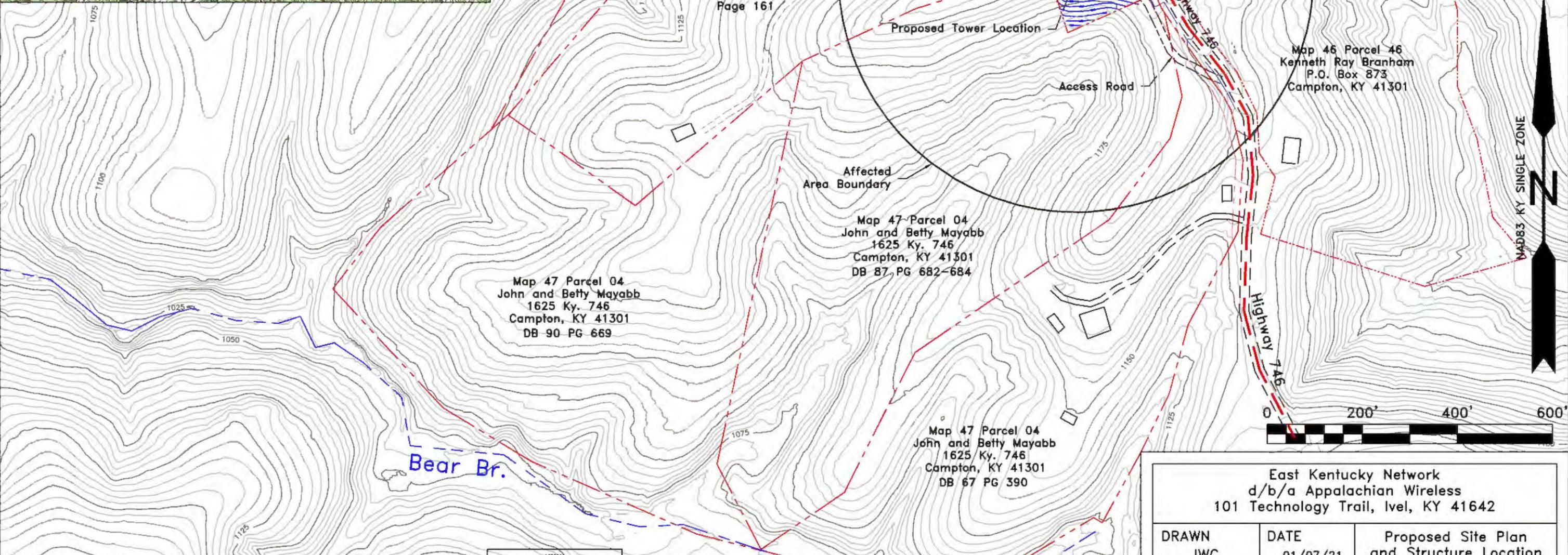
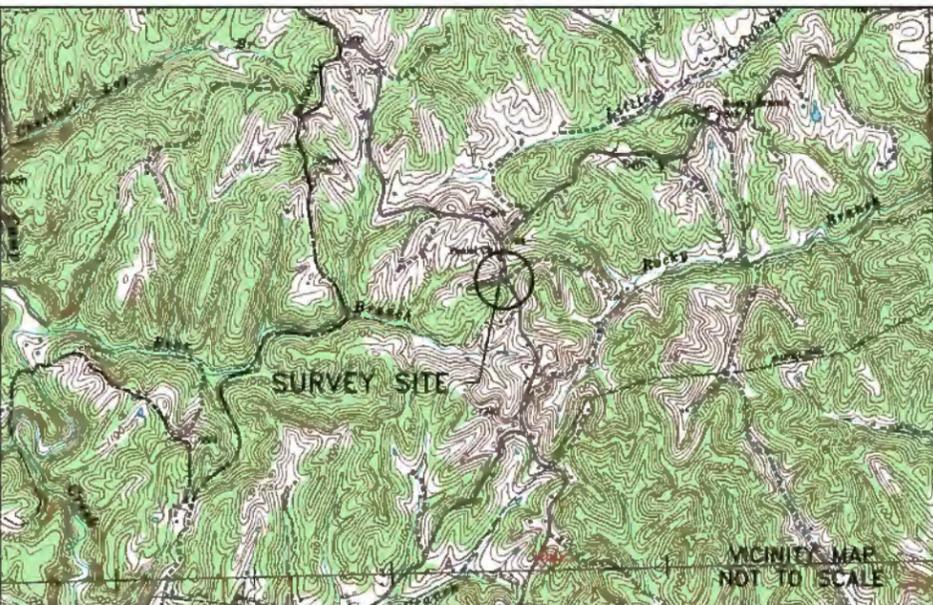


SURVEY STA SET FOUND  
 IRON PIN WITH CAP (18" X .5" REBAR PLASTIC CAP MARKED LS2259)  
 BOUNDARY LINE  
 ROAD  
 WATER LINE

| East Kentucky Network<br>d/b/a Appalachian Wireless<br>101 Technology Trail, Ivel, KY 41642 |                  |  |
|---|------------------|--|
| DRAWN<br>JWC  | DATE<br>01/07/21 | Campton Tower Site<br>Tower Replacement<br>Proposed Layout<br>Located off of Hwy 746<br>Wolfe County, Kentucky |
| APPROVED<br>JWC   | DATE<br>01/07/21 |  |
| SCALE<br>1" = 20'   | SHEET<br>2 of 3  | PROJECT NO.<br>Campton/mayabb 2c 20  |

# Exhibit 10

APPALACHIAN WIRELESS  
 101 TECHNOLOGY TRAIL  
 IVEL, KY. 41642  
 PROPOSED NEW TOWER  
 CAMPTON IN WOLFE COUNTY



|   |                  |  |
|---|------------------|--|
| East Kentucky Network<br>d/b/a Appalachian Wireless<br>101 Technology Trail, Ivel, KY 41642 |                  |  |
| DRAWN<br>JWC  | DATE<br>01/07/21 | Proposed Site Plan<br>and Structure Location<br>Campton Tower Site<br>Off Highway 746<br>in Wolfe Co., KY. |
| APPROVED<br>JWC   | DATE<br>01/07/21 |  |
| SCALE<br>1" = 200'  | SHEET<br>1 of 3  | PROJECT NO.<br>Campton/Campton200PVA   |

**J W CAUDILL ENGINEERING**  
 9283 HWY 15 STE. C ISOM, KY 41824  
 ENGINEER'S CERTIFICATE: I HEREBY CERTIFY THAT INFORMATION SHOWN  
 REFLECTS THE INFORMATION OBTAINED AND PROVIDED BY THE WOLFE COUNTY  
 PROPERTY VALUATION ADMINISTRATION OFFICE IN CAMPTON, KY.  
*James W. Caudill* 12305 01/07/21  
 JAMES W. CAUDILL P.E.# DATE



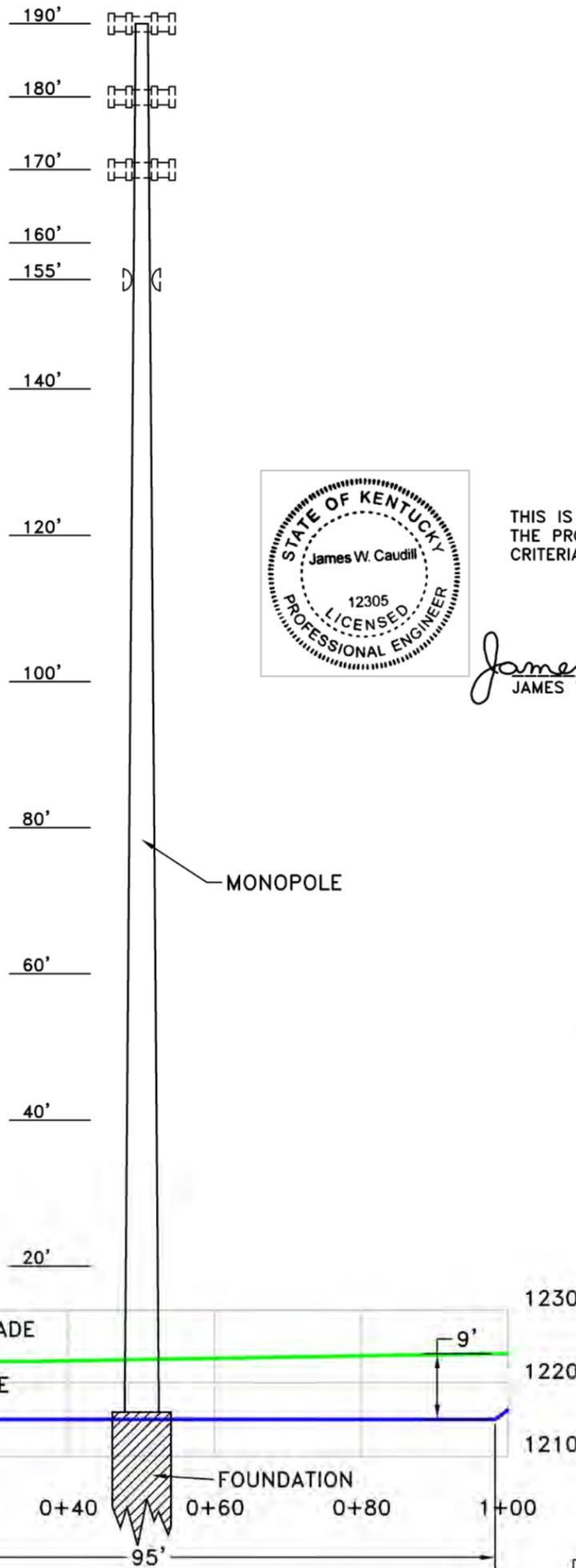
Map 47 Parcel 03  
 B. Scott Graham  
 P.O. Box 637  
 Stanton, KY 40380  
 DB 122 PG 455

LEGEND

|               |       |
|---------------|-------|
| PROPERTY LINE | ---   |
| ACCESS ROAD   | ----  |
| LOT BOUNDARY  | -.-.- |

# Exhibit 11

# PROFILE WITH TOWER



THIS IS A VERTICAL PROFILE SKETCH OF THE TOWER INDICATING THE PROPOSED ANTENNA AND DISH ELEVATIONS. NO DESIGN CRITERIA WAS CONSIDERED IN THE PREPARATION OF THIS DRAWING.

*James W. Caudill* 12305 01/07/21  
 JAMES W. CAUDILL PE #. DATE

NOTE: SEE FOUNDATION DRAWINGS FOR DETAILS

01/07/21  
 SCALE 1" = 20'



|   |                  |  |
|---|------------------|--|
| East Kentucky Network<br>d/b/a Appalachian Wireless<br>101 Technology Trail, Ivel, KY 41642 |                  |  |
| DRAWN<br>JWC  | DATE<br>01/07/21 | Campton Tower Site<br>Tower Replacement<br>Proposed Layout<br>Located off of Hwy 746<br>Wolfe County, Kentucky |
| APPROVED<br>JWC   | DATE<br>01/07/21 |  |
| SCALE<br>1" = 20'   | SHEET<br>3 of 3  | PROJECT NO.<br>Campton/mayabb 2c 20  |

# Exhibit 12

| Utility ID | Utility Name  | Utility Type | Class | City            | State |
|------------|---|--------------|-------|-----------------|-------|
| 4107900    | 365 Wireless, LLC                                     | Cellular     | D     | Atlanta         | GA    |
| 4109300    | Access Point, Inc.                                    | Cellular     | D     | Cary            | NC    |
| 4108300    | Air Voice Wireless, LLC                               | Cellular     | A     | Bloomfield Hill | MI    |
| 4110650    | Alliant Technologies of KY, L.L.C.                    | Cellular     | C     | Morristown      | NJ    |
| 44451184   | Alltel Communications, LLC                            | Cellular     | A     | Basking Ridge   | NJ    |
| 4110850    | AltaWorx, LLC   | Cellular     | C     | Fairhope        | AL    |
| 4107800    | American Broadband and Telecommunications Company     | Cellular     | C     | Toledo          | OH    |
| 4108650    | AmeriMex Communications Corp.                         | Cellular     | D     | Dunedin         | FL    |
| 4105100    | AmeriVision Communications, Inc. d/b/a Affinity 4     | Cellular     | D     | Virginia Beach  | VA    |
| 4110700    | Andrew David Balholm dba Norcell                      | Cellular     | C     | Clayton         | WA    |
| 4108600    | BCN Telecom, Inc.                                     | Cellular     | D     | Morristown      | NJ    |
| 4110550    | Blue Casa Mobile, LLC                                 | Cellular     | D     | Santa Barbara   | CA    |
| 4108750    | Blue Jay Wireless, LLC                                | Cellular     | C     | Carrollton      | TX    |
| 4111050    | BlueBird Communications, LLC                          | Cellular     | C     | New York        | NY    |
| 4202300    | Bluegrass Wireless, LLC                               | Cellular     | A     | Elizabethtown   | KY    |
| 4107600    | Boomerang Wireless, LLC                               | Cellular     | B     | Hiawatha        | IA    |
| 4105500    | BullsEye Telecom, Inc.                                | Cellular     | D     | Southfield      | MI    |
| 4110050    | CampusSims, Inc.                                      | Cellular     | D     | Boston          | MA    |
| 4100700    | Cellco Partnership dba Verizon Wireless               | Cellular     | A     | Basking Ridge   | NJ    |
| 4106600    | Cintex Wireless, LLC                                  | Cellular     | D     | Rockville       | MD    |
| 4111000    | ComApp Technologies LLC                               | Cellular     | C     | Melrose         | MA    |
| 4101900    | Consumer Cellular, Incorporated                       | Cellular     | A     | Portland        | OR    |
| 4106400    | Credo Mobile, Inc.                                    | Cellular     | A     | San Francisco   | CA    |
| 4108850    | Cricket Wireless, LLC                                 | Cellular     | A     | San Antonio     | TX    |
| 4001900    | CTC Communications Corp. d/b/a EarthLink Business I   | Cellular     | D     | Grand Rapids    | MI    |
| 10640      | Cumberiand Cellular Partnership                       | Cellular     | A     | Elizabethtown   | KY    |
| 4101000    | East Kentucky Network, LLC dba Appalachian Wireless   | Cellular     | A     | Ivel            | KY    |
| 4002300    | Easy Telephone Service Company dba Easy Wireless      | Cellular     | D     | Ocala           | FL    |
| 4109500    | Enhanced Communications Group, LLC                    | Cellular     | D     | Bartlesville    | OK    |
| 4110450    | Excellus Communications, LLC                          | Cellular     | D     | Chattanooga     | TN    |
| 4105900    | Flash Wireless, LLC                                   | Cellular     | C     | Concord         | NC    |
| 4104800    | France Telecom Corporate Solutions L.L.C.             | Cellular     | D     | Oak Hill        | VA    |
| 4109350    | Global Connection Inc. of America                     | Cellular     | D     | Norcross        | GA    |
| 4102200    | Globalstar USA, LLC                                   | Cellular     | B     | Covington       | LA    |
| 4109600    | Google North America Inc.                             | Cellular     | A     | Mountain View   | CA    |
| 33350363   | Granite Telecommunications, LLC                       | Cellular     | D     | Quincy          | MA    |
| 4106000    | GreatCall, Inc. d/b/a Jitterbug                       | Cellular     | A     | San Diego       | CA    |
| 10630      | GTE Wireless of the Midwest dba Verizon Wireless      | Cellular     | A     | Basking Ridge   | NJ    |
| 4110600    | Horizon River Technologies, LLC                       | Cellular     | C     | Atlanta         | GA    |
| 4103100    | i-Wireless, LLC                                       | Cellular     | A     | Newport         | KY    |
| 4109800    | IM Telecom, LLC d/b/a Infiniti Mobile                 | Cellular     | D     | Tulsa           | OK    |
| 22215360   | KDDI America, Inc.                                    | Cellular     | D     | New York        | NY    |
| 10872      | Kentucky RSA #1 Partnership                           | Cellular     | A     | Basking Ridge   | NJ    |
| 10680      | Kentucky RSA #3 Cellular General                      | Cellular     | A     | Elizabethtown   | KY    |
| 10681      | Kentucky RSA #4 Cellular General                      | Cellular     | A     | Elizabethtown   | KY    |
| 4109750    | Konatel, Inc. dba telecom.mobi                        | Cellular     | D     | Johnstown       | PA    |
| 4110900    | Lunar Labs, Inc.                                      | Cellular     | C     | Detroit         | MI    |
| 4107300    | Lycamobile USA, Inc.                                  | Cellular     | D     | Newark          | NJ    |
| 4108800    | MetroPCS Michigan, LLC                                | Cellular     | A     | Bellevue        | WA    |
| 4109650    | Mitel Cloud Services, Inc.                            | Cellular     | D     | Mesa            | AZ    |
| 4202400    | New Cingular Wireless PCS, LLC dba AT&T Mobility, PCS | Cellular     | A     | San Antonio     | TX    |
| 10900      | New Par dba Verizon Wireless                          | Cellular     | A     | Basking Ridge   | NJ    |
| 4000800    | Nextel West Corporation                               | Cellular     | D     | Overland Park   | KS    |
| 4001300    | NPCR, Inc. dba Nextel Partners                        | Cellular     | D     | Overland Park   | KS    |

|          |   |          |   |                |    |
|----------|---|----------|---|----------------|----|
| 4001800  | OnStar, LLC   | Cellular | A | Detroit        | MI |
| 4110750  | Onvoy Spectrum, LLC   | Cellular | C | Plymouth       | MN |
| 4109050  | Patriot Mobile LLC  | Cellular | D | Southlake      | TX |
| 4110250  | Plintron Technologies USA LLC                                   | Cellular | D | Bellevue       | WA |
| 33351182 | PNG Telecommunications, Inc. dba PowerNet Global Communications | Cellular | D | Cincinnati     | OH |
| 4202100  | Powertel/Memphis, Inc. dba T-Mobile                             | Cellular | A | Bellevue       | WA |
| 4107700  | Puretalk Holdings, LLC  | Cellular | A | Covington      | GA |
| 4106700  | Q Link Wireless, LLC  | Cellular | A | Dania          | FL |
| 4108700  | Ready Wireless, LLC   | Cellular | B | Hiawatha       | IA |
| 4110500  | Republic Wireless, Inc.   | Cellular | D | Raleigh        | NC |
| 4111100  | ROK Mobile, Inc.  | Cellular | C | Culver City    | CA |
| 4106200  | Rural Cellular Corporation                                      | Cellular | A | Basking Ridge  | NJ |
| 4108550  | Sage Telecom Communications, LLC dba TruConnect                 | Cellular | D | Los Angeles    | CA |
| 4109150  | SelecTel, Inc. d/b/a SelecTel Wireless                          | Cellular | D | Freemont       | NE |
| 4106300  | SI Wireless, LLC  | Cellular | A | Carbondale     | IL |
| 4110150  | Spectrotel, Inc. d/b/a Touch Base Communications                | Cellular | D | Neptune        | NJ |
| 4200100  | Sprint Spectrum, L.P.   | Cellular | A | Atlanta        | GA |
| 4200500  | SprintCom, Inc.   | Cellular | A | Atlanta        | GA |
| 4109550  | Stream Communications, LLC                                      | Cellular | D | Dallas         | TX |
| 4110200  | T C Telephone LLC d/b/a Horizon Cellular                        | Cellular | D | Red Bluff      | CA |
| 4202200  | T-Mobile Central, LLC dba T-Mobile                              | Cellular | A | Bellevue       | WA |
| 4002500  | TAG Mobile, LLC   | Cellular | D | Carrollton     | TX |
| 4109700  | Telecom Management, Inc. dba Pioneer Telephone                  | Cellular | D | South Portland | ME |
| 4107200  | Telefonica USA, Inc.  | Cellular | D | Miami          | FL |
| 4108900  | Telrite Corporation dba Life Wireless                           | Cellular | D | Covington      | GA |
| 4108450  | Tempo Telecom, LLC  | Cellular | D | Kansas City    | MO |
| 4109950  | The People's Operator USA, LLC                                  | Cellular | D | New York       | NY |
| 4109000  | Ting, Inc.  | Cellular | A | Toronto        | ON |
| 4110400  | Torch Wireless Corp.  | Cellular | D | Jacksonville   | FL |
| 4103300  | Touchtone Communications, Inc.                                  | Cellular | D | Whippany       | NJ |
| 4104200  | TracFone Wireless, Inc.   | Cellular | D | Miami          | FL |
| 4002000  | Truphone, Inc.  | Cellular | D | Durham         | NC |
| 4110300  | UVNV, Inc.  | Cellular | D | Costa Mesa     | CA |
| 4105700  | Virgin Mobile USA, L.P.   | Cellular | A | Atlanta        | GA |
| 4110800  | Visible Service LLC   | Cellular | C | Lone Tree      | CO |
| 4106500  | WiMacTel, Inc.  | Cellular | D | Palo Alto      | CA |
| 4110950  | Wing Tel Inc.   | Cellular | C | New York       | NY |
| 4109900  | Wireless Telecom Cooperative, Inc. dba theWirelessFreeway       | Cellular | D | Louisville     | KY |

# Exhibit 13

S & S Tower Services  
120 Branden Dr.  
Mousie, KY 41839

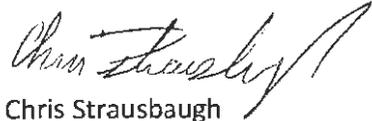
Kentucky Public Service Commission  
211 Sower Blvd.  
P.O. Box 615  
Frankfort, KY 40602-0615

Dear Commissioners:

The Construction Manager for the proposed communications facility will be Dave Strausbaugh. His contact information is (606) 497-6730 or [dstrausbaugh010@gmail.com](mailto:dstrausbaugh010@gmail.com).

Dave has been in the industry completing civil construction and constructing towers since 1991. He has worked for S&S Tower Services since 2015 as Construction Manager overseeing the construction of telecommunications towers and sites.

Thank you,



Chris Strausbaugh  
Owner  
S&S Tower Services  
(606) 497-5798